

LIGHT SHIP SWBS WEIGHT GROUP STUDY REPORT

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### Introduction

A study was undertaken to examine the relationships between three digit SWBS weight groups in groups 2, 3, 5, and 6, and various characteristics of a ship displacing less than 3600 tons. Of particular interest, was a comparison of real ship data (i.e., data obtained from ships already built, already under construction, or of sufficiently detailed design as to make their weight reports reliable) to the algorithms currently being used in the SESDOC program to predict group weights.

### Background

The eleven ships used as the database for this study are shown in Table I. These ships range from the 135 LT SES-110 to the 3585 LT FFG-7 (Olive Hazard Perry). With the exception of the SES-110, all of the ships are combatants and all except the 3KSES and PCM have been built. The PCG-612 is a ship which was built specifically for the Royal Saudi Naval Forces. The PG-92, FF1049, FF1059, and PF-103 are all older ships which have not benefitted from the latest in lightweight materials and technology. However, they were still considered useful for this study.

Two basic types of plots were created using these ship's data; SWBS group weight vs. ship displacement and SWBS group weight vs. the SESDOC algorithm's driving variable (see Table II). Only a few of the SESDOC algorithms were plotted since there was limited information readily available on SESDOC variables such as ship volume, complement breakdown (number of CPO's, etc.), and installed kW.

### Plot Description

In the plots which follow, a set of symbols is used to indicate the data points which belong to each ship. These are shown in Table I along with the displacement of each ship.

The plots of Section I show the algorithms from SESDOC (indicated by the dashed lines) and the corresponding points from the database. These plots compare data obtained from SESDOC with "real world" ship's data.

Section II plots contain curves which were drawn to represent a reasonable approximation of real data. These are not arithmetic curve fits. They were included only to indicate the trend the data appears to follow.

Section III contains those plots which were originally intended for Section II, but could not be used. These plots either contained too little data or too scattered data to be able to determine a trend.

### Problems Encountered

A major problem in collection of data involved older ships data being recorded in the old BSCI weight groups. The BSCI groups were more general than the current SWBS weight groups, so one BSCI group might encompass as many as eleven SWBS groups. There being no way to break the BSCI group down into SWBS groups, plots of the BSCI groups were made using the older BSCI data and the appropriate combinations of SWBS data (see sections II and III). While this is not directly comparable to the SESDOC algorithmns, they can still provide information as to the trends of group combinations.

Obtaining data on ship volumes also proved to be difficult. The NAVSEA technical data bank did not contain volume data. Most of the data obtained was gotten from individuals in SEA 501 who happened to have reports with the needed infomation. It was suggested that the Arrangements Branch (SEA 55W1) might have volume information available, but there was not sufficient time during the course of this study to find out. Any future investigation should check this source.

### Conclusions and Recommendations

With the data collected thus far, it appears that the vast majority of the SESDOC algorithmns are valid approximations of SWBS group weights. A few are somewhat optimistic (Group W583, for example), but generally the algorithmns are, if anything, conservative estimates (see Group W651).

A great deal more study should be done to refine the algorithmns even though they look quite good now. With only eleven ships in the database and a great lack of other data (volumes, etc.), this study has only begun the work needed to document SESDOC's accuracy or determine other useful algorithmns. With proper documentation and refinement, the SESDOC algorithmns could prove to be an invaluable design tool.

TABLE 1 - Ship Indicator Symbols and Displacements

<u>SHIP</u>	<u>SYMBOL</u>	<u>DISPLACEMENT</u>
SES-110	△	135
PCG-612	□	680
3KSES	○	3021
PCM	◊	560
PHM-1	◇	231
PHM-3	◊	231
PG-92	□	242
FF-1059	▽	2931
FF-1049	◊	2511
PF-103	▶	1106
FFG-7	◀	3585

AGEH-1 = H1  
PCH-1 = H2  
PHM-1 = H3  
JEFF A = H4  
ROHR 10/76 = H5  
BELL 5/75 = H6  
BELL 3/76 = H7  
MXSES = H8  
SES 100A = H9  
LSES = H10  
LOCK 2K = H11  
PGH 2 = H12

DLG 26 = D1  
DLGN 35 = D2  
DE 1057 = D3  
DLGN 38 = D4

PF 105 = P1  
PGM 94 = P2  
PCG 612 = P3  
PGG 511 = P4

FFG 7 = F1

CVN 67 = C1  
CVN 68/69 = C2

LPH 12 = L1  
LHA 4 = L2  
LST 1179 = L3  
LSD 37 = L4  
LPD 13 = L5  
LCU 1646 = L6  
LKA 117 = L7

TAGOR 16 = A1  
AE 35 = A2  
AS 40 = A3  
AD 37 = A4

VOLUME  $\times 10^{-6}$

TABLE 2 - SESDOC Equations For Weight

<u>SWBS GROUP</u>	<u>SESDOC EQUATION</u>
331	= 0.00739 VOLA
332	= 0.02678 COMP
511	= 0.02 COMP
512	= 0.028 COMP
513	= 0.075 VSH
514	= 0.4 + 0.025 VOLA + 0.07 COMP
531	= 0.036 COMP <sup>1.1045</sup>
533	= 0.03077 COMP
556	= 1 + 0.025 VOLA
581	= 0.0085 VOLA
582	= 0.00001 VOLA
583	= 0.015 COMP
593	= 0.04 VOLA
622	= 0.0134 VOLA
625	= 0.60 + 0.00001 VLSS
635	= 0.036 VOLA
637	= 0.018 VOLA
641	= 0.32 NOFF
644	= 0.01444 COMP
651	= 0.085 COMP
652	= 0.0075 COMP
664	= 0.022 VOLA
671	= 0.024 VOLA

VOLA = SHIP VOLUME ( $\text{ft}^3/1000$ )

COMP = COMPLEMENT

VSH = VOLUME OF SIDEHULLS ( $\text{ft}^3/1000$ )VLSS = VOLUME OF SUPERSTRUCTURE ( $\text{ft}^3/1000$ )

NOFF = NUMBER OF OFFICERS

REFERENCES

1. "Shipwork Breakdown Structure," The Naval Ship Engineering Center, NAVSEA 0900-LP-039-9010 (1 Aug 1977).
2. SES-110 Final Weight Report
3. "PCG/PGG Data Package", PMS 304-10 (19 Feb 1981).
4. Estimated Weight Report for 3KSES
5. Calculated Weight Report for PCM
6. Final Weight Report for PHM-1 and PHM-3
7. Final Weight Report for PGM-92
8. Final Weight Report for DE-1059
9. Final Weight Report for DE-1049
10. Final Weight Report for PF-103
11. Final Weight Report for FFG-7

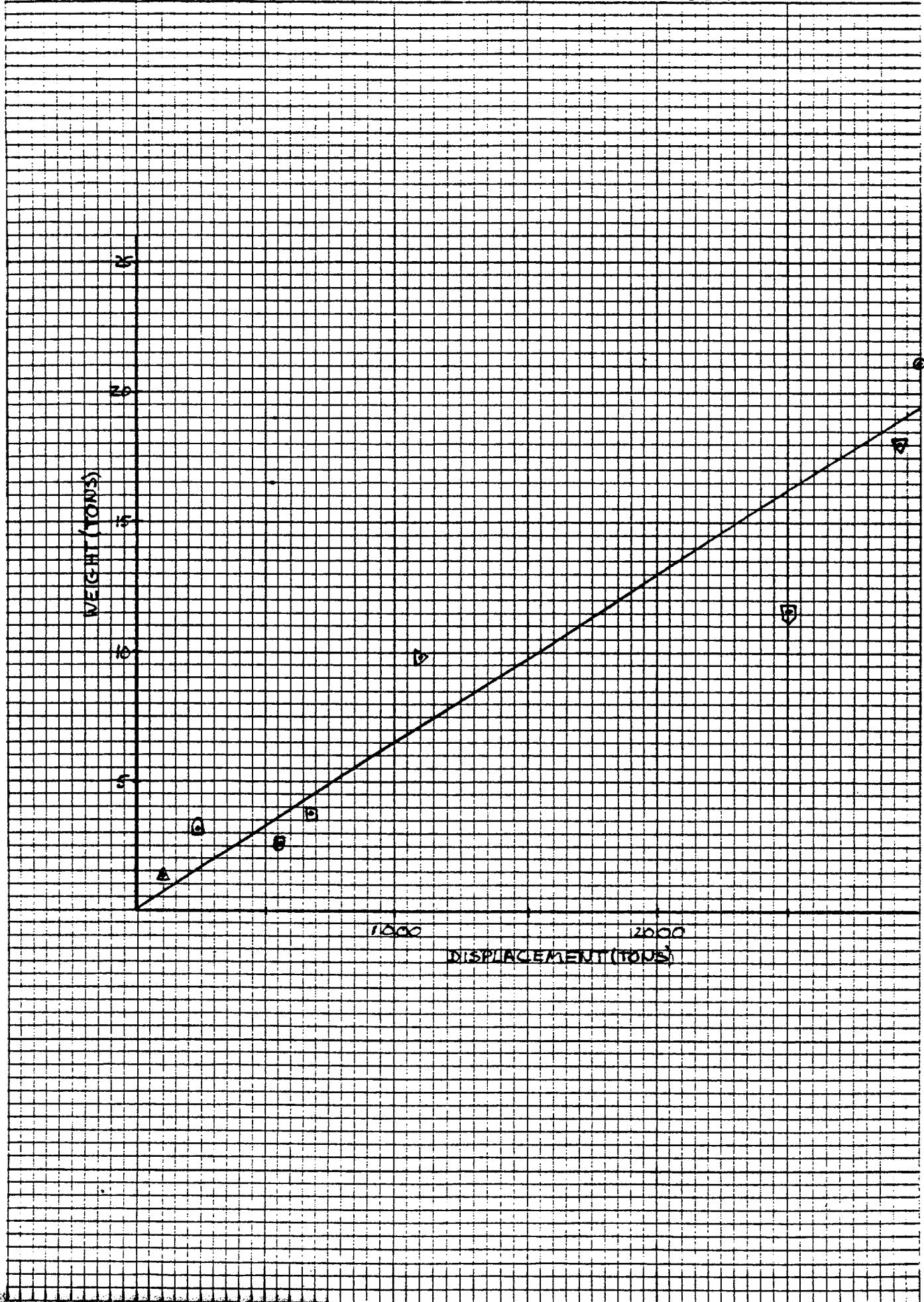
**SECTION I**

**SESDOC Algorithmn Plots**

PSC = 225

SWEI GROUPS W 162 + 25°

FRAME 10X10 TO 1 INCH  
10TH IMP FREQU



SPI.MI - 20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED

WEIGHT (TONS)

2 5 8 11 14 17 20 23 26 29 32 35 38 41 44 47 50 53 56

TONS

DISPLACEMENT (TONS)

TONS

TONS

KSC #605

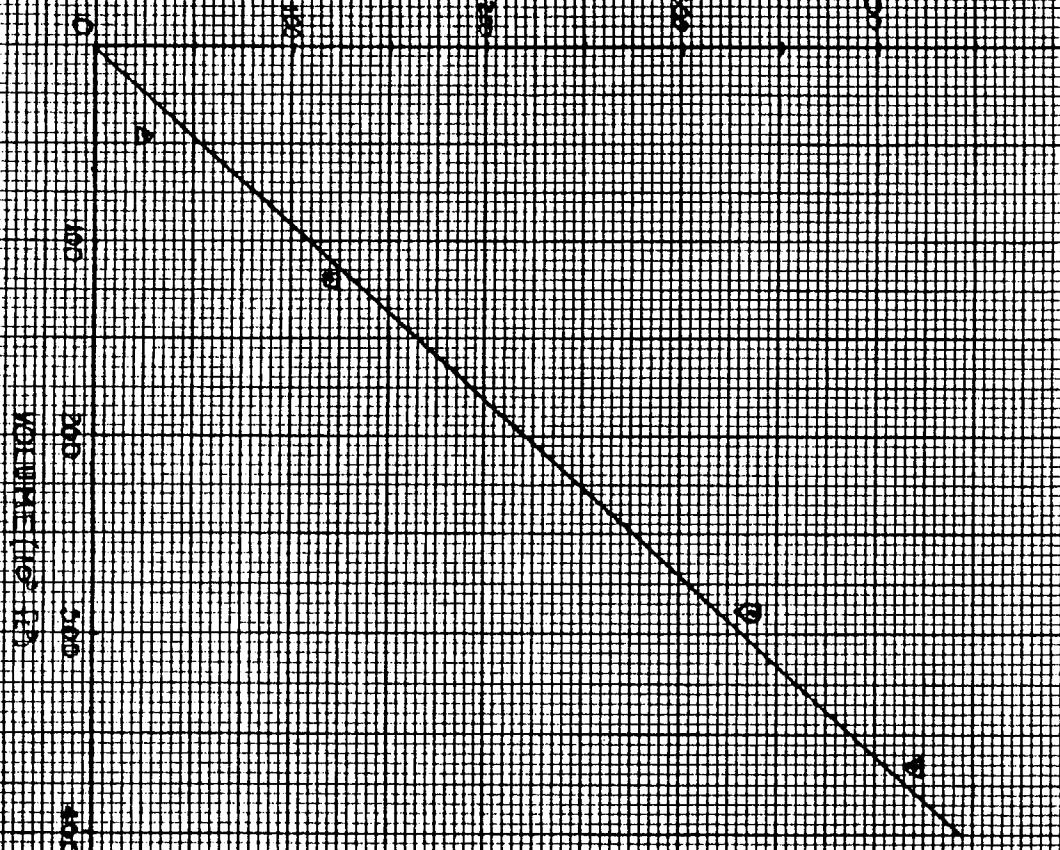
SWPC GRADIDE W100-50-304 1002812

## **SECTION II**

**Real Ship Data Trend Plots**

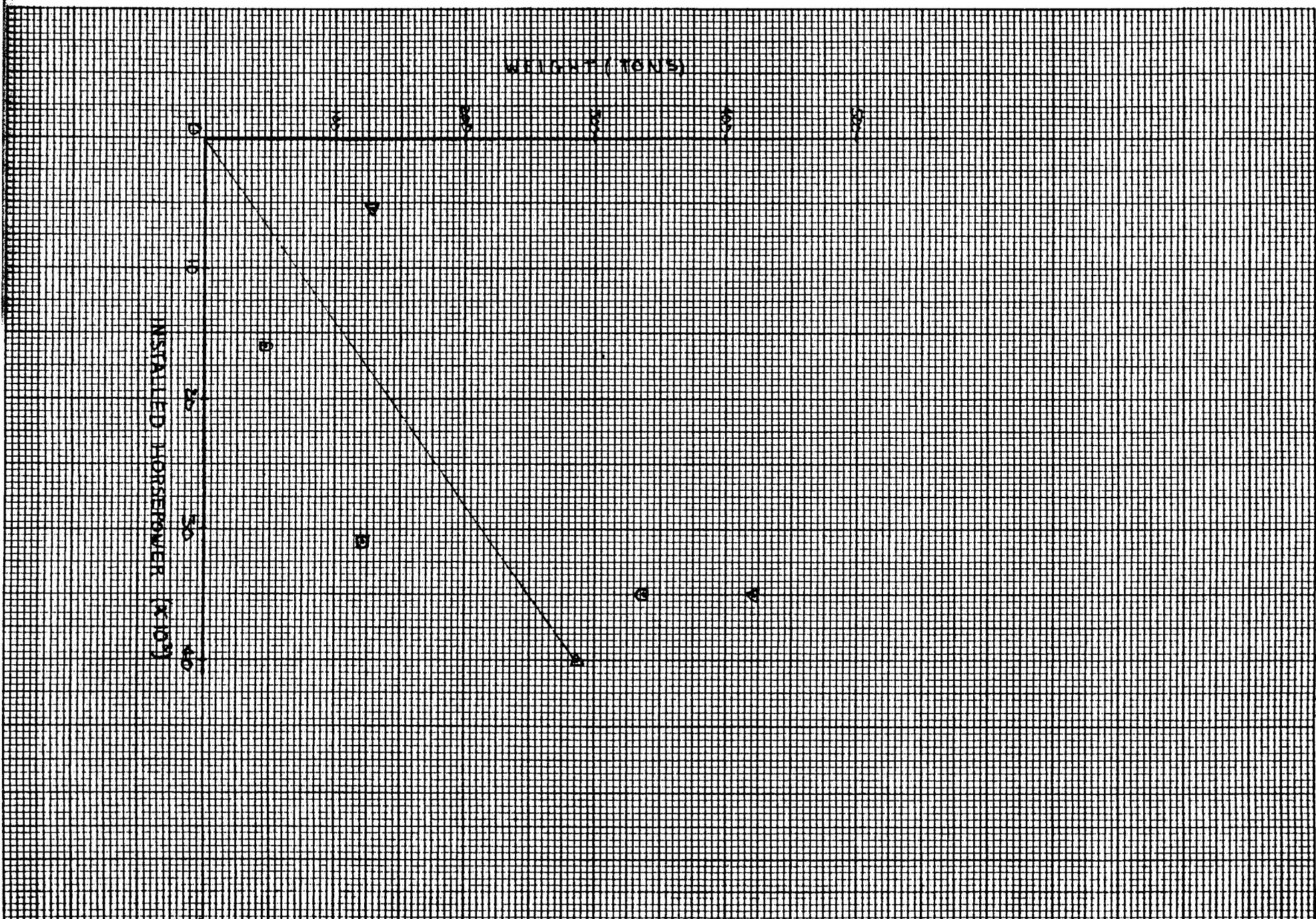
FPM. 20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED

WEIGHT (TONS)



SUPER SWINE 2 TOTAL SHIP VOLUME

FPI MI-20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED

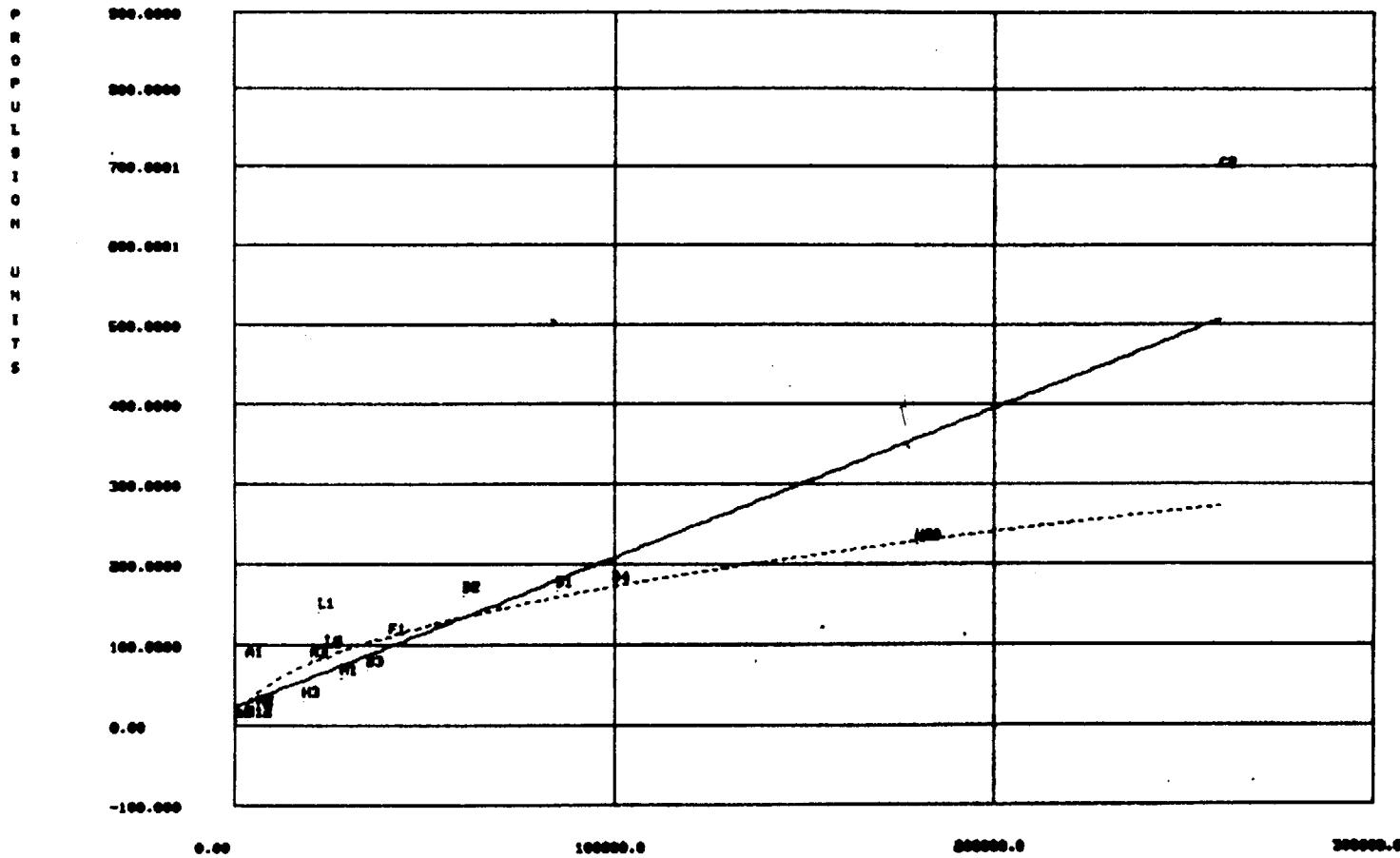


TO CONTINUE, TYPE CONTINUE

0 CONTINUE

PROPELLUTION UNITS (W230-W42) VS SHP

— ALL DATA —— 0.00000 —— 1.00000



W230 = 23.671 + 0.00164 SHP<sup>1.010</sup>  
= 6.610 + 0.833 SHP<sup>0.416</sup>

WT 233 Propul & st Comb Engines.

WT 234 GT

SPLOM-10 X 10 TO 1 RICH  
10TH LINE HEAVY

WEIGHT (TONS)

0 10 20 30

①

②

1000

2000

DISPLACEMENT (TONS)

1234 GAS TURBINES

PP1 (OM. 10 X 10 1/2 X 1 INCH  
10TH TIME HEAVY)

WEIGHT (TONS)

0 10 20 30 40 50 60 70

B E

DISPLACEMENT (TONS)

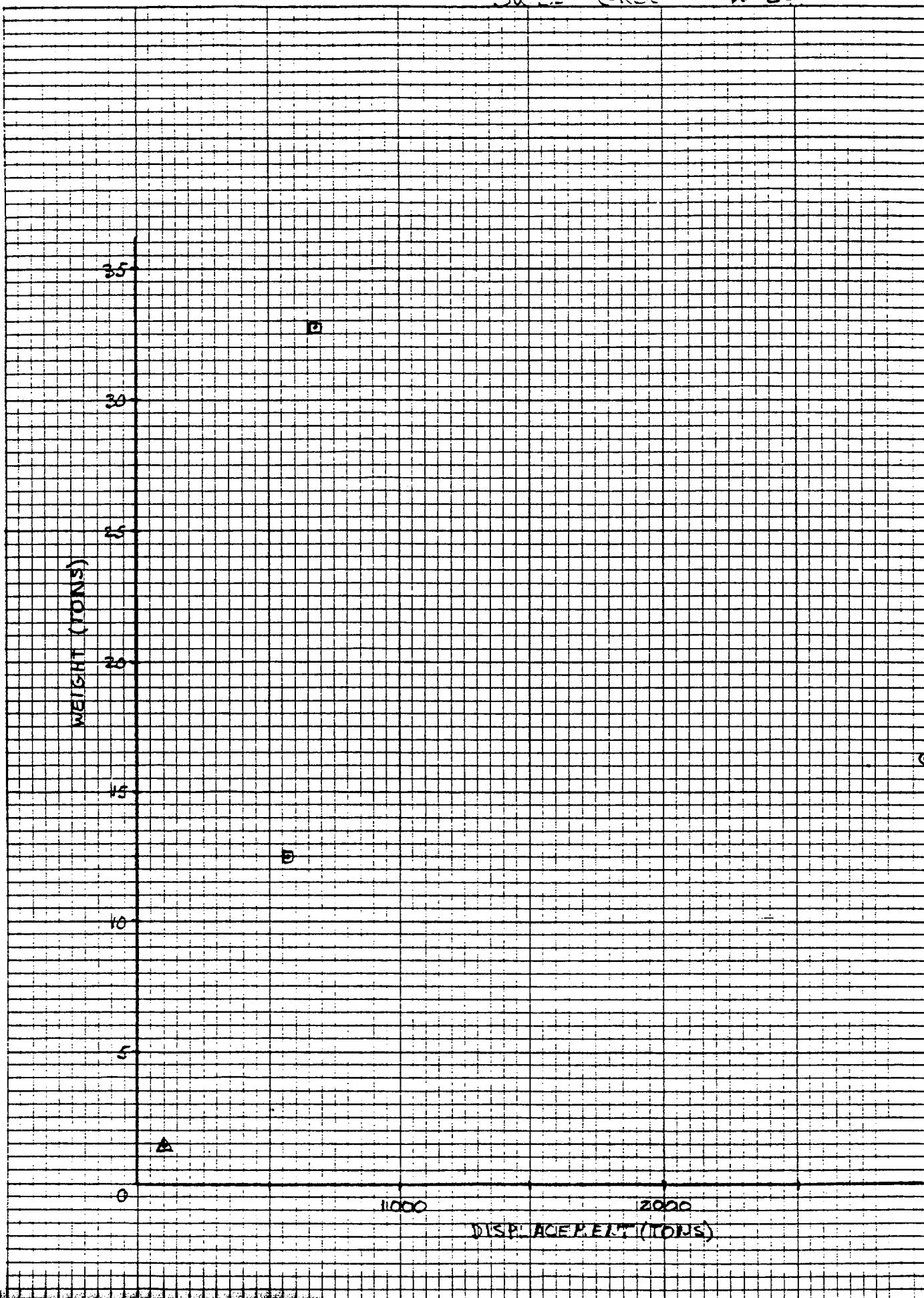
10000

20000

W 241

REDUCTION GEARS

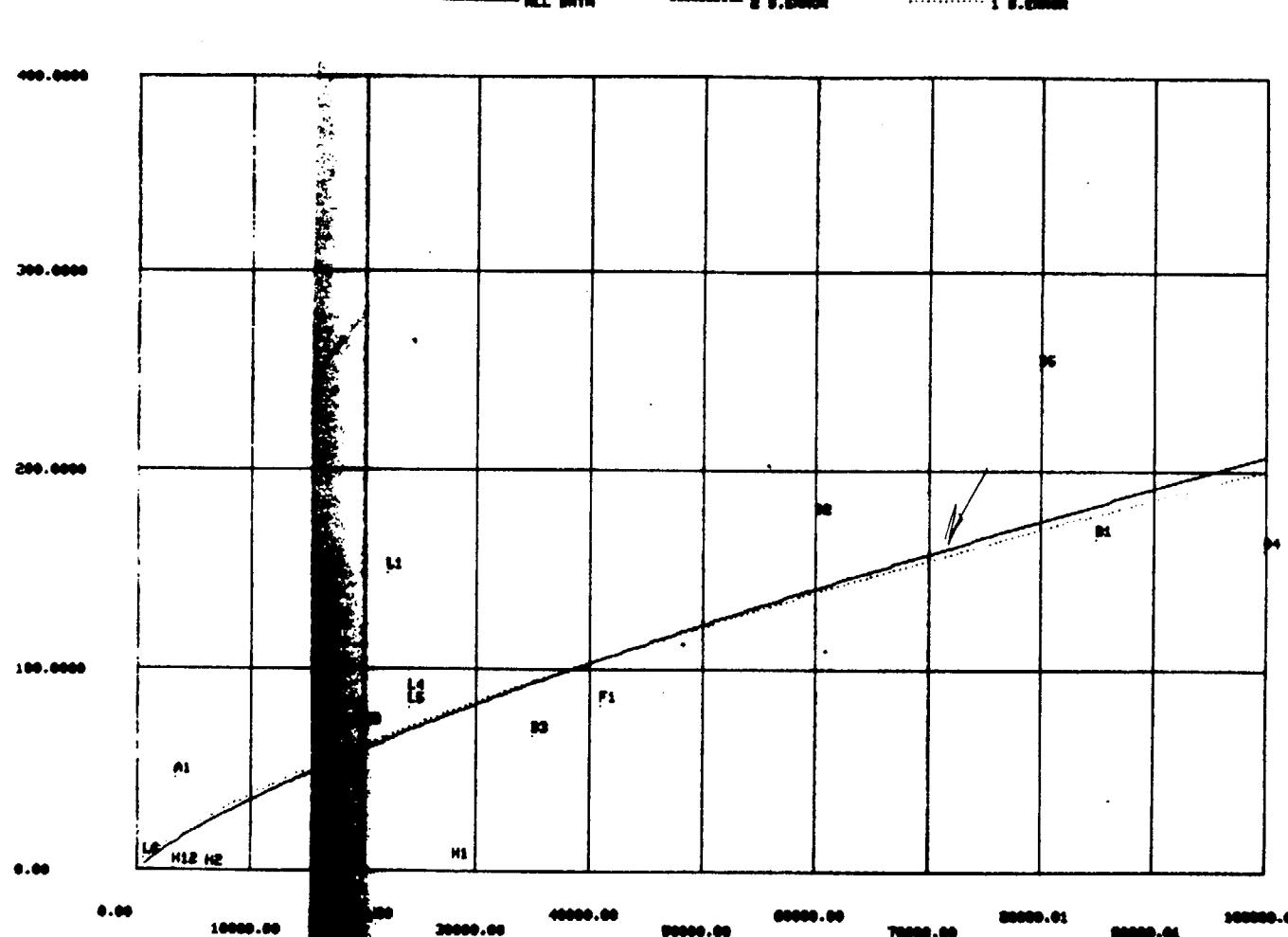
SWEET GROUP W 26'



CONTINUE

## TRANSMISSION AND PROP SYS (243-248) VS SHP

TRANSMISSION AND PROP SYS

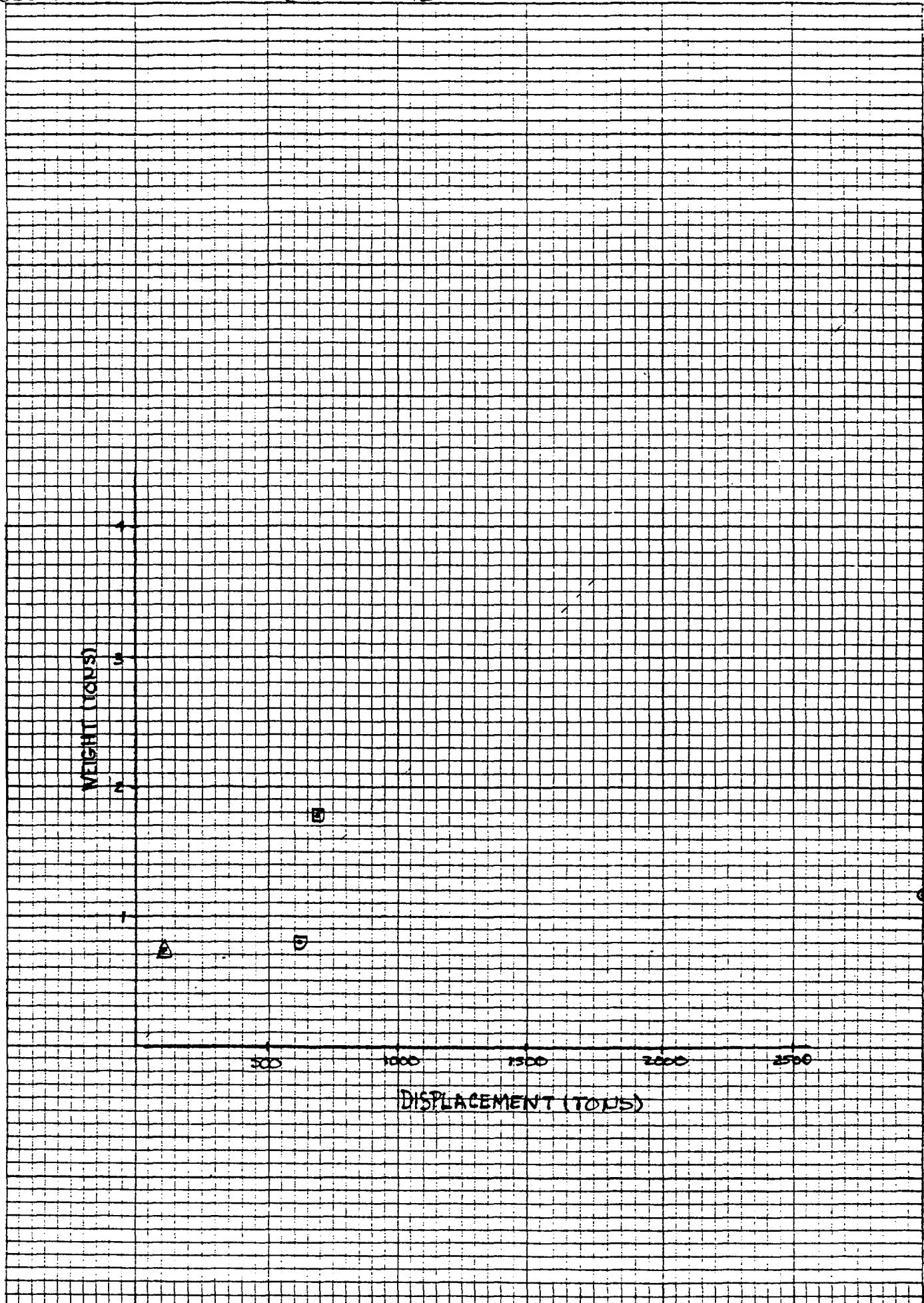


$$W 243 = -2.167 + 0.0261 \cdot e^{-0.12} \quad \text{at}$$

$$= -0.404 + 0.0261 \cdot e^{-0.12}$$

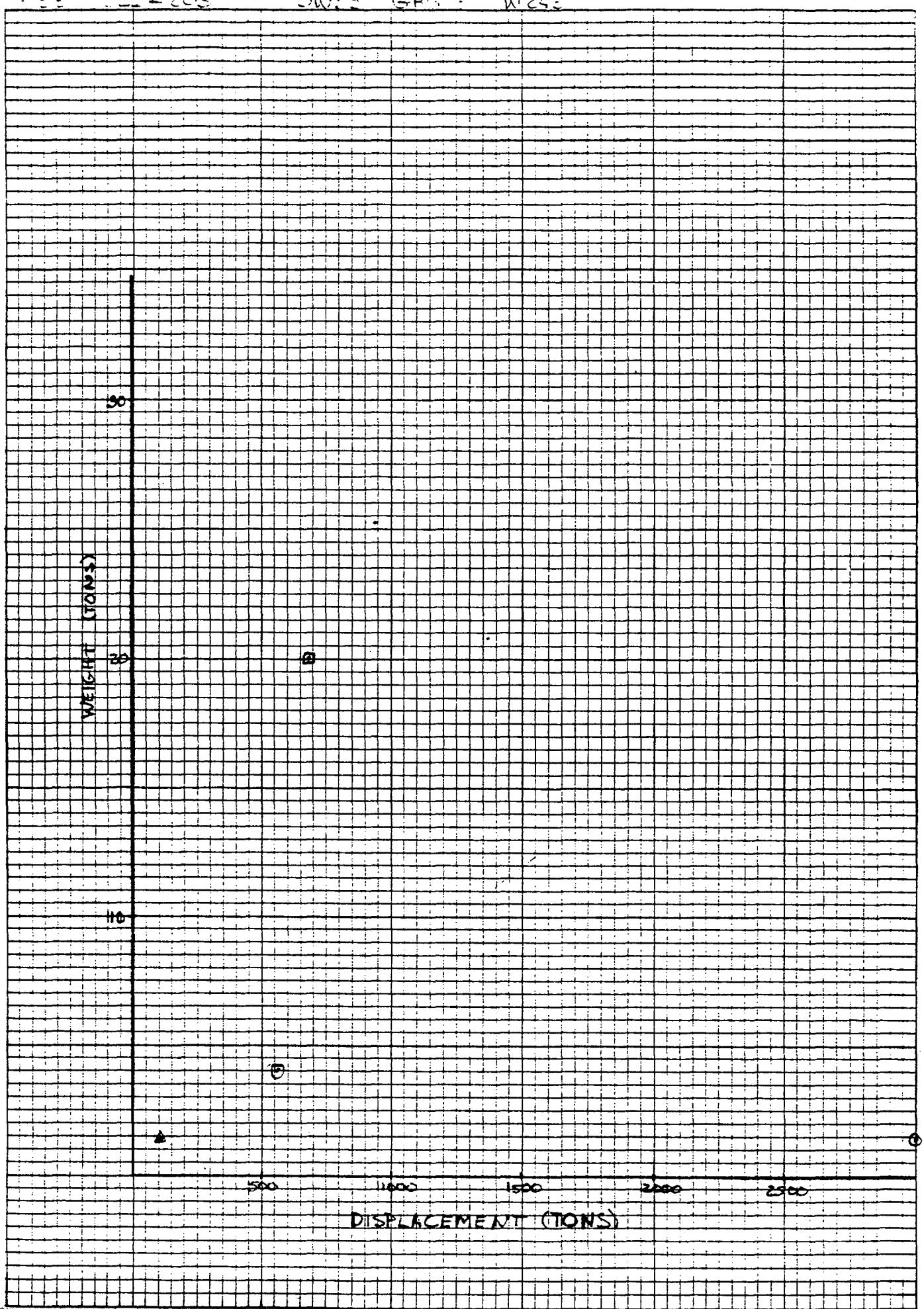
SEE BILL 20 SW - 242

FRAMES 10 X 10 TO 1 INCH  
FOOT LINE HEAVY



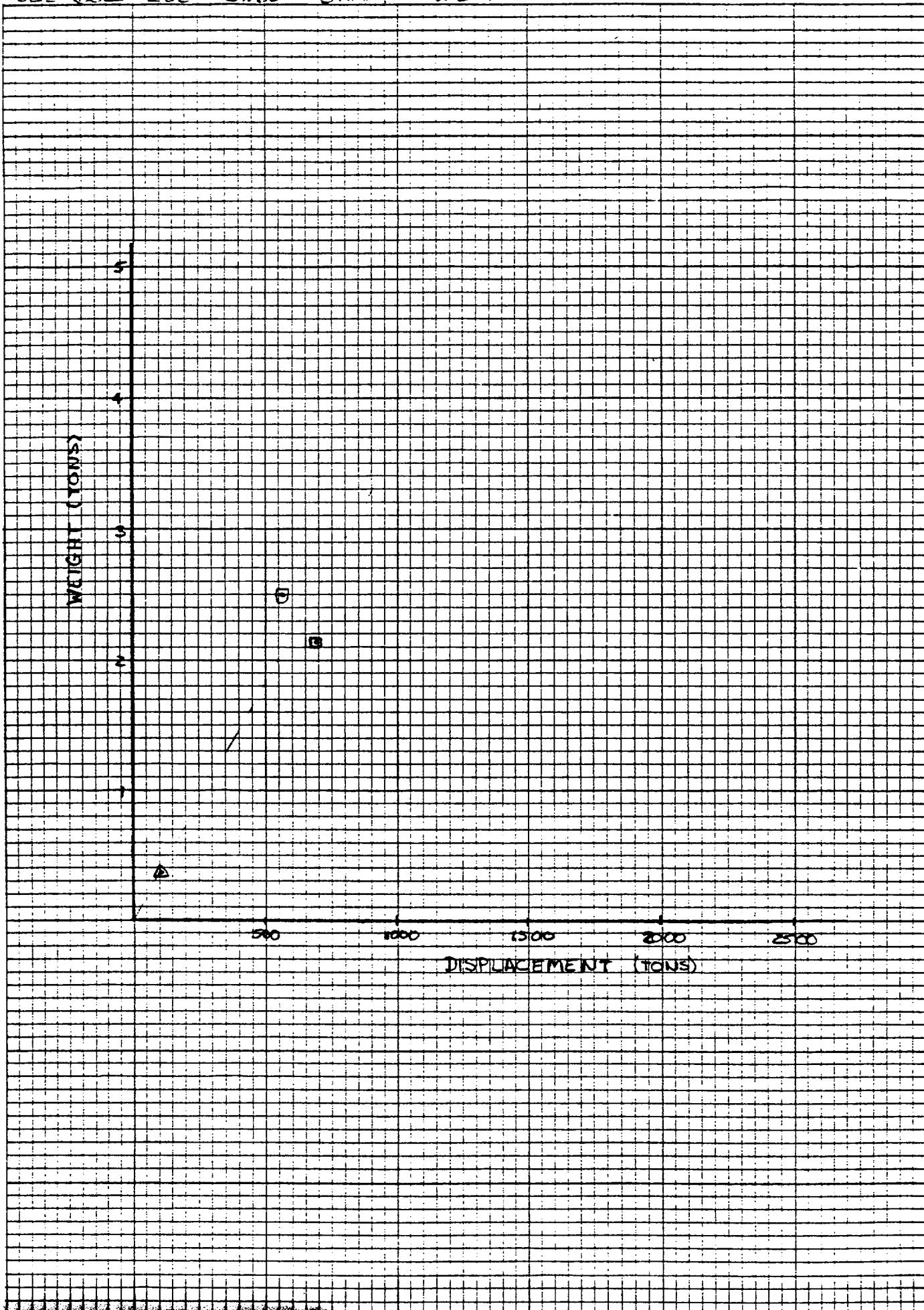
COUPLINGS

STRETCH IN X TO 1 INCH  
WITH THE HEAVY



LAFTING

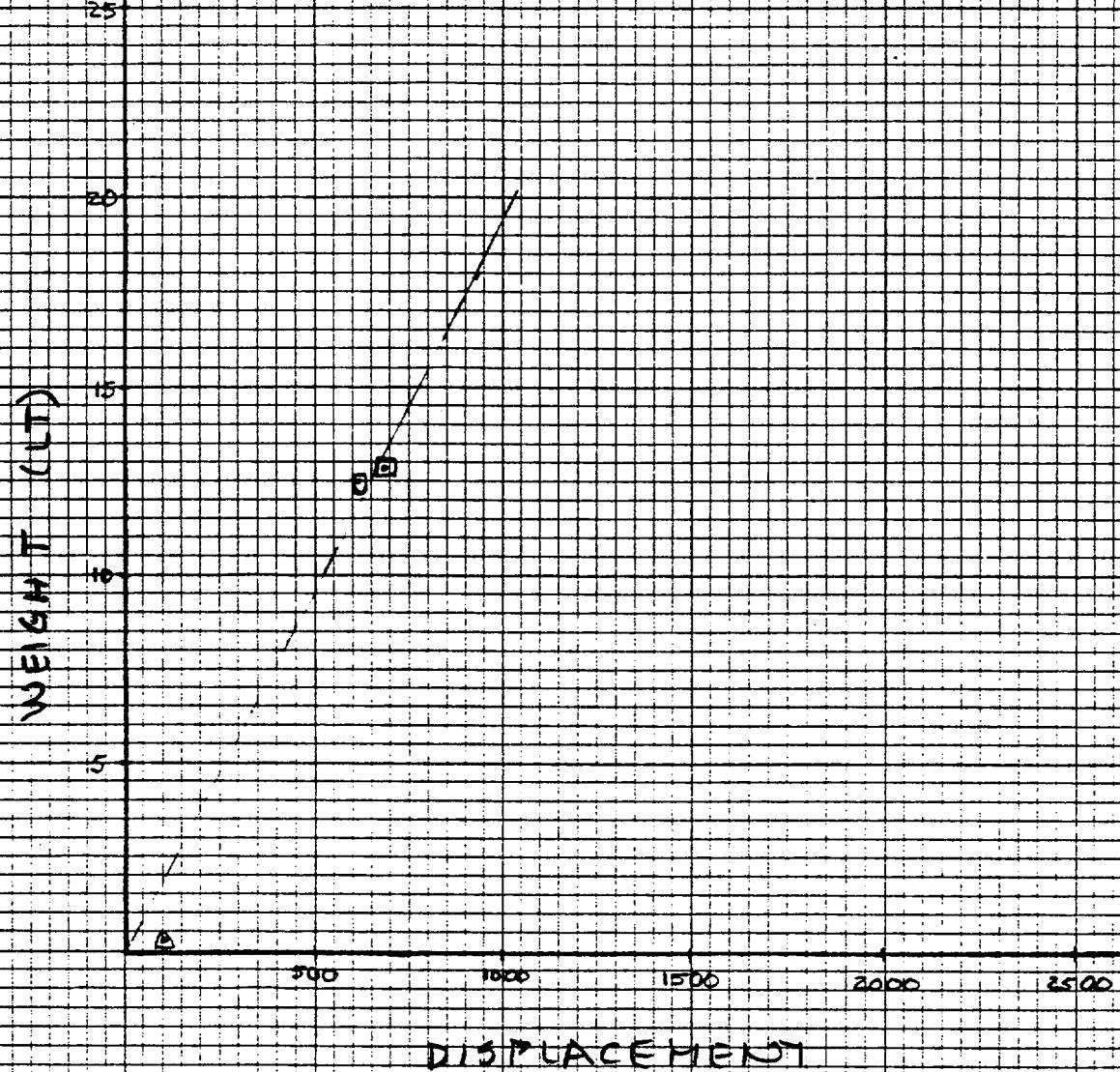
SEE PAGE 203 SWPS GROUP W'24



SHAFT BEARINGS

SEE EC CT # 203

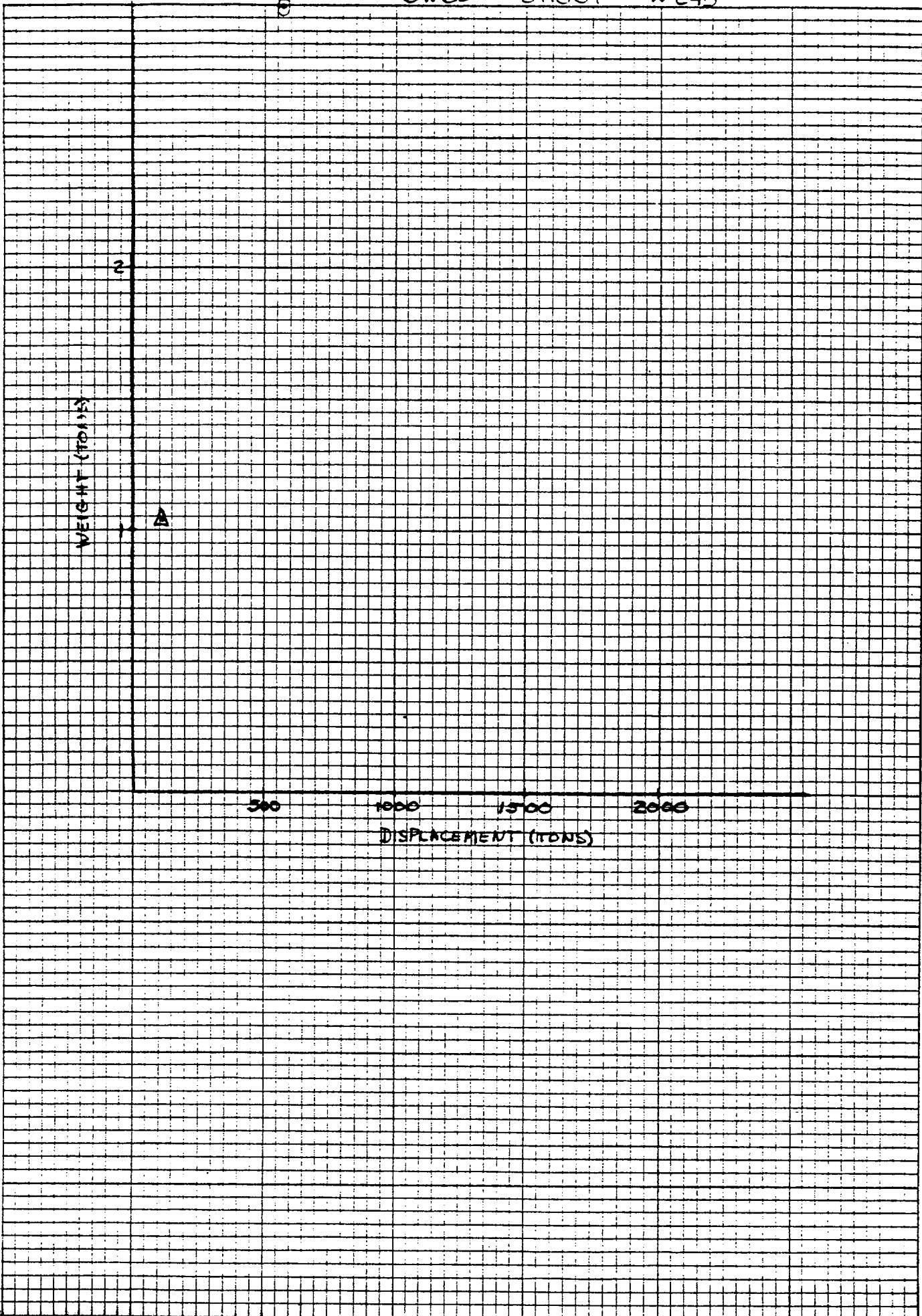
SWEET GROUP W245



OPULATORS

WZ48 LIFT SYSTEM

SWP GROUP WZ45



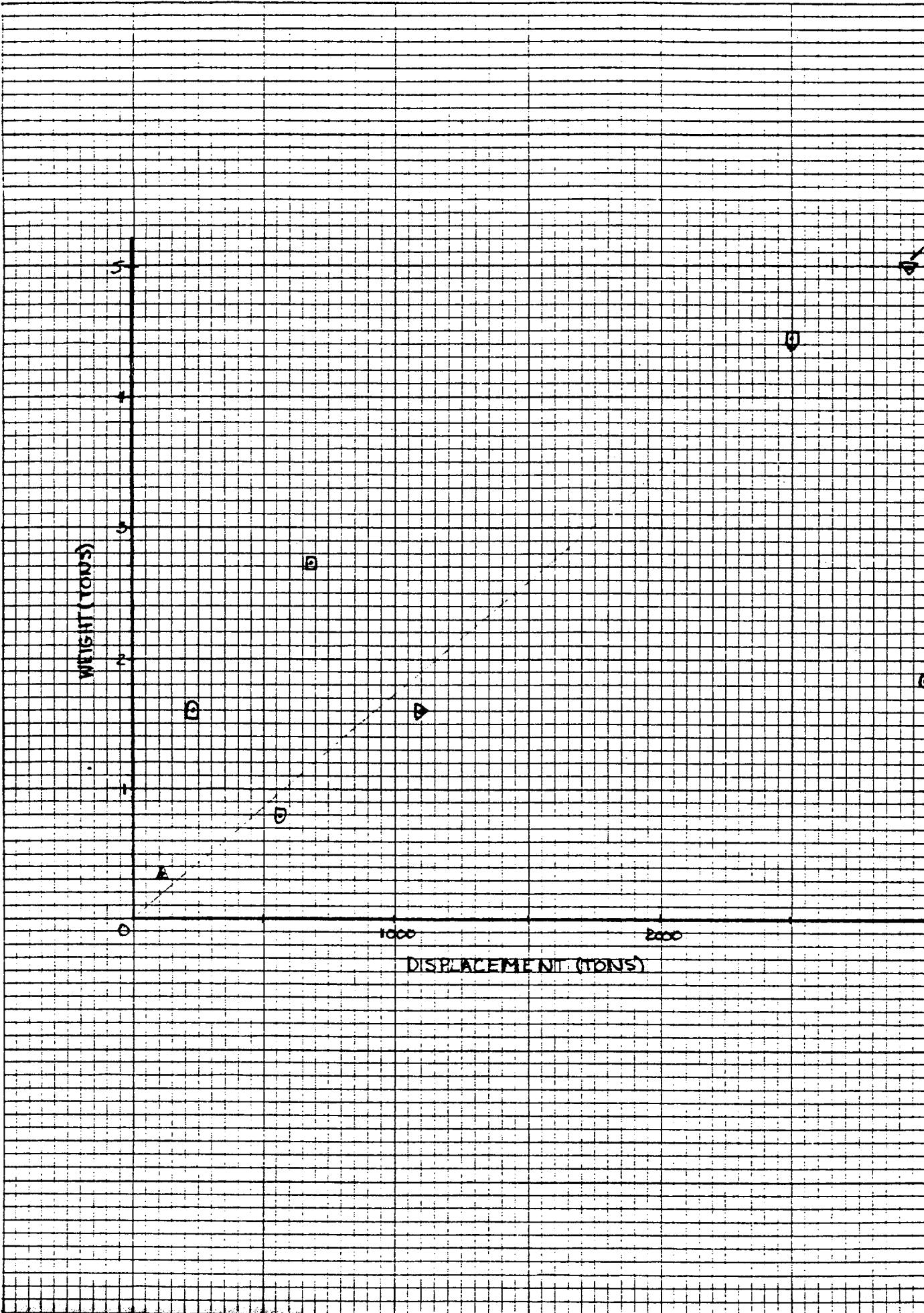
FRACTION IN X 10 TO 1 INCH  
TWIN LINE HEAVY

LIFT SYS

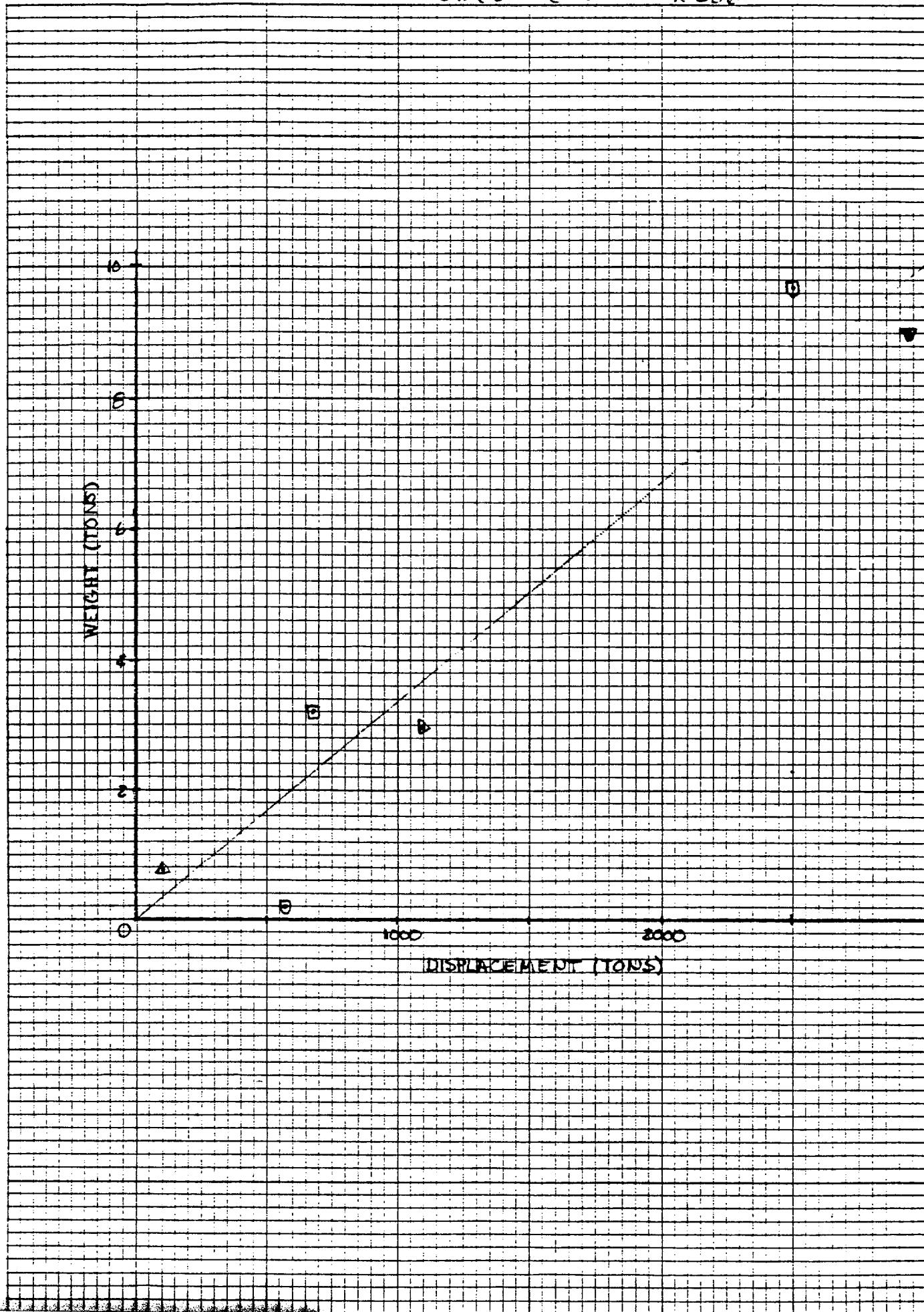
PENNA IN X 10 TO 1 INCH  
10H TIP HEAVY

SWP: G.P. 12 W252

FRONT IN X 10 TO 1 INCH  
INITIAL HEAVY



SWE = 5750 = W 256



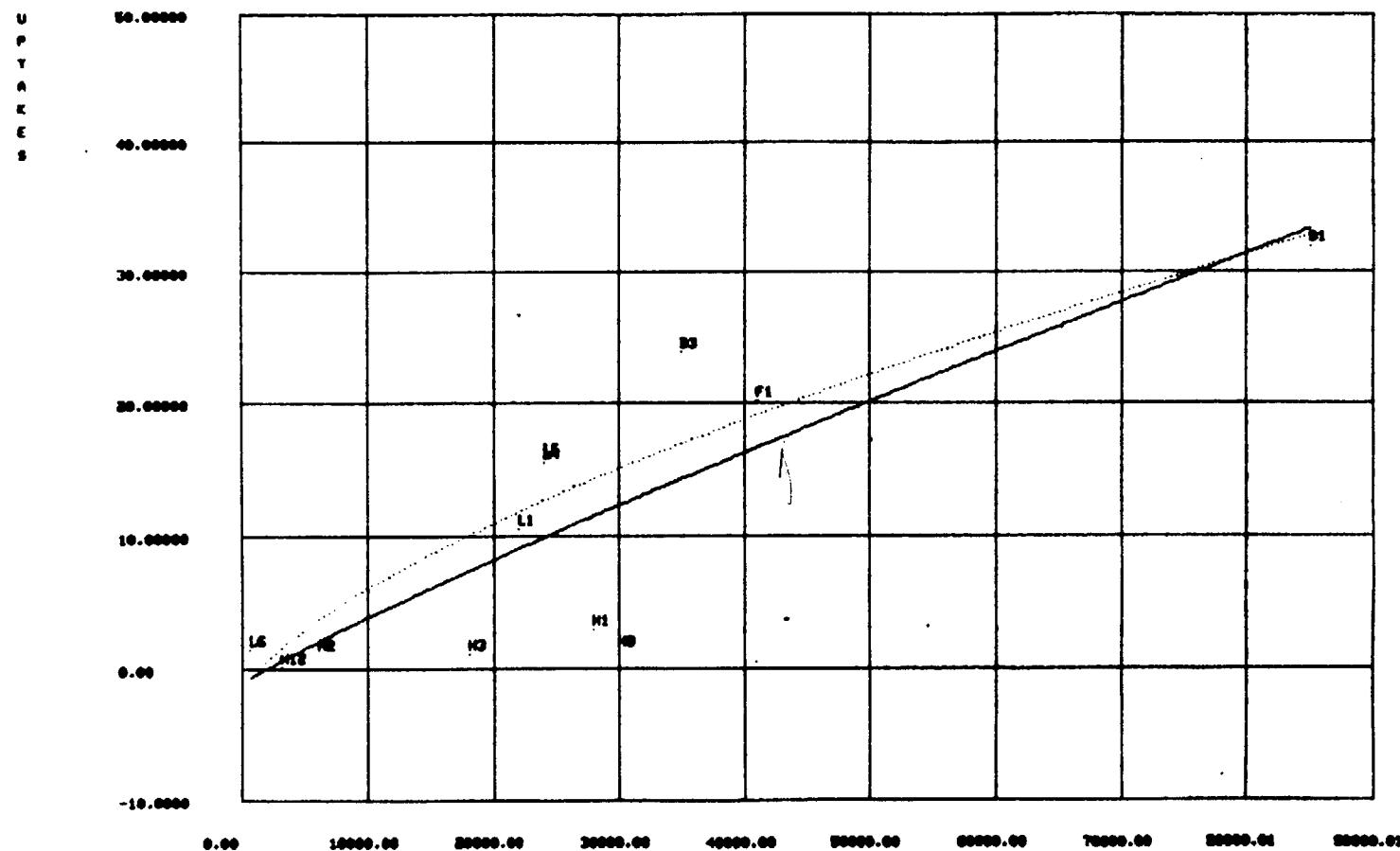
CIRC + COOLING WATER

TO CONTINUE, TYPE CONTINUE

& CONTINUE

UPTAKES (258)

— ALL DATA ————— E.S.ERROR ..... I.S.ERROR

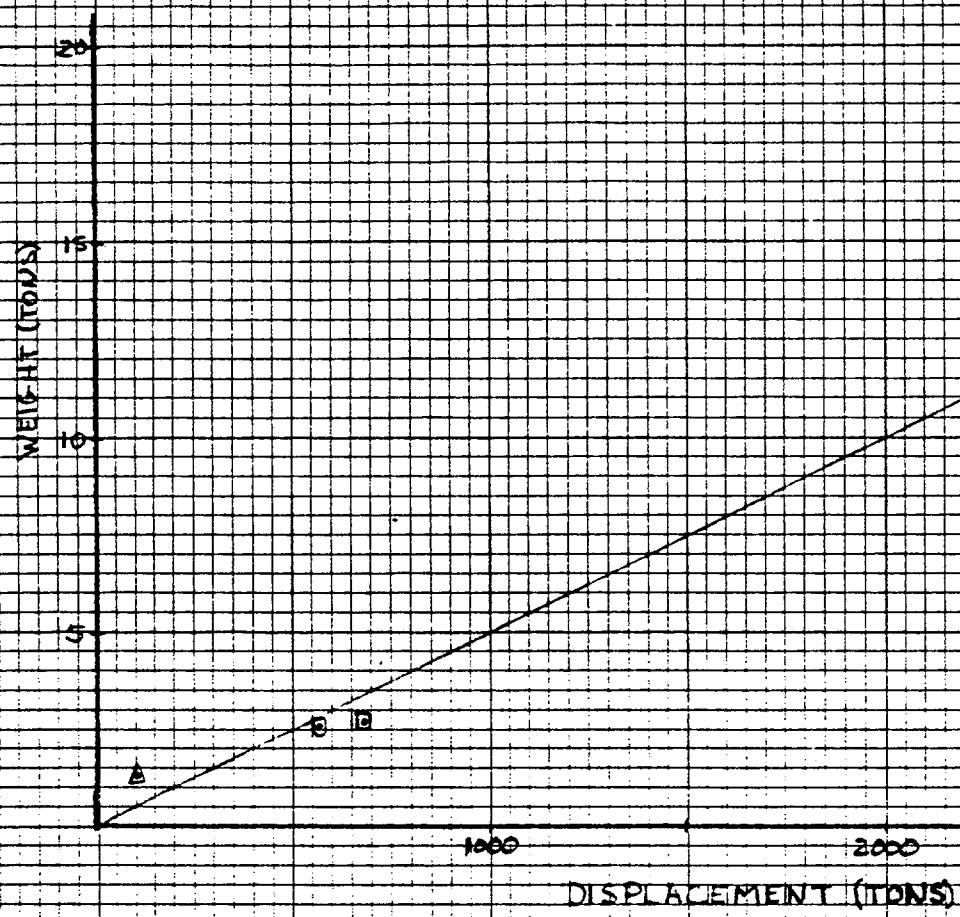


$$W_{258} = -1.126 + 0.20118 \times C_P$$

S.D. =  $\sqrt{(\sum (Y_i - W_{258})^2) / n}$

SEE PAGE 2 OF

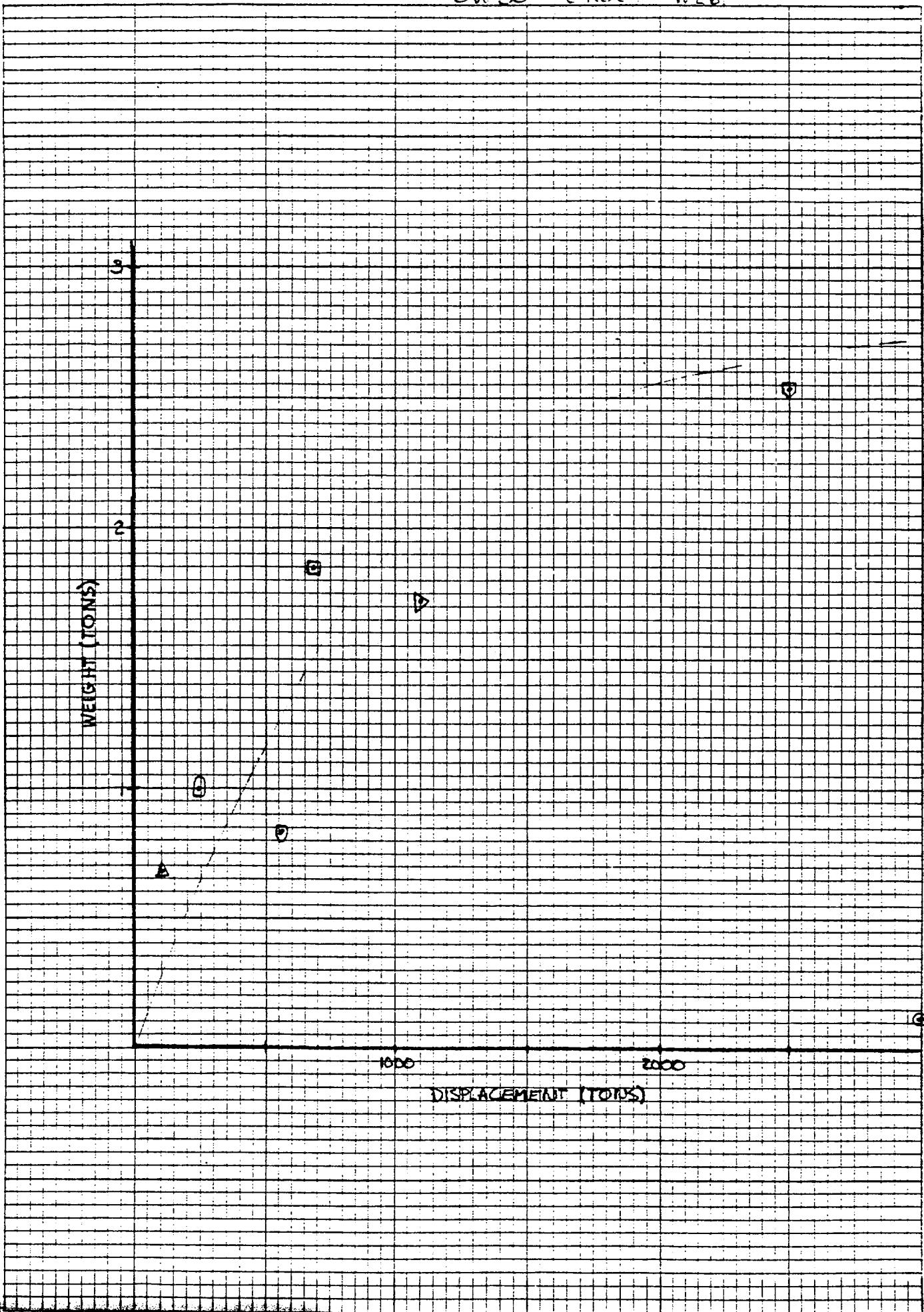
SWPL GF 201F W 25°



UPTAKES

SWES GROUP W26

TRIOMA TO 10 TO 1 RATIO  
THIN LINE HEAVY



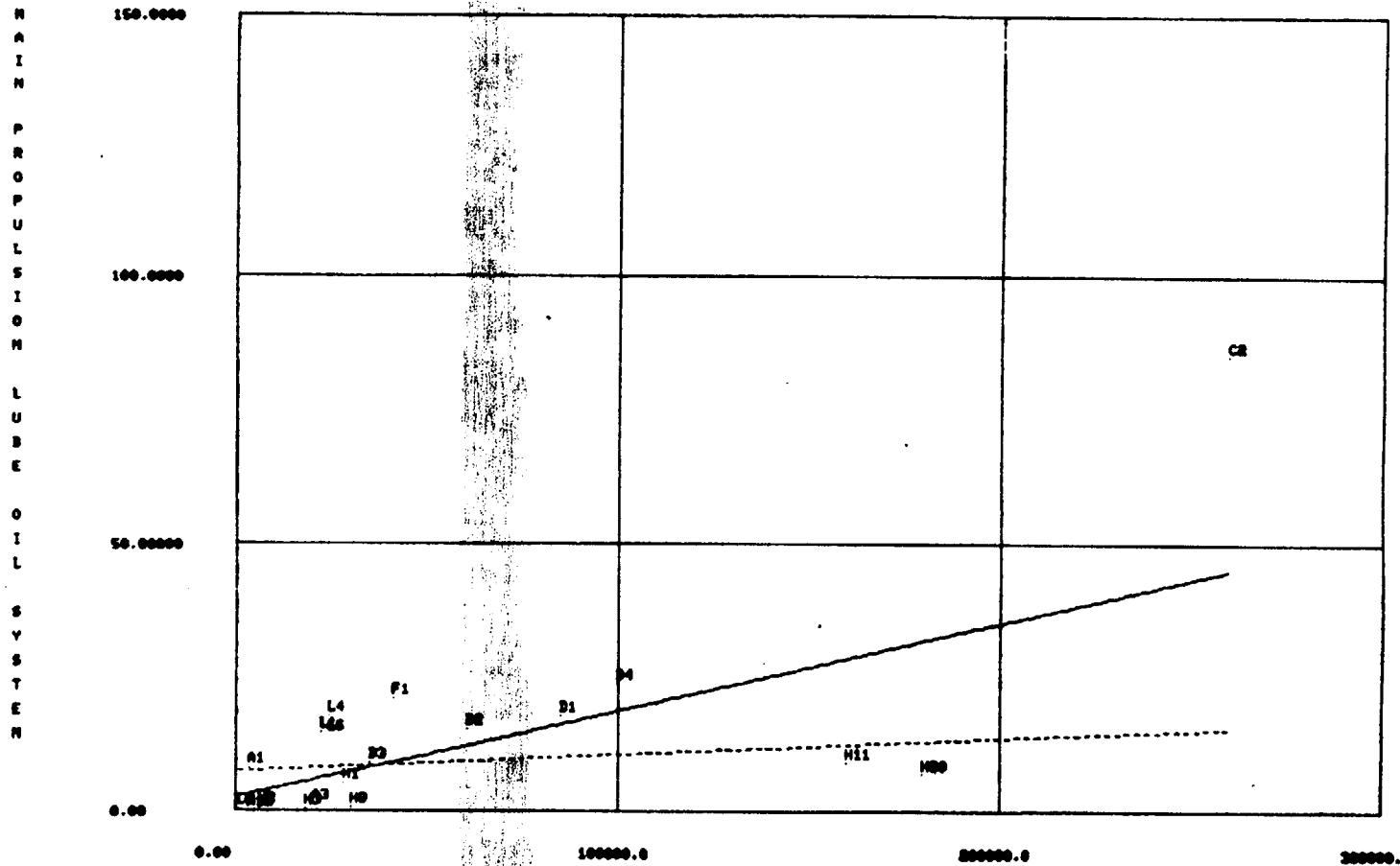
DEL SERVICE SYS

TO CONTINUE, TYPE CONTINUE

© CONTINUE

MAIN PROPULSION LUBE OIL SYSTEM (868-864)

— ALL DATA ————— B.S. ERROR ..... I.S. ERROR



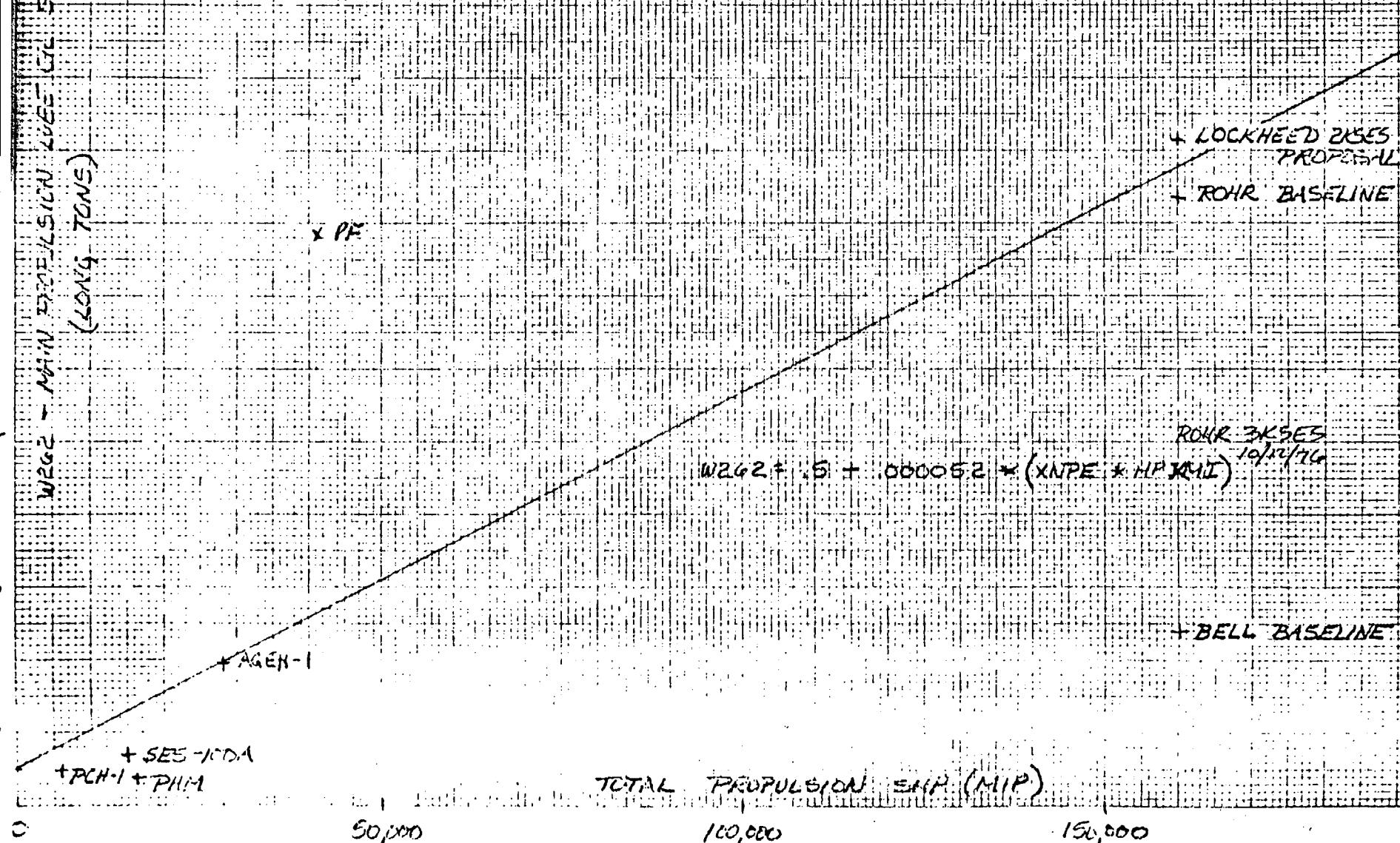
W = 2.72 + 0.000143 CLP

R<sup>2</sup> = 0.000035 - 244

Fig. 9

W262 - MAIN PROPULSION AUGER SYSTEM

REPRODUCED BY GOVERNMENT  
8-12-74  
7  
6  
5  
4  
3  
2  
1  
W262 - MAIN PROPULSION SYSTEM



SWBS ERATE WZ62

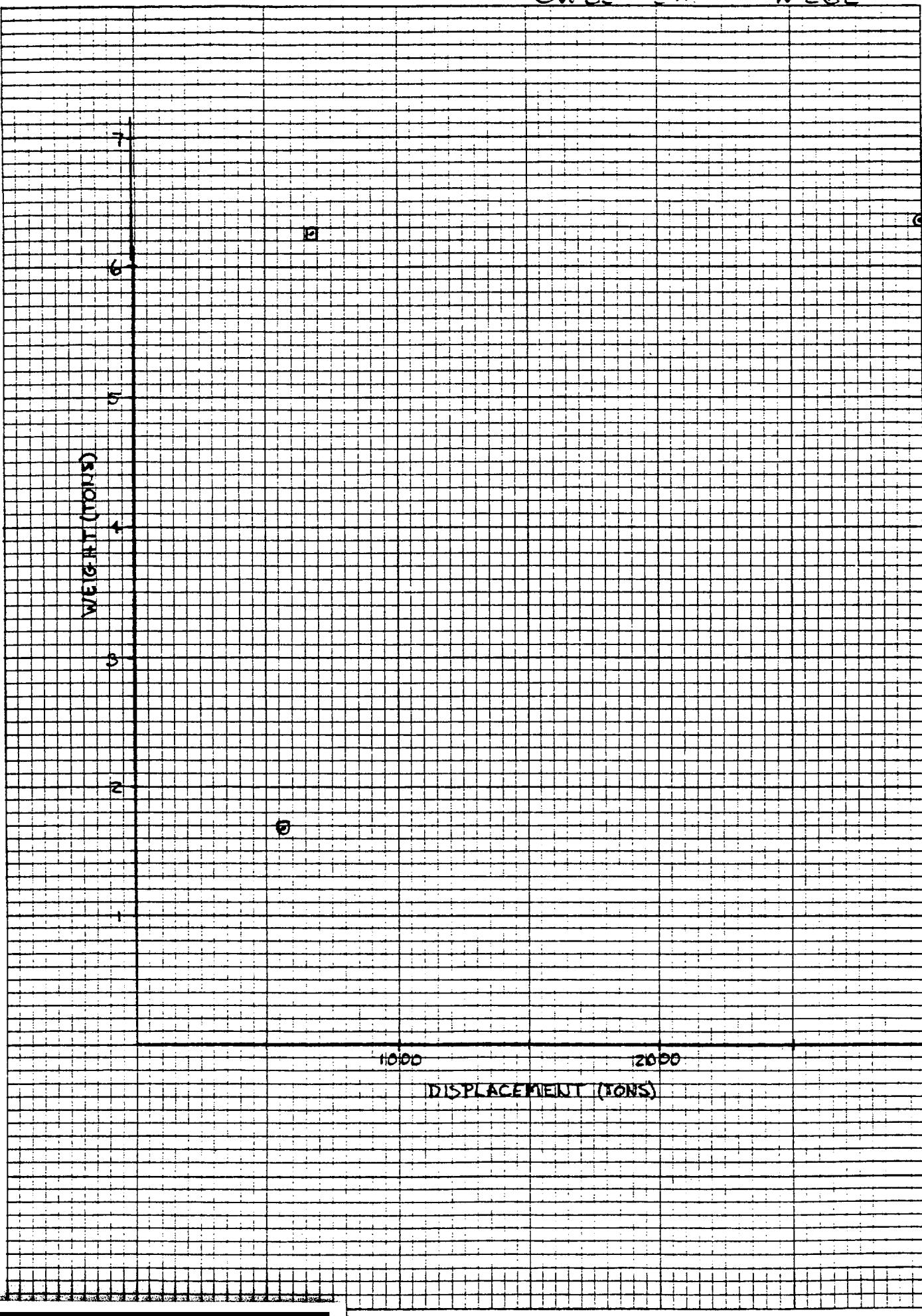
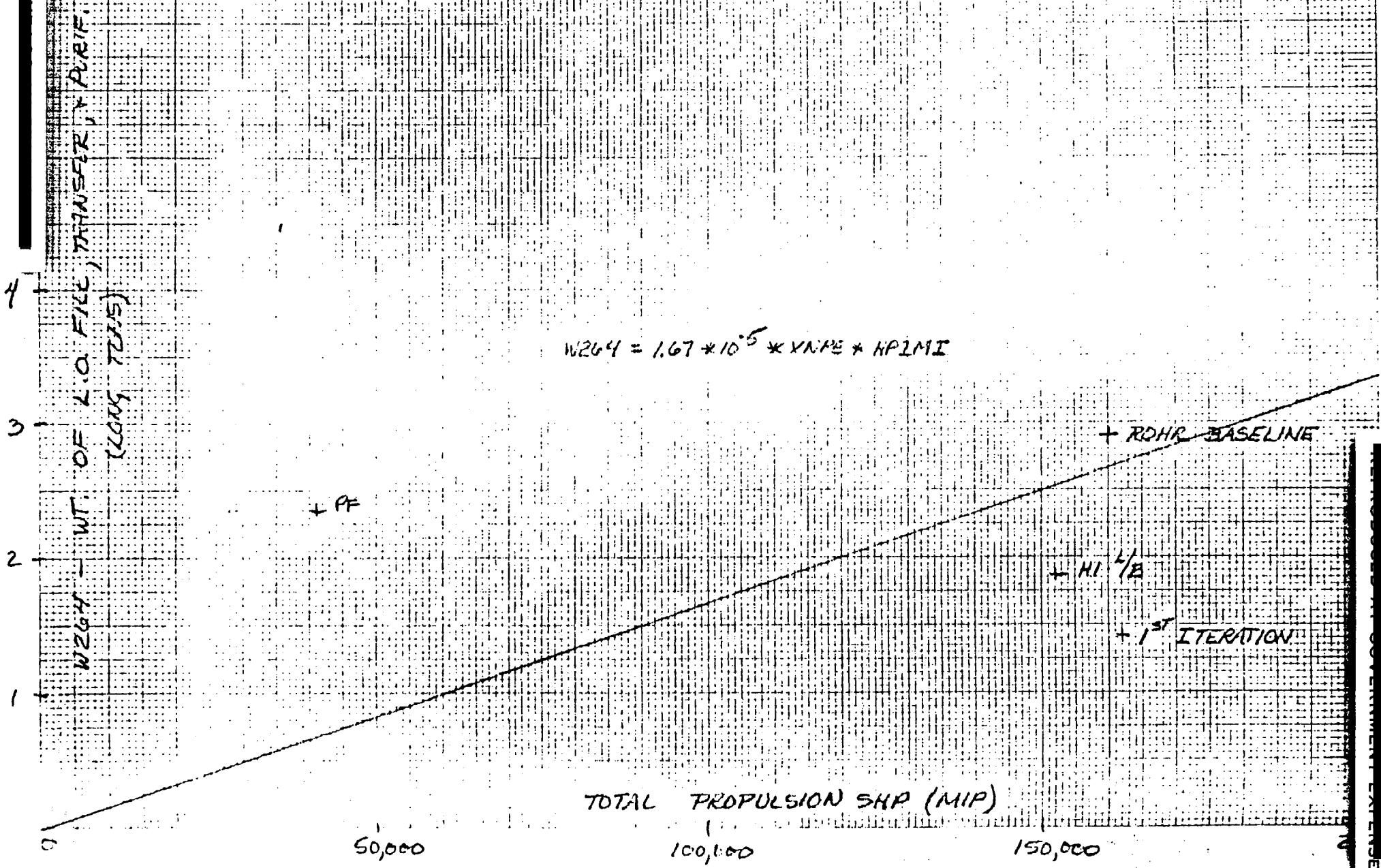
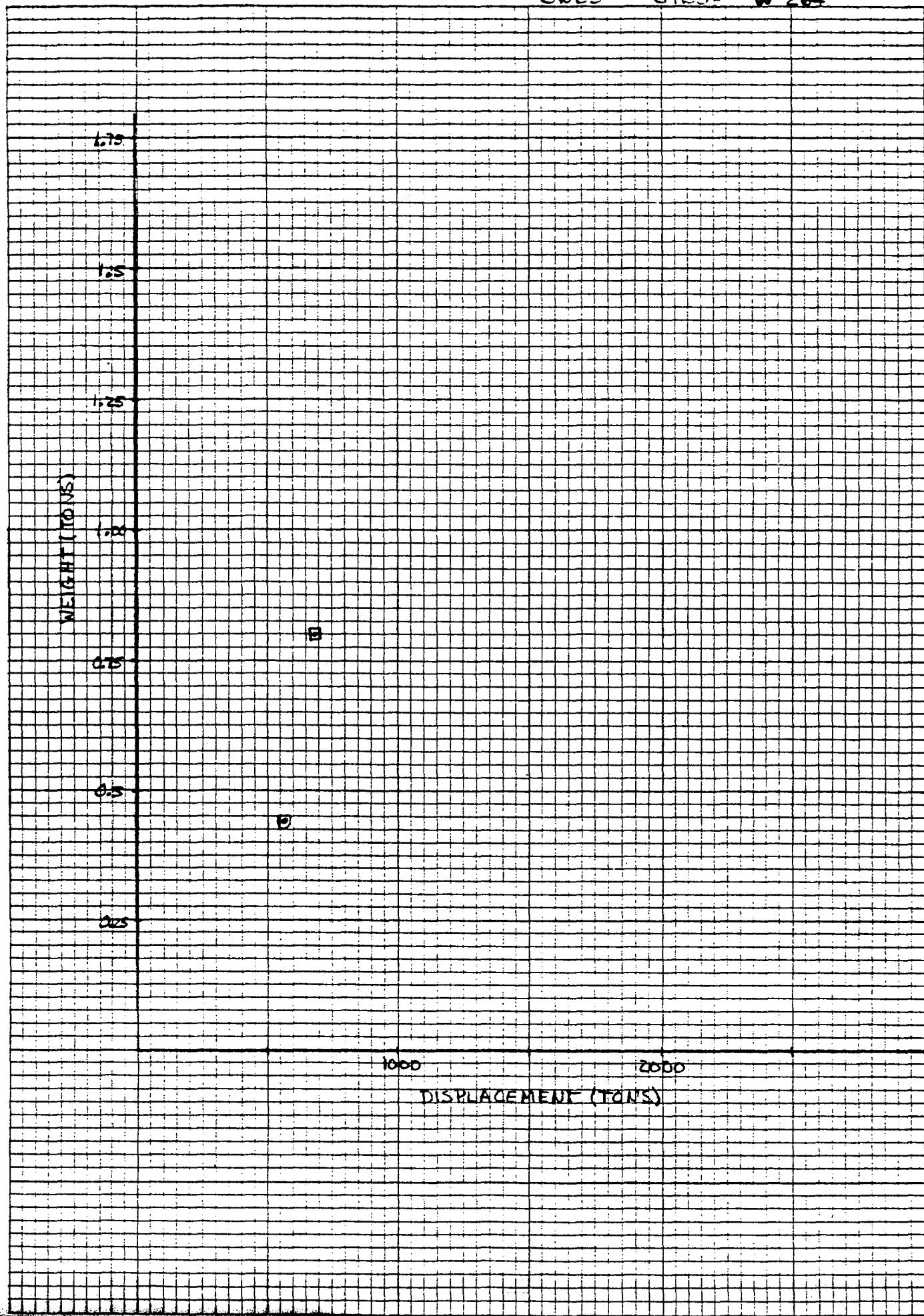


Fig. 10

W264 - L.O. FILL, TRANSFER, & PURIF. SYSTEM





#### **TO COTTON. WE SAY YES!**

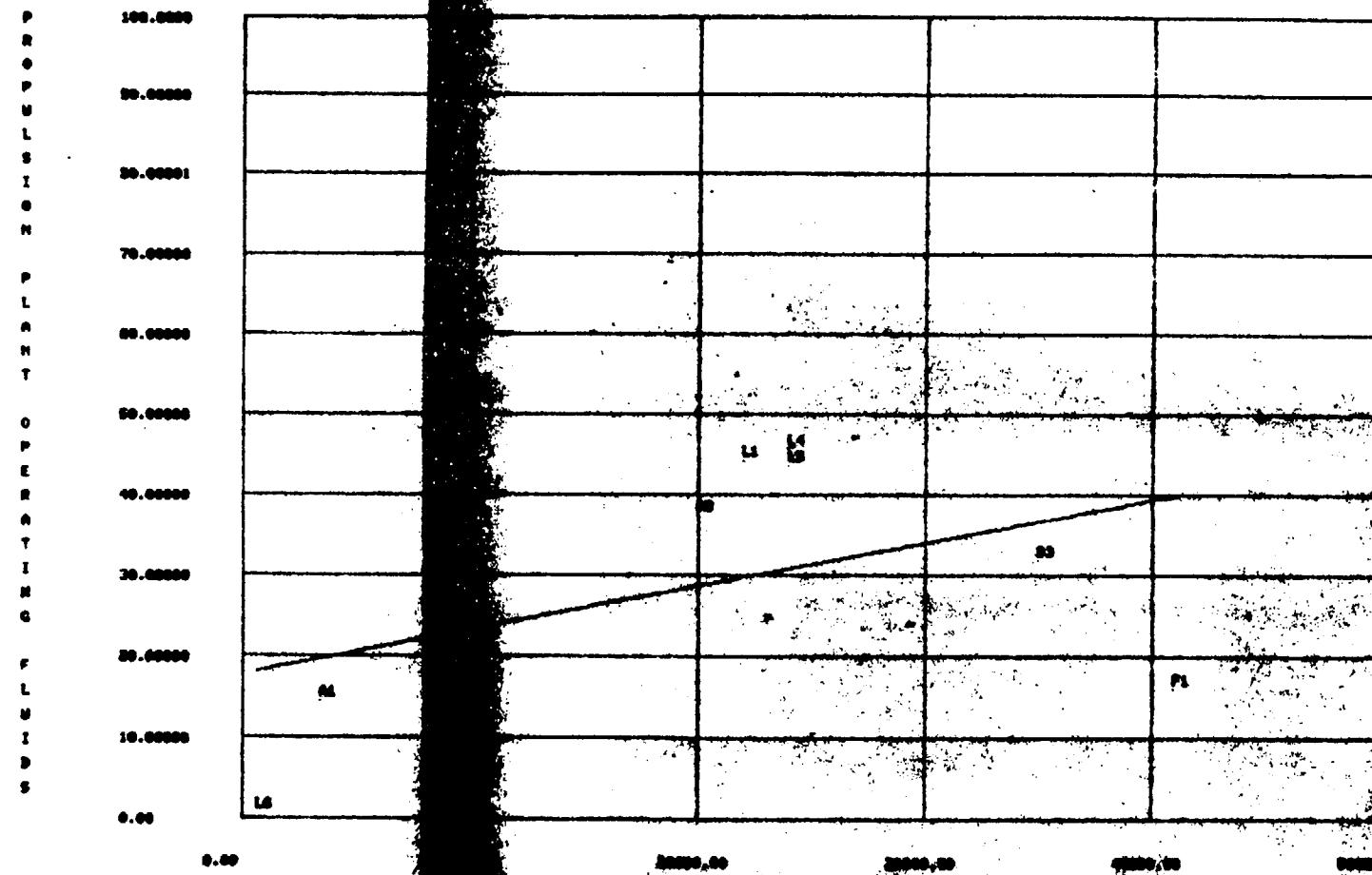
• 800

## PROPULSION PLANTS - FLOWING FLUIDS (200)

— 44 —

— 1 —

.....



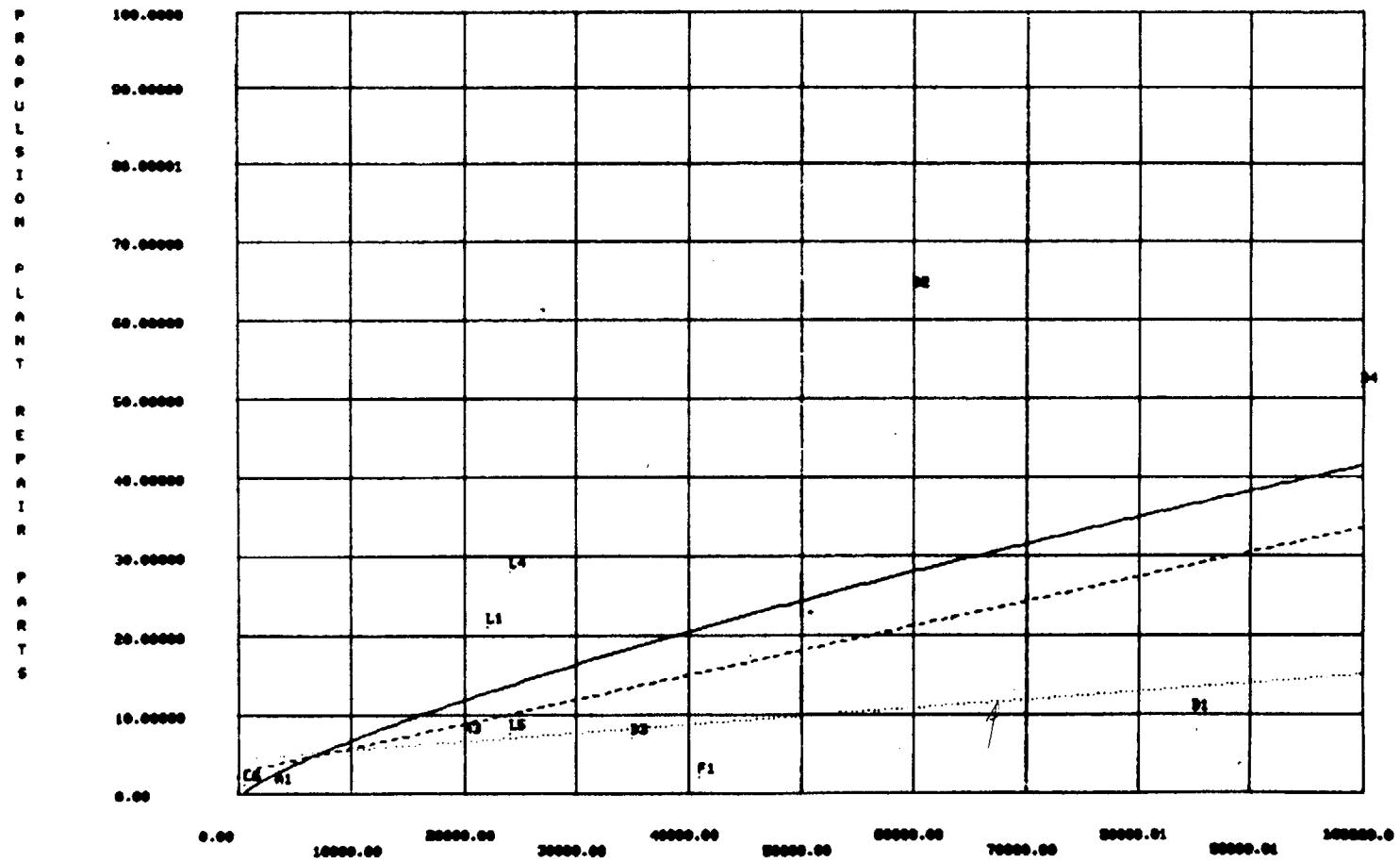
$$V_{2778} = 17.803 + 0.000 \text{mag}$$

TO CONTINUE, TYPE CONTINUE

S CONTINUE

PROPELLION PLANT REPAIR PARTS (899)

— ALL DATA — B S. ERROR — I S. ERROR



WZ99 = -0.614 + 0.001 - 0.4P

2 - 2.941 + 0.0021 - 0.4P

1 - 4.541 + 0.0021 - 0.4P

X  
H1<sup>1/2</sup>B

W279 - PROPULSION PLATE REPAIR PARTS

Fig 11

W279 - PROPULSION PLATE REPAIR PARTS

Pg X

R

2.0

1.0

PLATE

BELL PLATE (BASELINE)

X PF

X ROLL 3K5E5  
10/24/16

(W220 + W240 + W250 + W260)

0

100

200

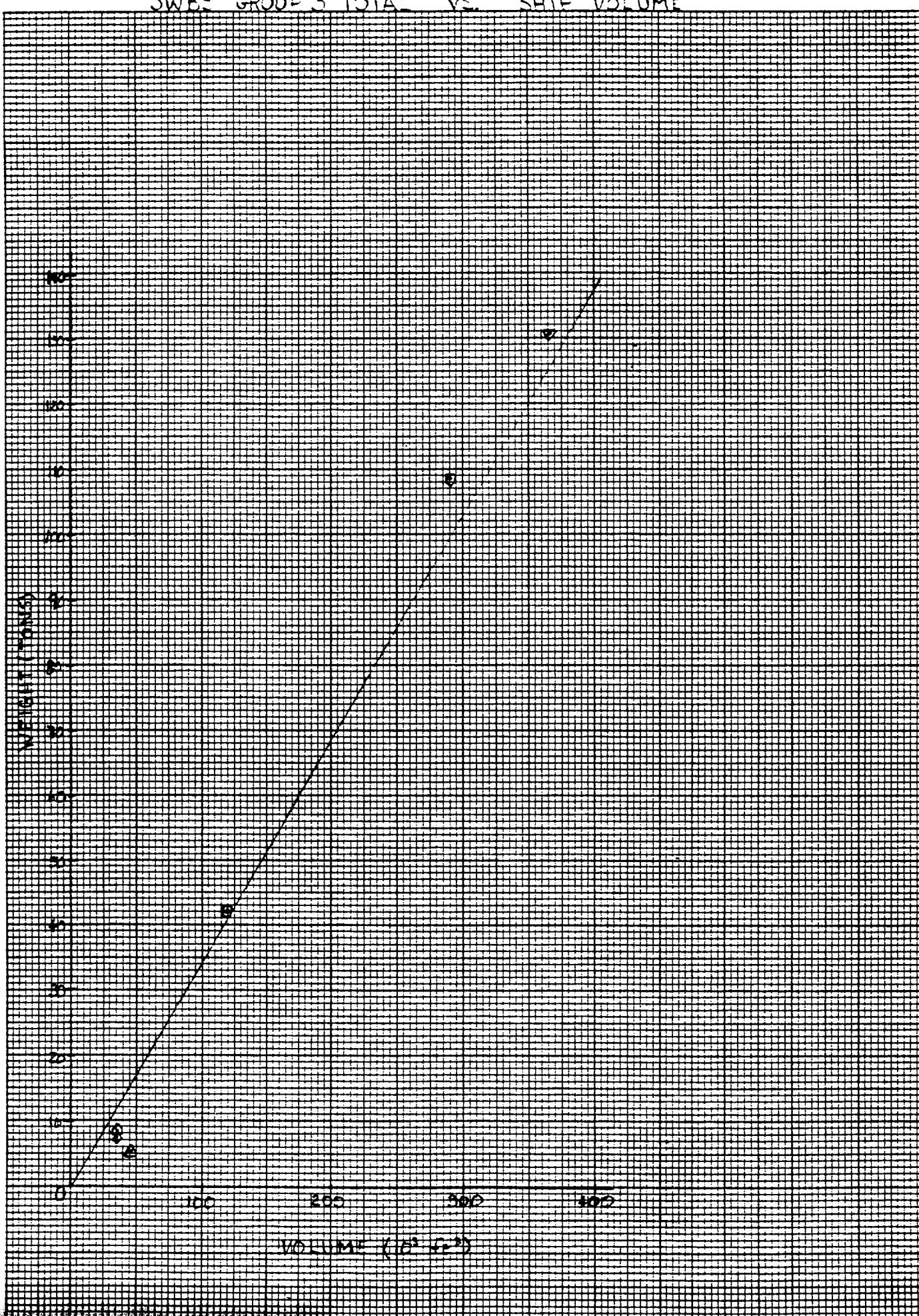
300

400

SE

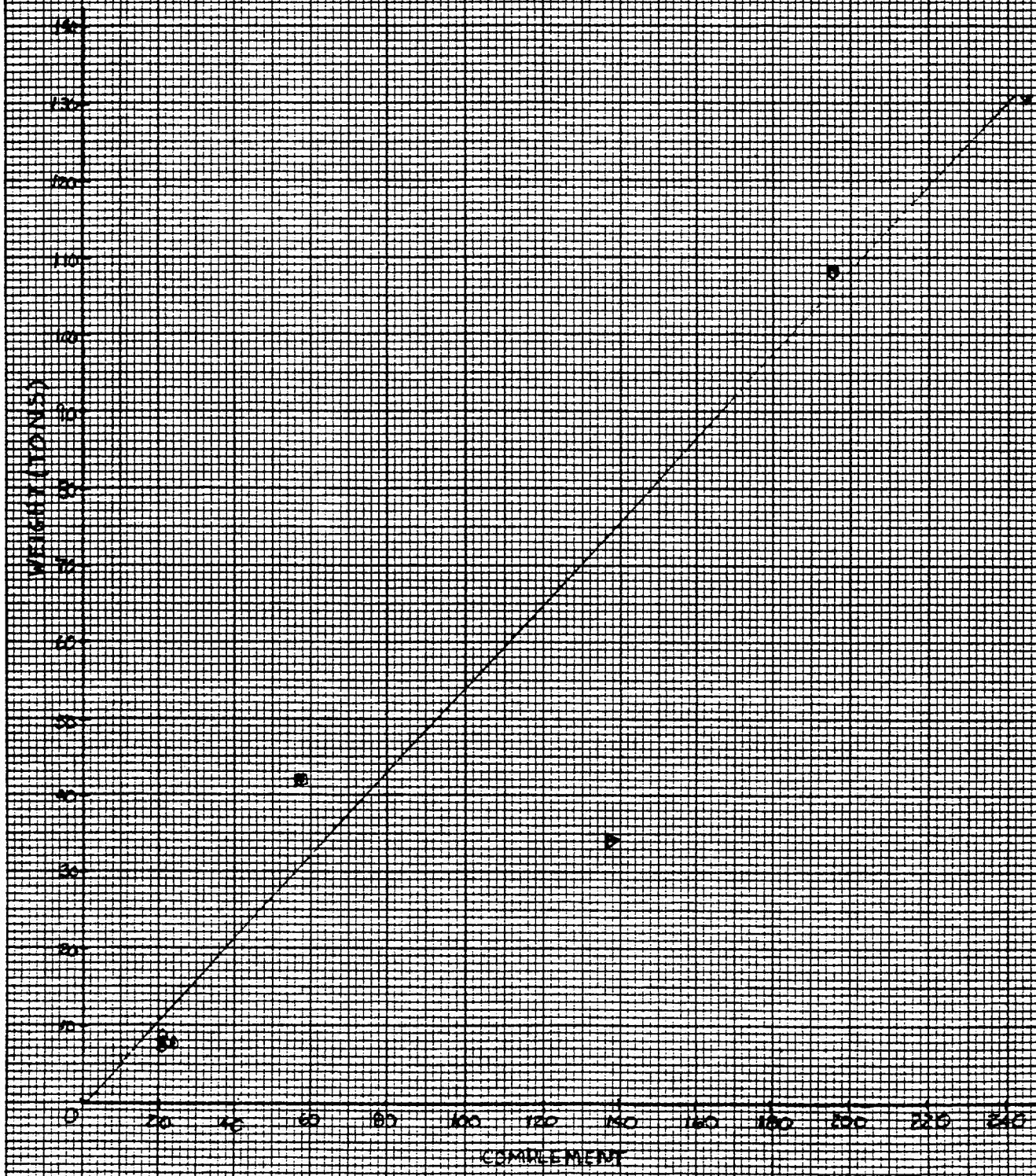
SWBS GROUP 3 TOTAL VS. SHIP VOLUME

FPM AT 20 X 20 TO 1 INCH  
SHIP LENGTH AND BREADTH PROGRESSIVELY ACCENTED



SWES GROUP E TOTAL VS. SHIP'S COMPLEMENT

FPI M1 20 X 20 10.1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED



### 311 Ship Service Power Generation ✓

$$W_{311} = K_{311} \times KW_I$$

where  $K_{311} = .0075 \text{ ft/KW}$

( $K_{311}$  is a constant based on ~~\_\_\_\_\_~~ hydrofoil  
data for gas turbine generators.)

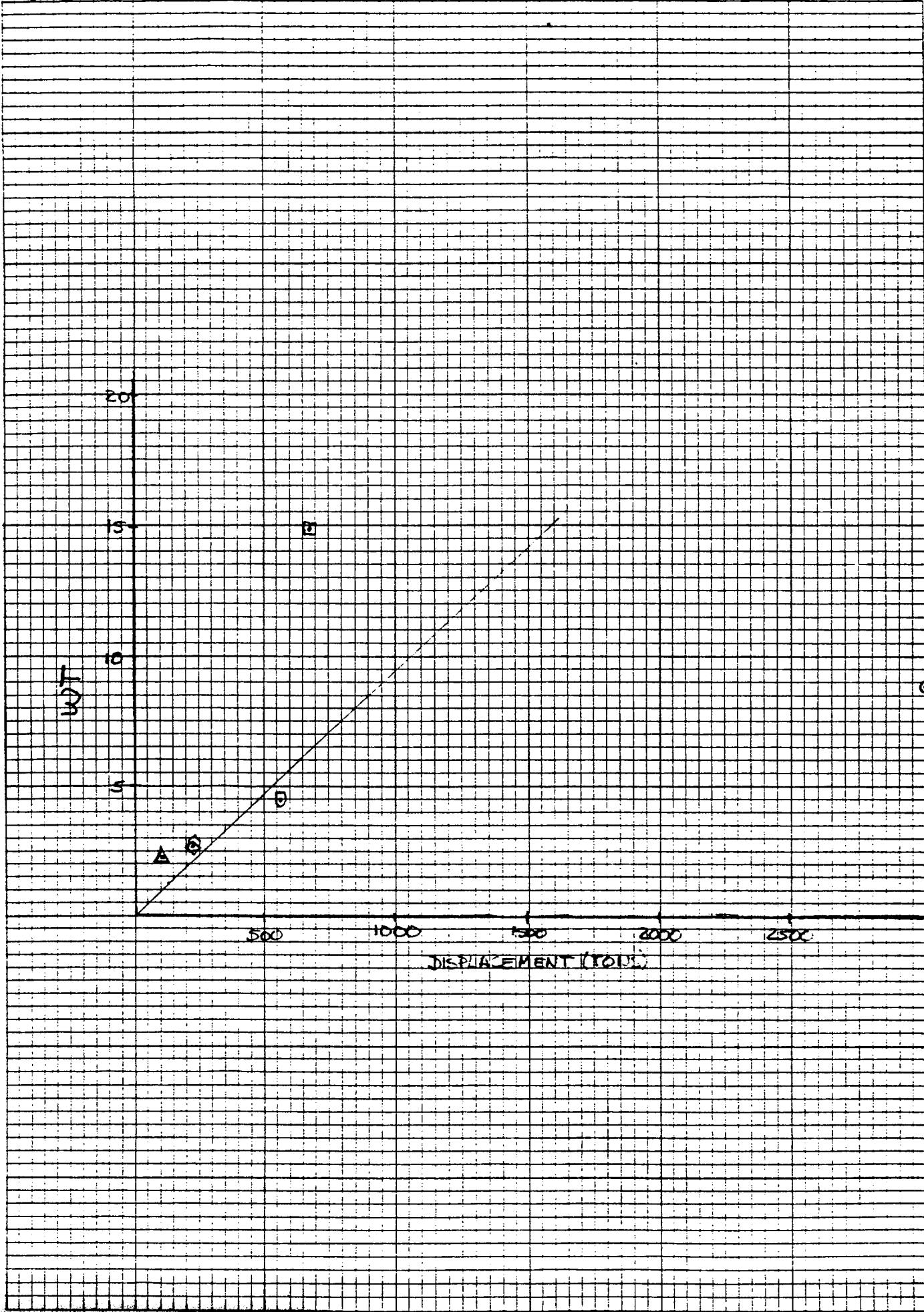
$KW_I$  = Installed KW

Algorithm is the same as ASSET.

SEE ESSCE EOC

SWES GROUP 311

FRONT IN X 10 TO 1 MACH  
INT'L HEAVY



► SERVICE POWER GENERATION

## 313 Bathrooms and Service Facilities

W313 = K313 - KWI

where  $K_{313} = .0003846 \text{ M/kW}$  (ASSET)

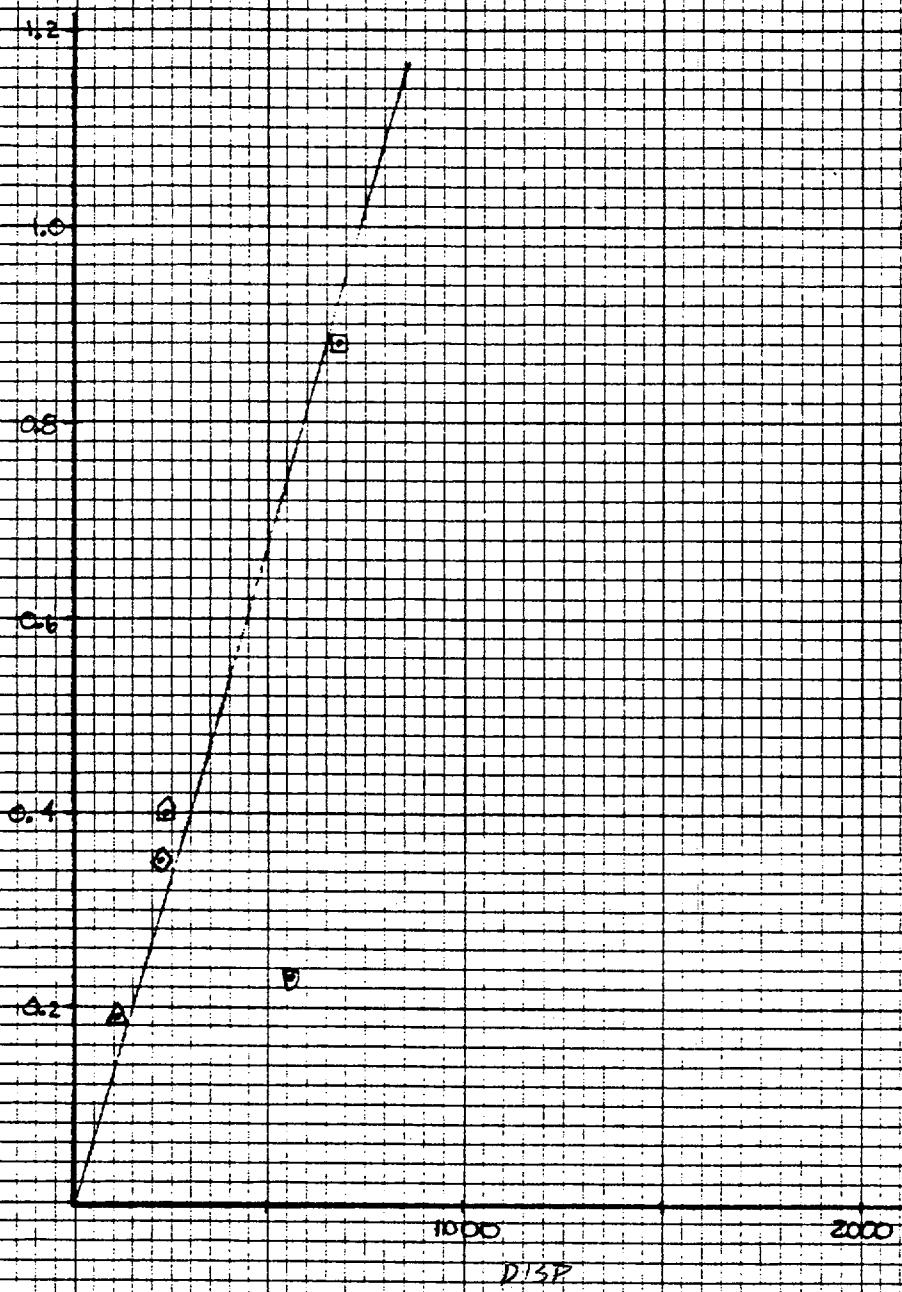
KWI = Installed KW

The Algorithm is also from ASSET.

SEE PAGE 302

SWE GROUT 313

FRONT IN X TO 1 INCH  
10TH TIME HEAVY



### 314 Power Conversion Equipment

$$W_{314} = K_{314} \times KW_I$$

where  $K_{314} = .0024 \text{ ft/KW}$

( $K_{314}$  is a constant based on hydrofoil  
data return data.)

$KW_I$  = Installed KW

~~Then~~

The algorithm is <sup>the same as</sup> based on ASSET.



Fig. 13

WE314 - POWER CONVERSION EQUIPMENT

REPRODUCED BY

WE314 - POWER CONVERSION EQUIPMENT  
(LONG TORS)

4.0

3.0

2.0

1.0

0

50

100

150

$$W314 = 0.315 \times (TE60 + TW60)$$

ROHC 2K-303 (4/10/75)

~~CONVERTER AND ASSOCIATED LOADS~~

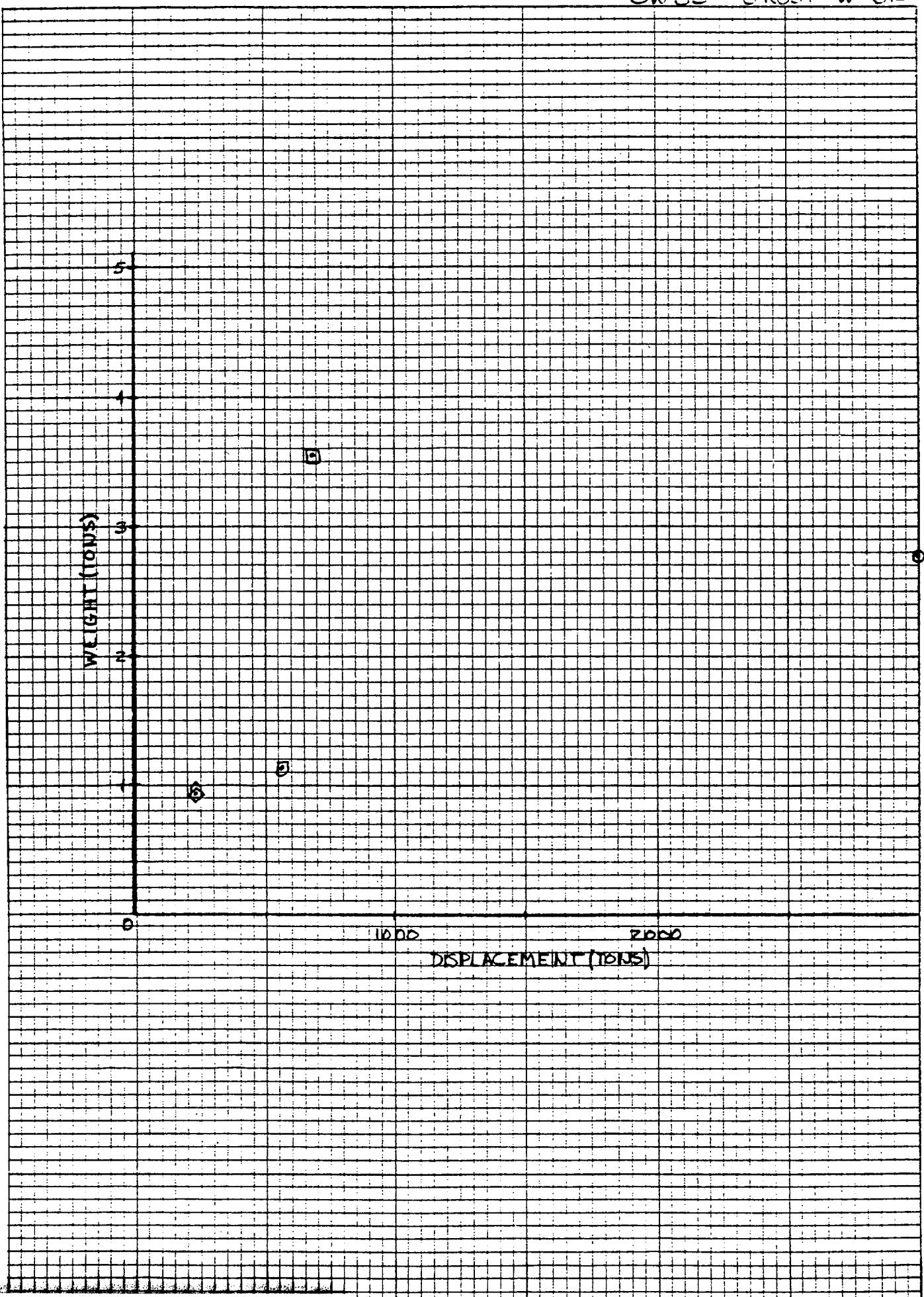
BASES HAS 2.98 L.T.  
TOTAL WE314 (TE412/16)

NOTE: KW FOR CONVERSION MUST TAKE  
INTO ACCOUNT A LOAD FACTOR AND  
CONVERTER EFFICIENCY

$$W314 = .0135 \times (TE400 + TW400)$$

KW FOR CONVERS. N.

.0244 X 10<sup>-3</sup>



### 321 Ship Service Power Cable ✓

$$W_{321} = K_{321} \cdot KW_I + L_{321} \cdot VOL_A$$

where  $K_{321} = .0034 \text{ ft}/\text{kW}$  +  $L_{321} = .0123 \text{ ft}/\text{ft}^3$

(These constants are based on return data from Hydrofoils and SESs.)

$KW_I$  = Installed KW, kW

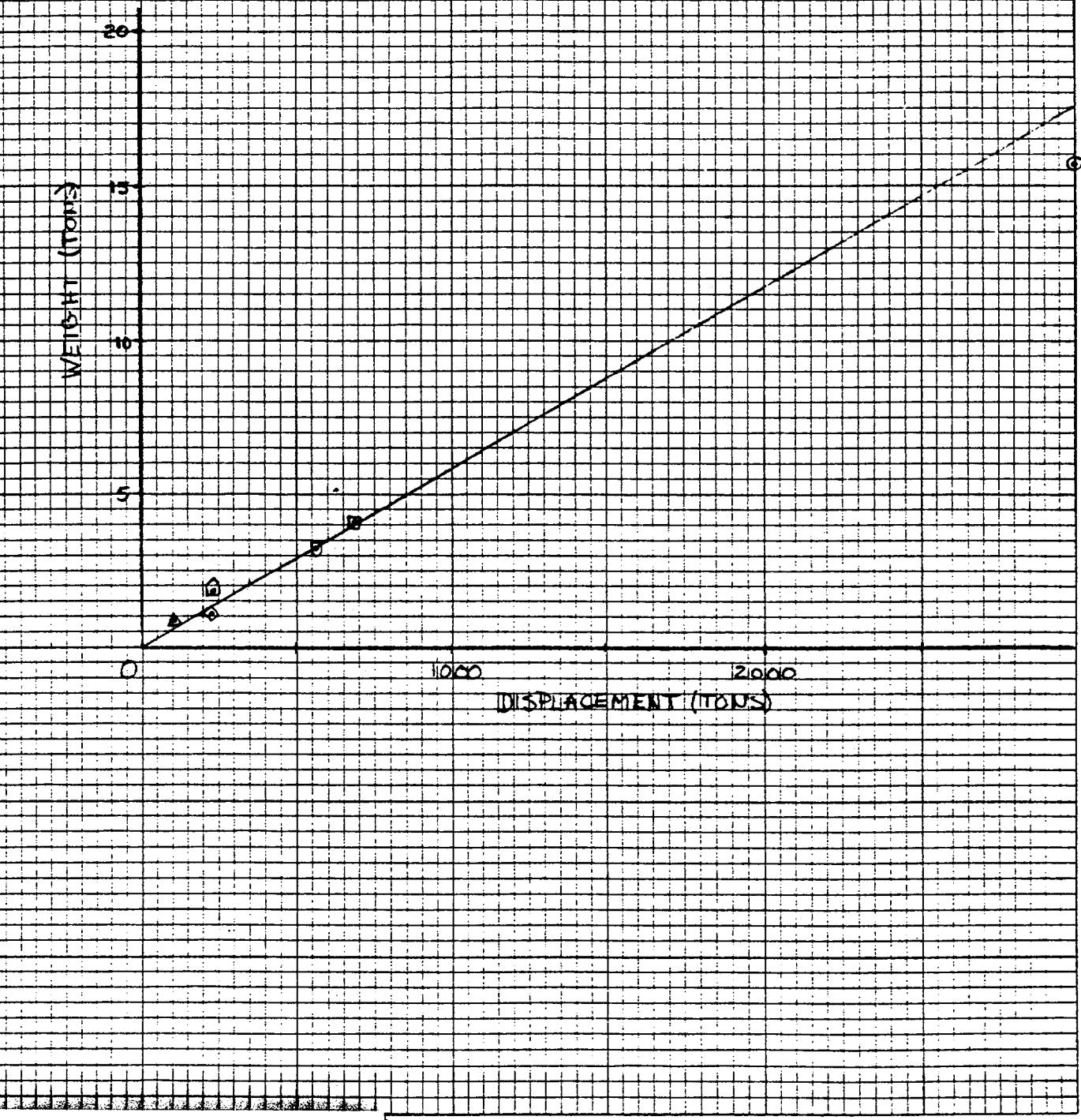
$VOL_A$  = Total Volume  $\times 10^{-3}$ ,  $\text{ft}^3$

The algorithm is based on the SES Design Manual.

SEE BSCZ-302

SWS GROUP W321

PILOT 10 X 10 TO 1 INCH  
1014 INF HEAVY



323 Casualty Power Cable ←

$$W_{323} = K_{323} * W_{321}$$

where  $K_{323} = .0346$  (SES Design Manual)

$W_{321}$  = Sharp Service Power Cable, lt

The algorithm is also from the SES Design Manual.

Fig. 15

W321 - SHIP SERVICE FLUER CABLE

W321 - SHIP SERVICE FLUER CABLE  
(0.105 TONS)

X AEWIC (0110/75)

X PF

$$W323 = .0346 \times W321$$

0

10

20

30

## 324 Switchgear and Panels ✓

$$W_{324} = K_{324} \cdot KW_I$$

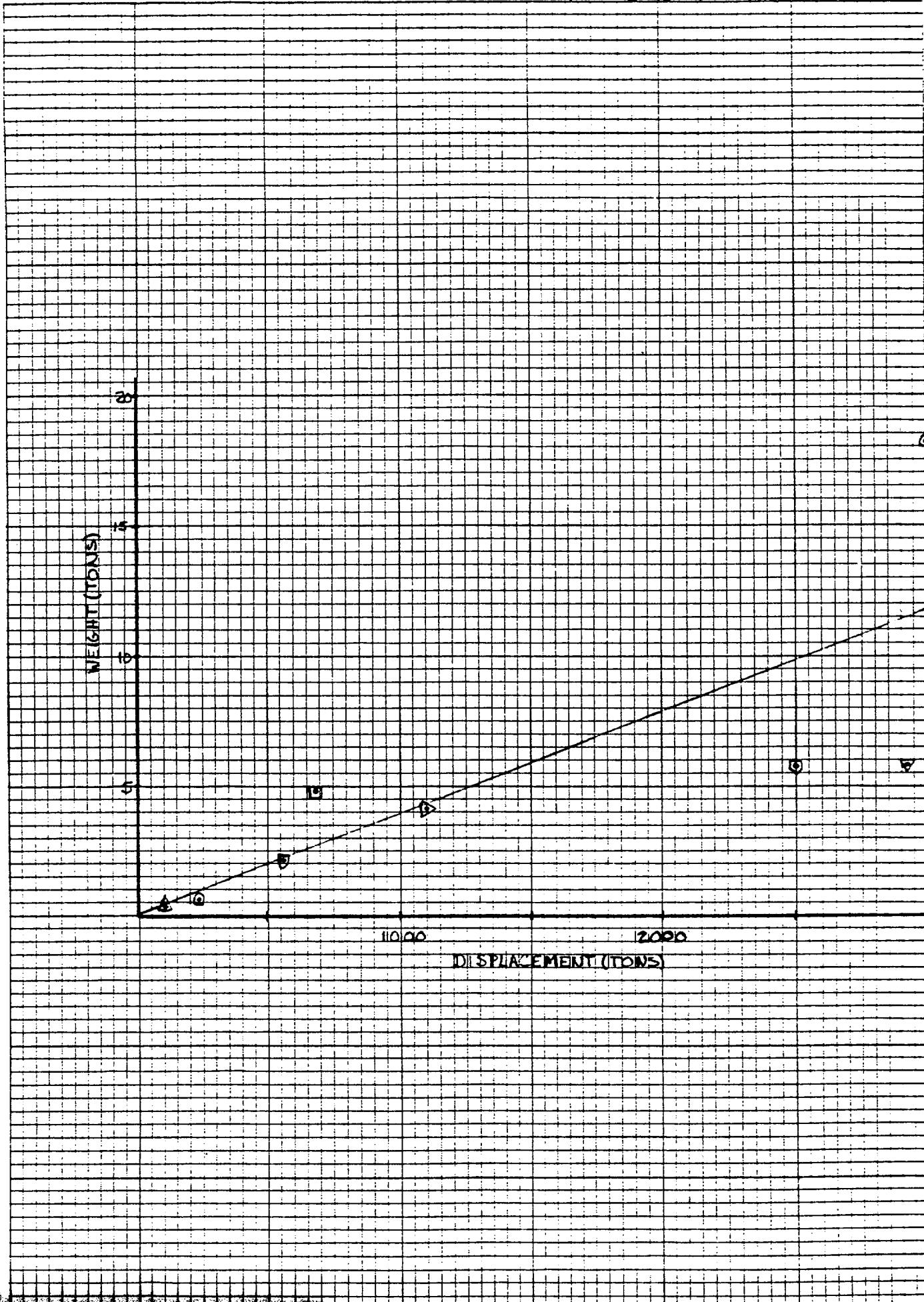
where  $K_{324} = .0035 \text{ lb/kw}$

( $K_{324}$  is a constant based on return weights  
for hydrofoils and SESs.)

$KW_I = \text{Installed KW, kw}$

The Algorithm is the same as ASSET.

SWE GROUP N 324



331 Lighting Distribution ✓

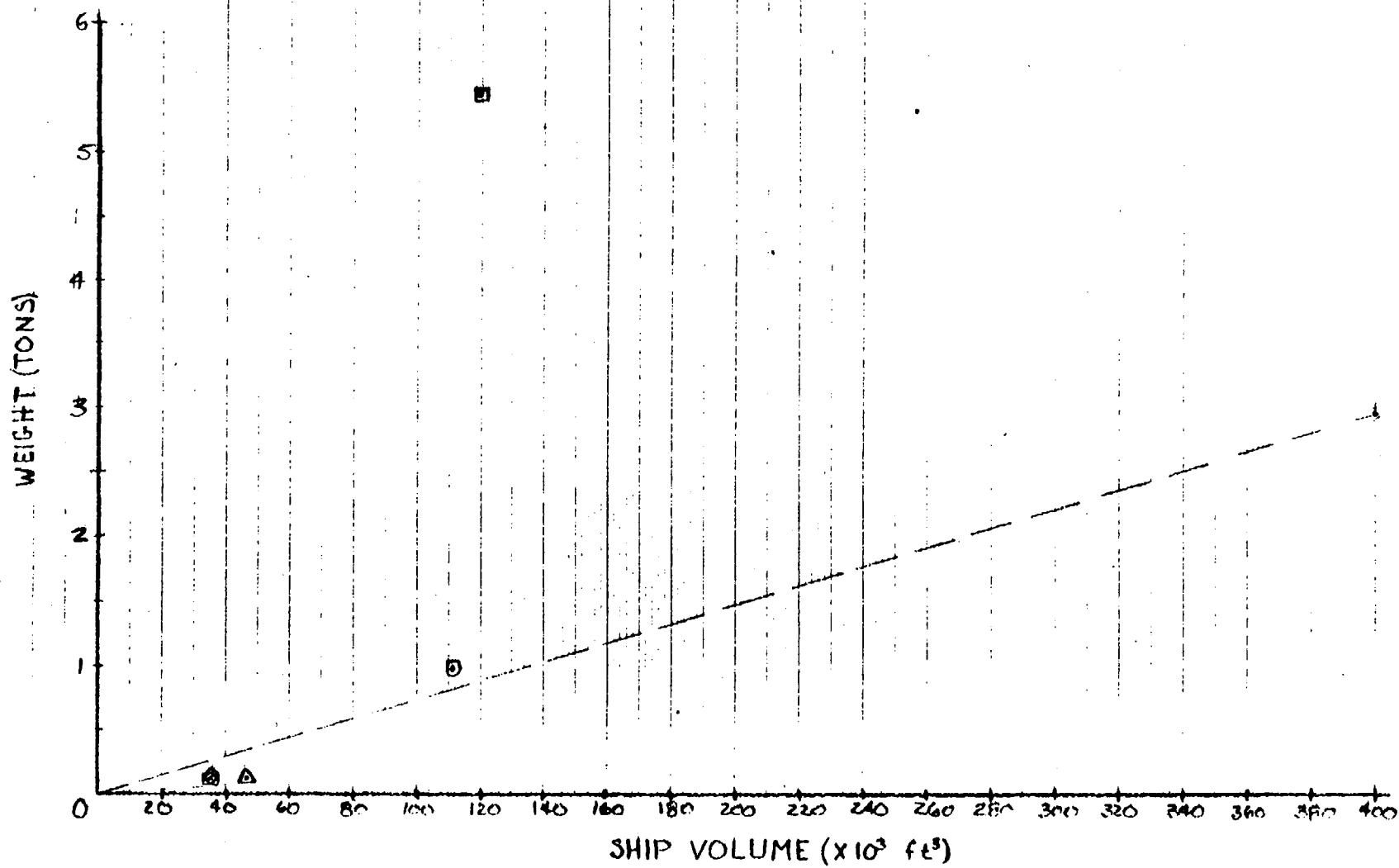
$$W_{331} = K_{331} \times VOL_A$$

where  $K_{331} = .0074 \text{ ft/lft}^3$

( $K_{331}$  is a constant determined from return data of hydrofoil and SESs.)

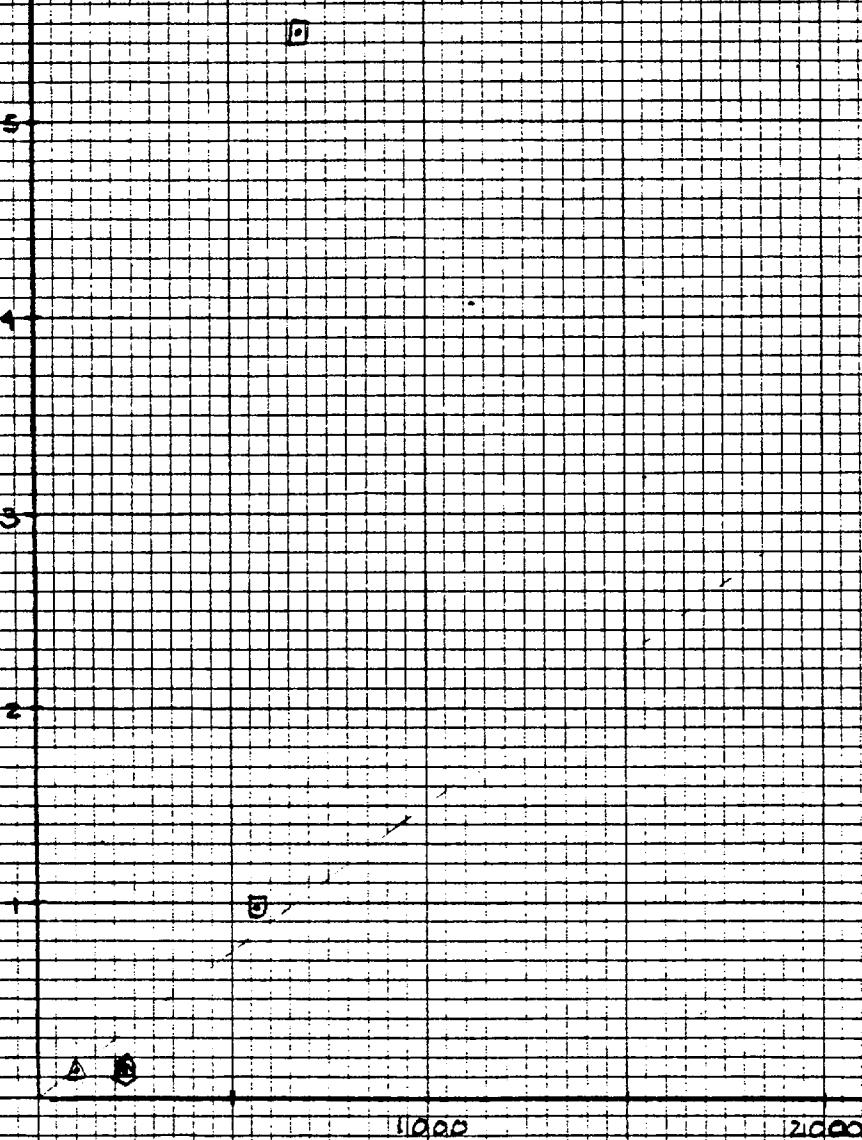
$$VOL_A = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

The algorithm is the same as ASSET and  
SES Design Manual

SWBS GROUP W 331 LIGHTING DISTRIBUTION

SEE 3002 = 303

SWS GROUT WESI



DISPLACEMENT (TONS)

## 332 Lighting Fixtures ✓

$$W_{332} = K_{332} * A_{COM}$$

$$\text{where } K_{332} = .027$$

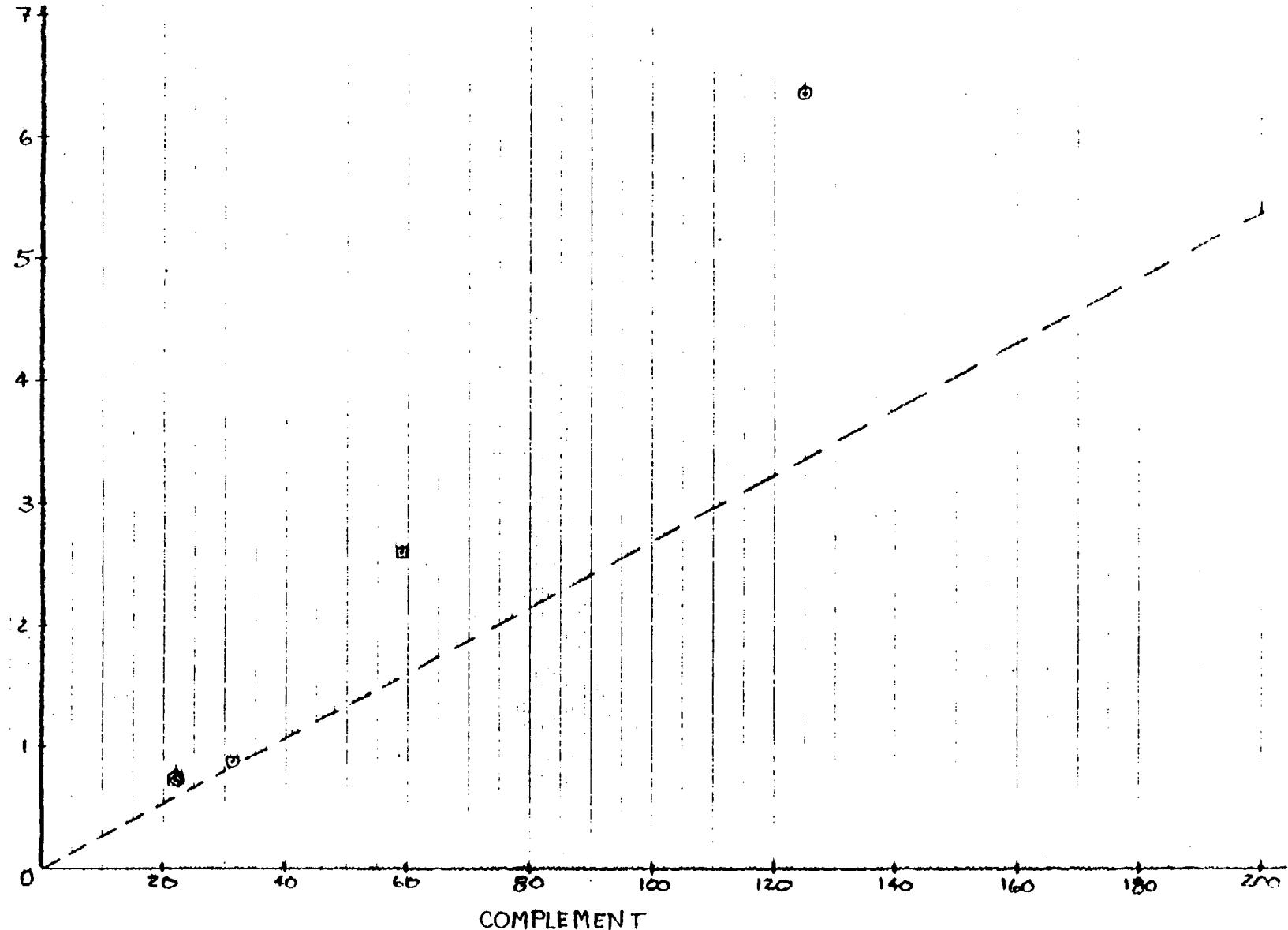
( $K_{332}$  is a constant drawn from return weights of hydrofoils and SESs.)

$A_{COM}$  = Total accommodations

•

This algorithm is the same as SES Design Manual.

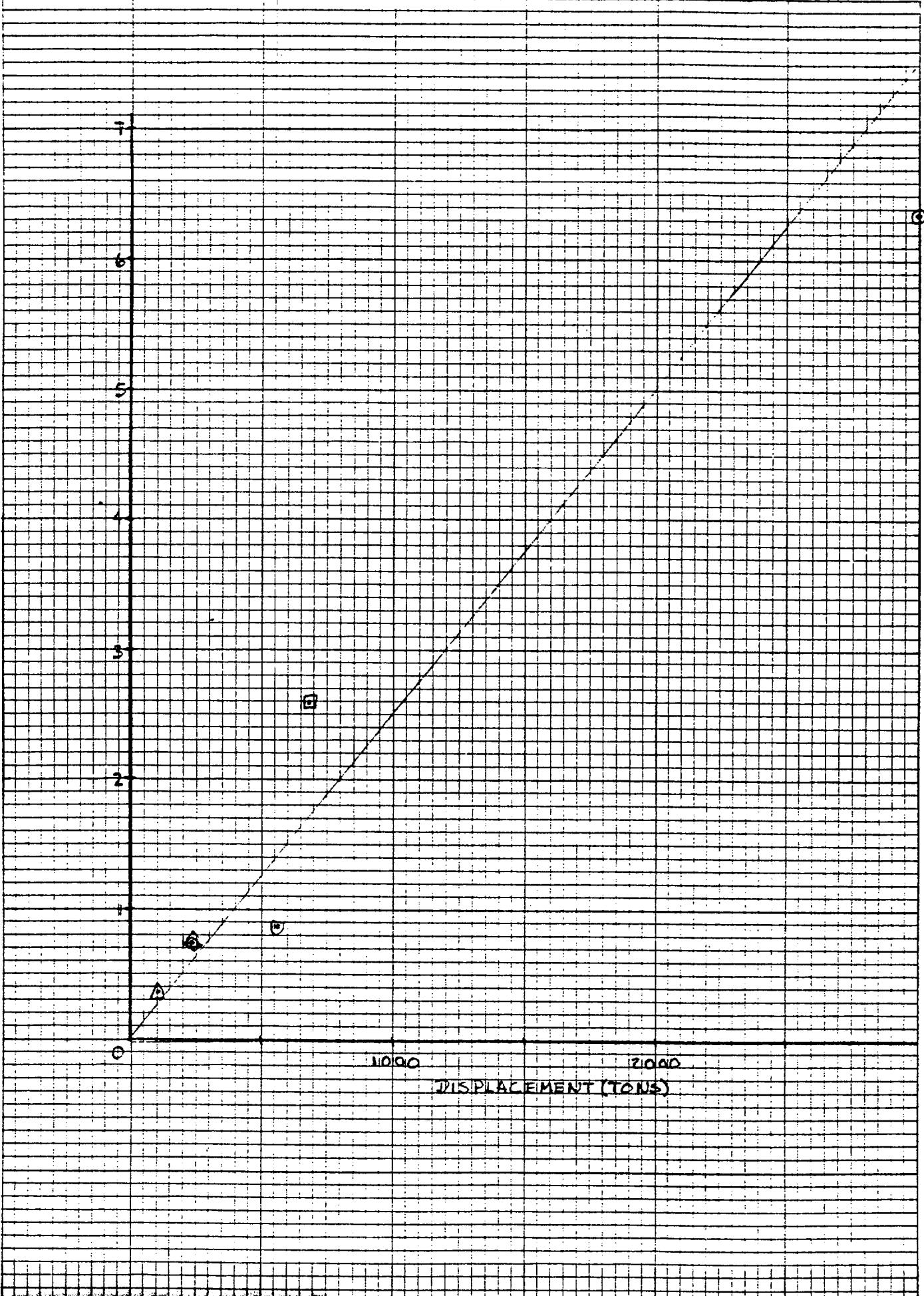
SWBS GROUP W332 LIGHTING FIXTURES



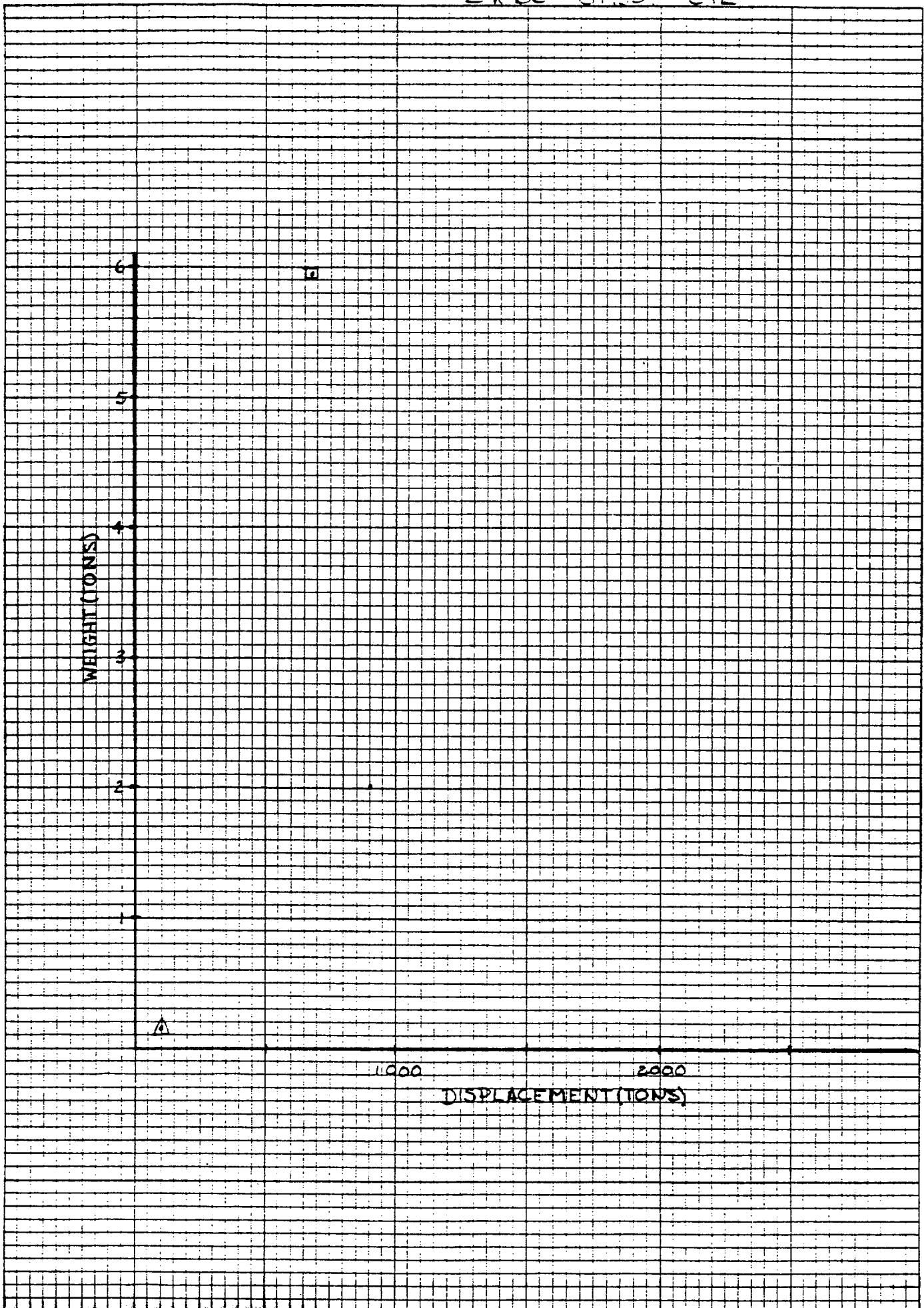
SEE PAGE 2 & 30E

SEE PAGE 30E

REDUCE IN X 10 TO 1 INCH  
SINCE THE HEAVY



SWE'S GRUVE 342



10MM 10 X 10 TO 1 INCH  
10TH LINE HEAVY

DRAWING PAPER NO. 1280-105  
TRACING PAPER NO. 1227-101  
CROSS SECTION - 10X10 TO 1 INCH

AQUABEE  
MADE IN U.S.A.

PF \*

Fig 19

W342 - DIESEL SUPPORT

W342 - DIESEL SUPPORT (LONG TORS)

PCH-1 X AGEH-1

W311 - SHIP'S GEN. MACHINES (DIESEL)  
(TORS)

0 10 20 30 40 50 60 70 80 90

343 Turbine Generator Support System ✓

$$W_{343} = K_{343} \times KWI$$

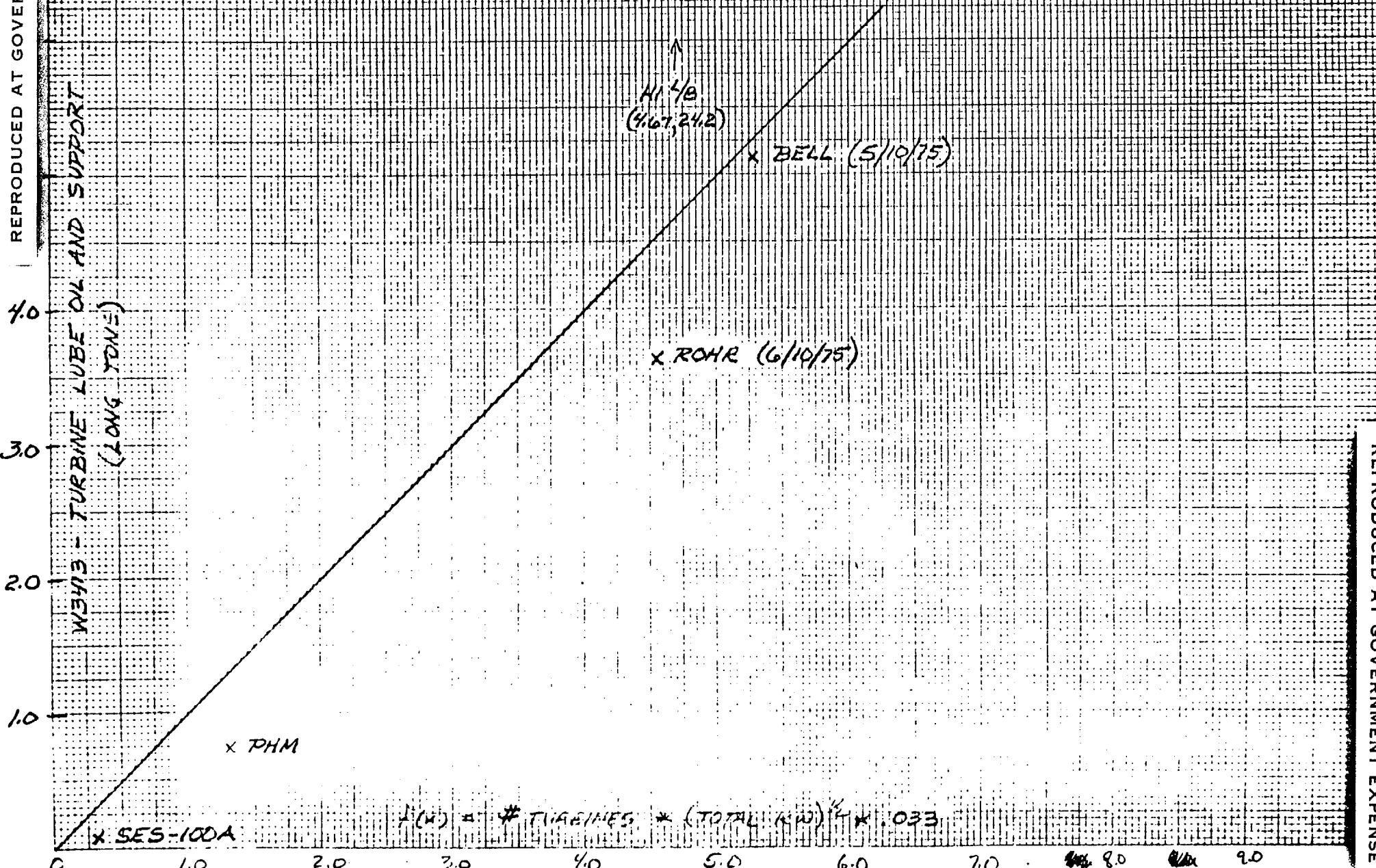
where ~~K~~  $K_{343} = .0061 \text{ ft/kw (ASSET)}$

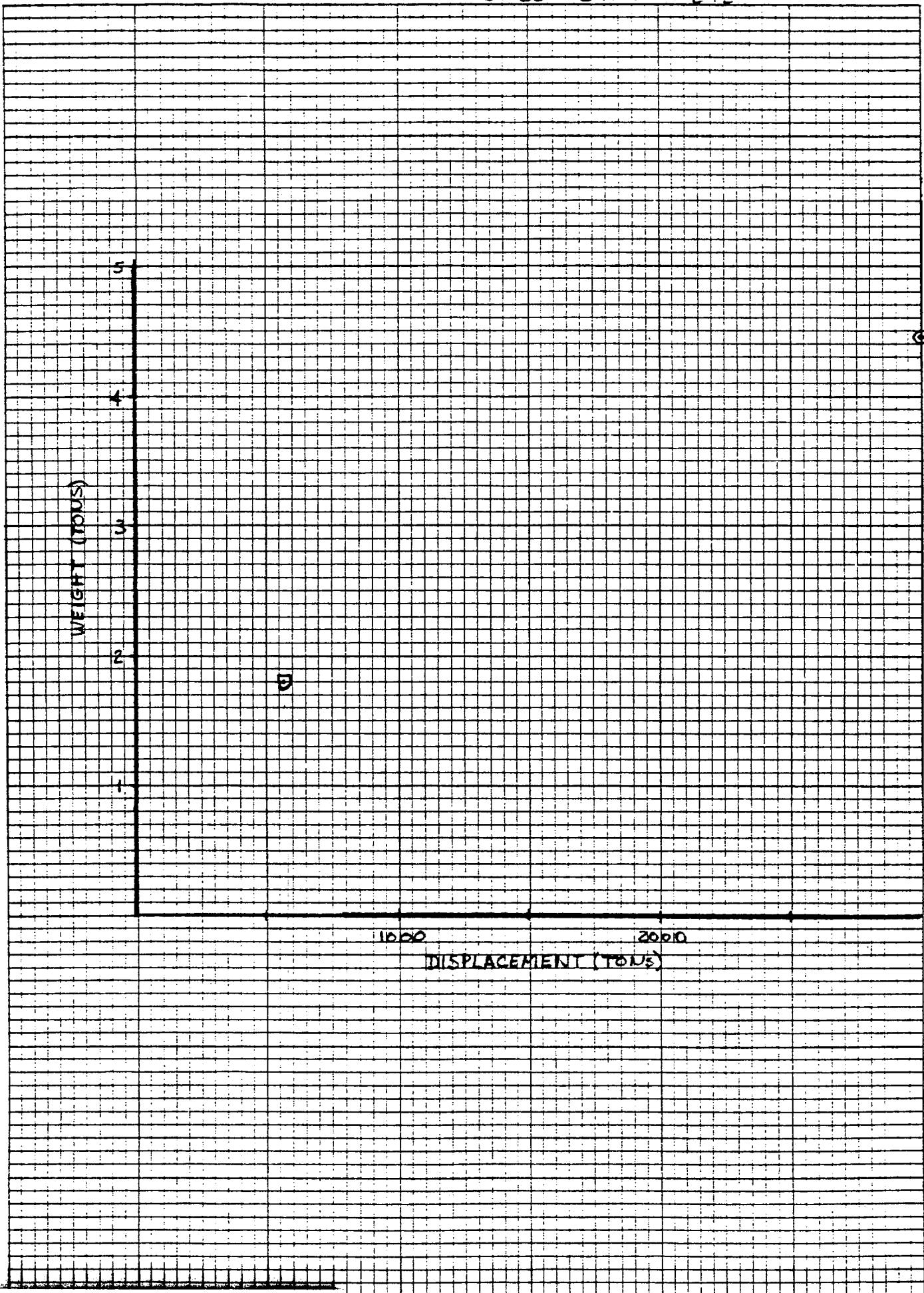
$KWI = \text{Install KW, kw}$

Algorithm is also the same as ASSET

ROUTE 3KSES  
(9.39, 9.78)

Fig 10

W3413 - TURBINE LUBE OIL AND SUPPORTW3413 - TURBINE LUBE OIL AND SUPPORT  
(Long YOH=)



398 Electric Plant Operating Fluids ✓

$$W_{398} = \frac{K_{398} \times KWI}{\text{_____}}$$

where  $K_{398} = .002 \text{ ft/kw}$

( $K_{398}$  is derived from return weights  
on hydrofoils and S6SS.)

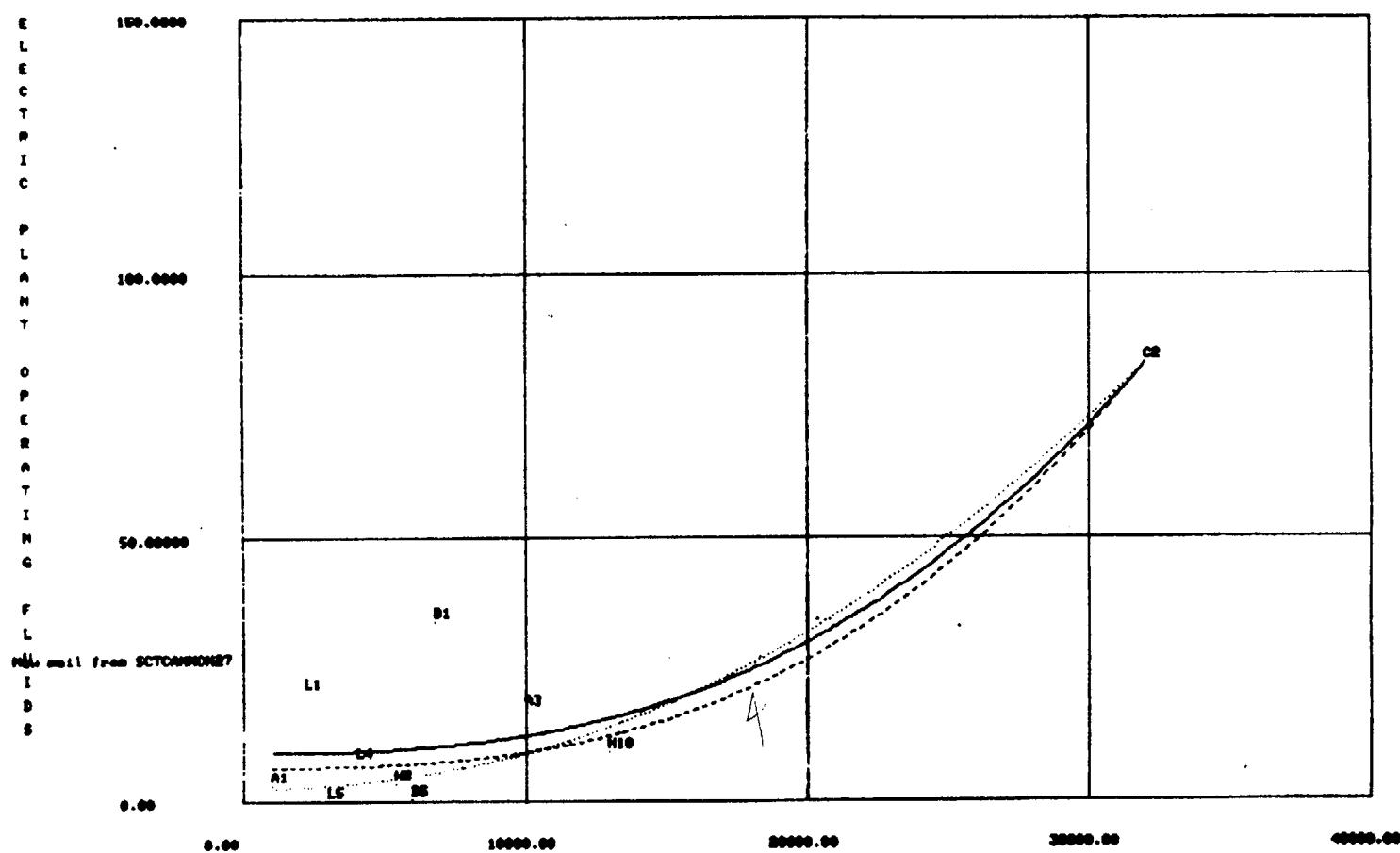
KWI = Installed KW, kw

The Algorithm is the same as ASSET.

To convey home, like sentiment

CONTINUE

## ELECTRIC PLANT OPERATING FLUIDS (300)



$$WZ+? = 7.341 + 2.427 \times 10^{-3} L + 1.1 \times 10^{-6} L^2$$

1.  $\text{C}_2\text{H}_5\text{OH}$  +  $\text{O}_2$   $\xrightarrow{\text{Cu}} \text{CH}_3\text{CHO} + \text{H}_2\text{O}$

$$= 2.07 + 3.80 \text{ KW}^{2.150}$$

## 399 Electric Plant Parts and Special Tools

$$W399 = K399 \times KWI$$

where  $K399 = .001 \text{ ft/lkw}$

( $K399$  is based on return weights of hydrofoils and SESs.)

$KWI$  = Installed KW, kw

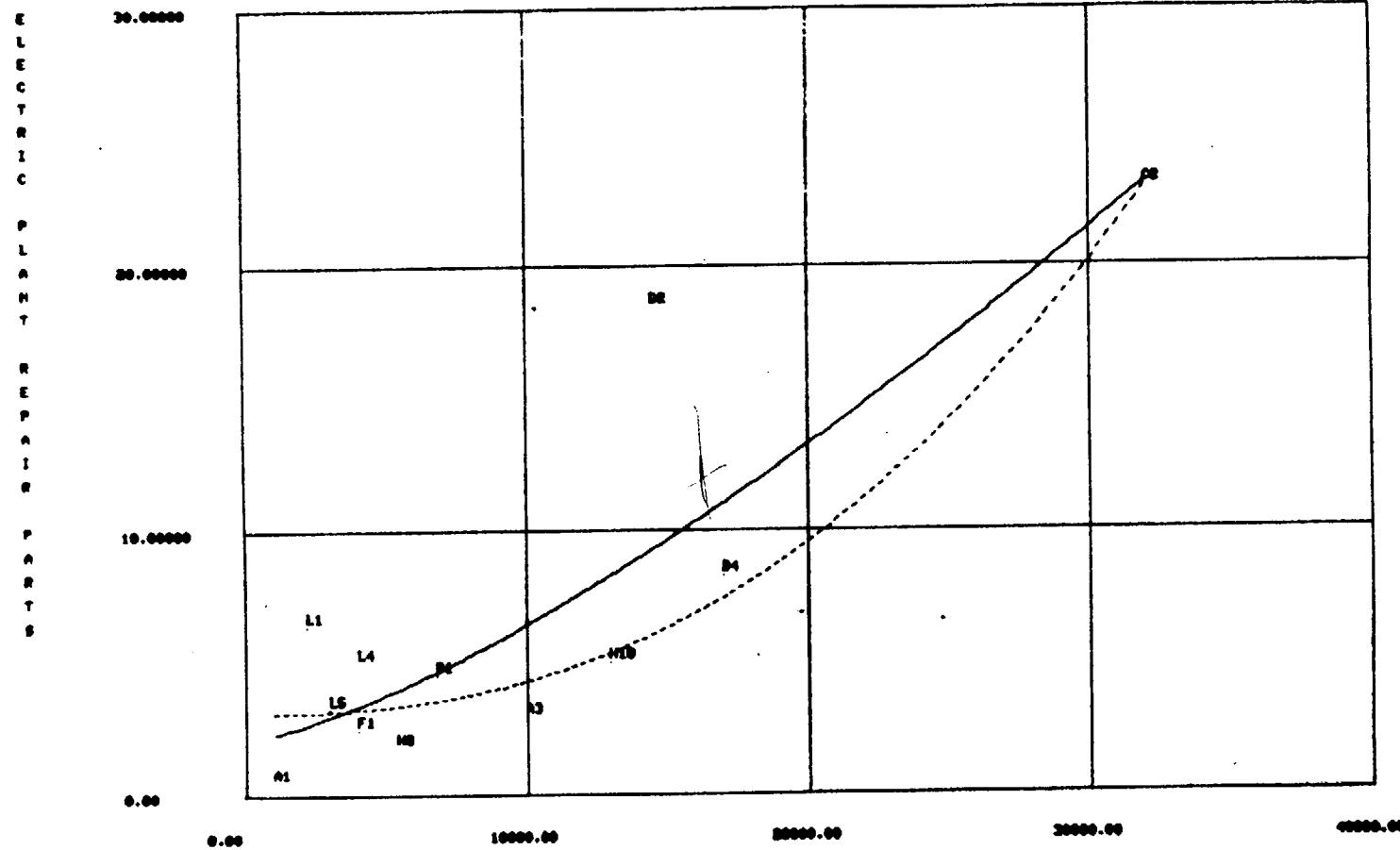
The algorithm is the same as ASSET.

TO CONTINUE, TYPE CONTINUE

© CONTINUE

## ELECTRIC PLANT REPAIR PARTS (398)

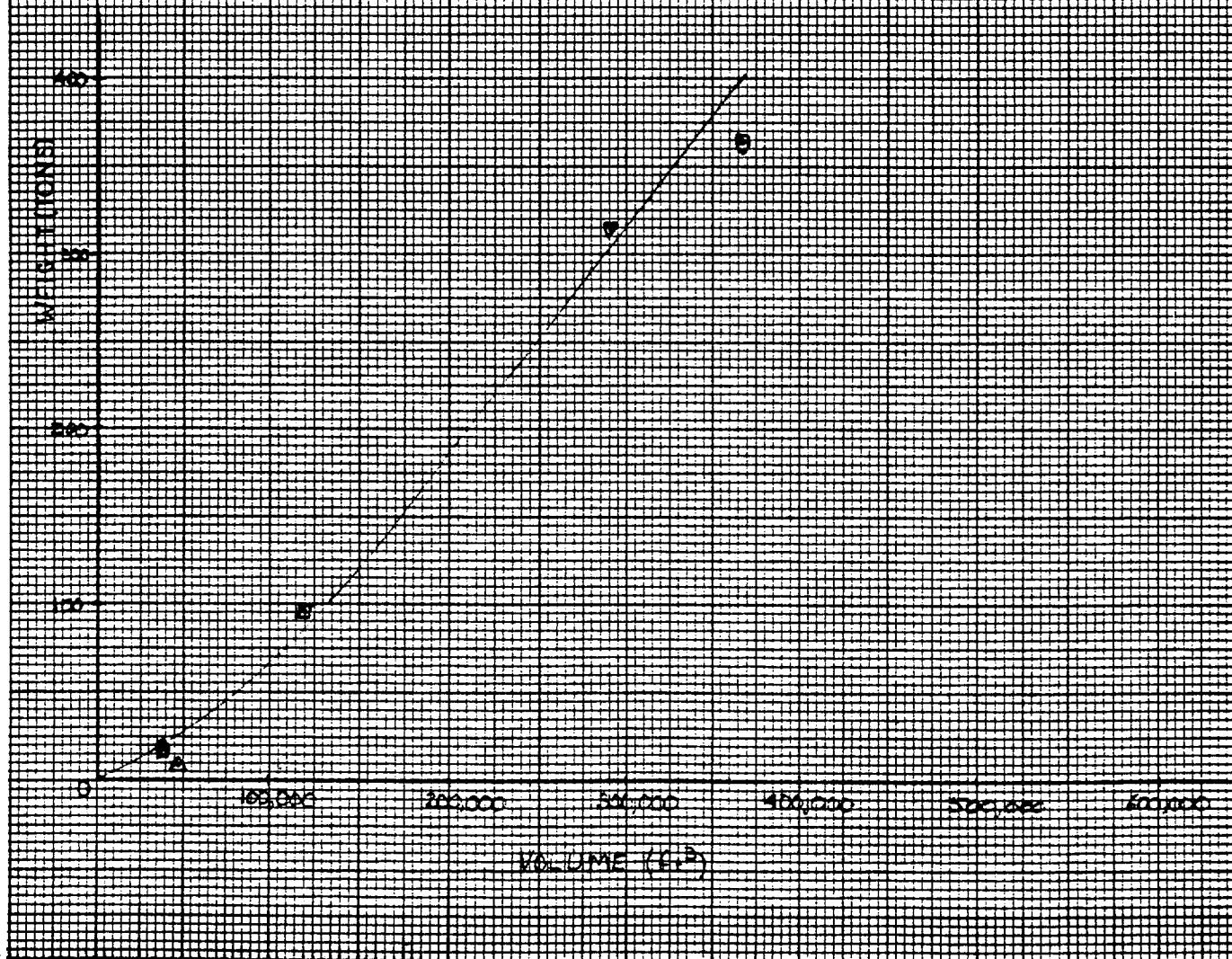
— ALL DATA — S.S. ERROR — I.S. ERROR

1372  
= 3.123 + 0.195 \* 10<sup>4</sup> (1.0)

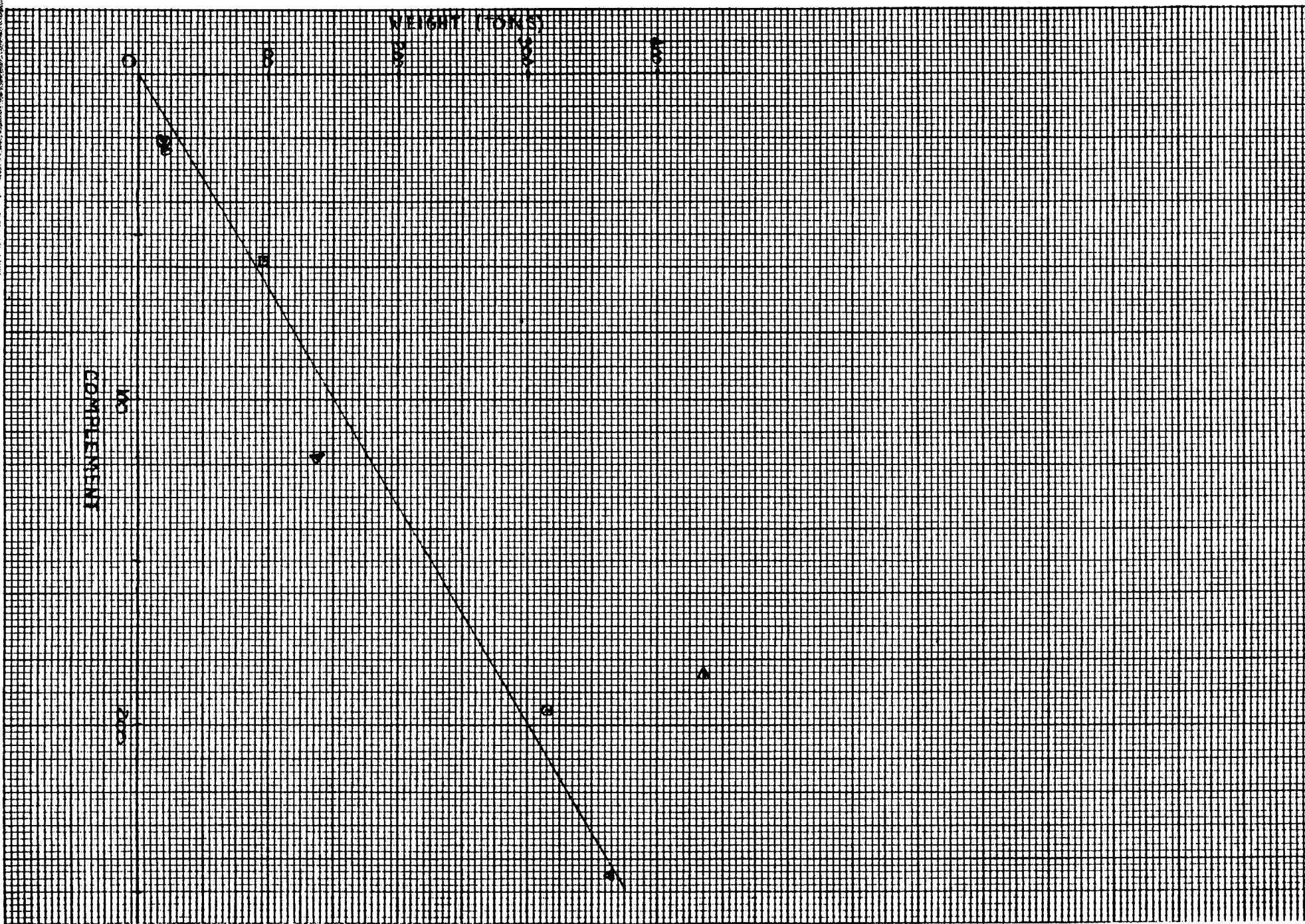
$$= 3.123 + 0.195 \times 10^4 (1.0)$$

SWRZ GPM/H VS TIME VS SHE VOLUME

FPL AM 20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED



FPI MI-20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED



✓ SII Compartment Heating

$$W_{SII} = K_{SII} \times \cancel{ASSET} VOLA \checkmark$$

$$\text{where } K_{SII} = .002 \text{ ft/gf}^3 \checkmark$$

( $K_{SII}$  is based on return data from hydrotools  
and SSES.)

$$\text{ACOM} = \text{Number of accommodations}$$
$$VOLA = \text{Total volume} \times 10^{-3}, \text{ ft}^3$$

The Algorithm is based same as ASSET.

ITEM  
EC → EA

Fig 20

W5M - COMMISSIONING NEGATIVES

X N14/12

2.0

1.0

W5M - COMMISSIONING  
(long runs)

PCH-1 (VOL1)

X PHM (VOL1)

$$f(x) = .204 * (VOL1 - (2.0 + VOLSH)) * 10^{-5}$$

X BELL (5/27/75)

X BELL (3/1/76)

X ROHR (6/10/75)

8/9/73 delete  
& use conventional

$$(VOL1 - (2.0 * VOLSH)) * 10^{-5}$$

0

1.0

2.0

3.0

4.0

5.0

6.0

7.0

8.0

9.0

10.0

SWPS GROUP W 5ii

2.0

1.5

1.0

0.5

0

REFLCTN IN X TO 1 INCH  
TOTAL TIME HEAVY

D E

00000

12000

## ✓ 512 Ventilation System

$$WS12 = KS12 * \text{VOLA}^{\sqrt{}}$$

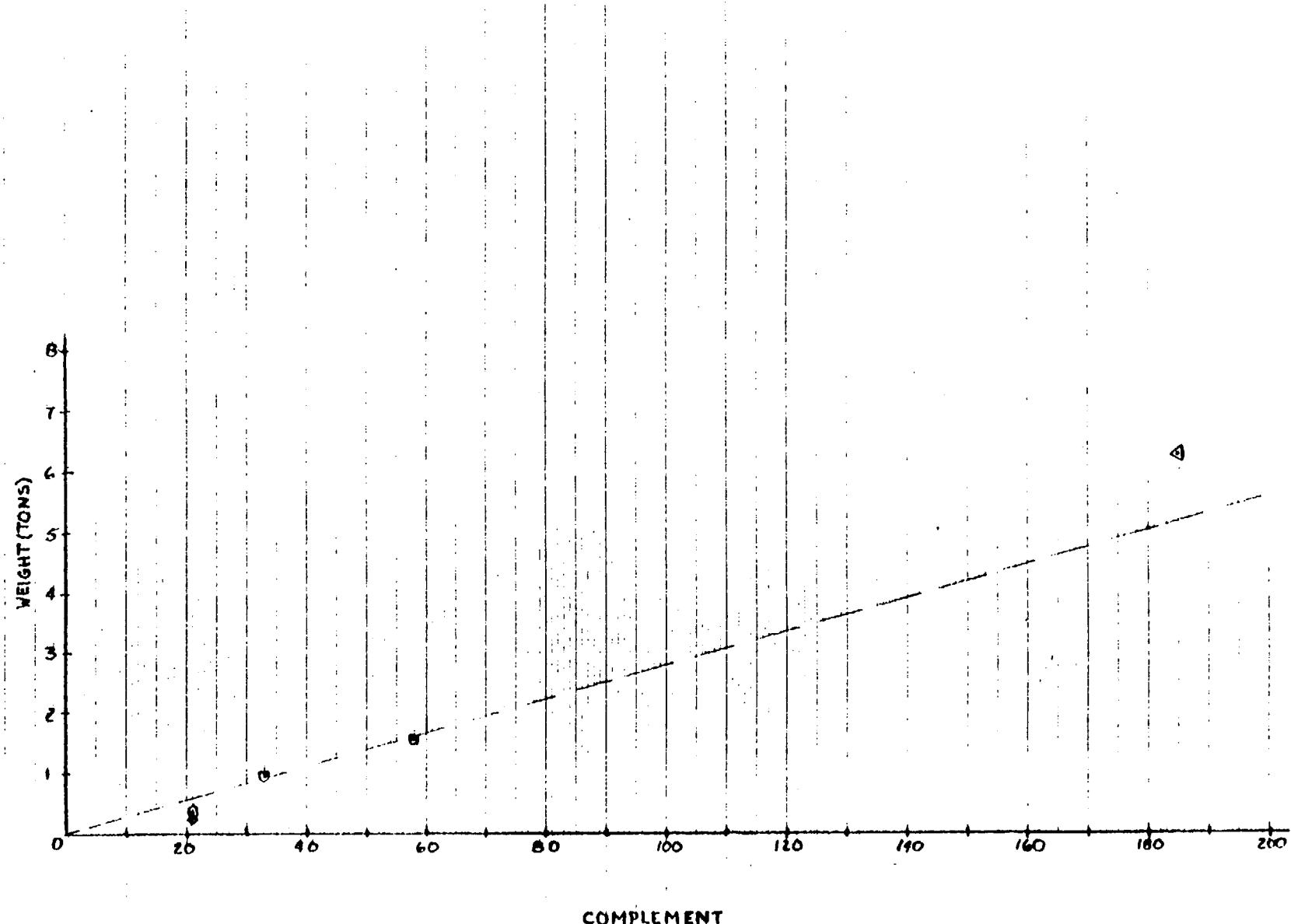
$$\text{where } KS12 = \text{[redacted}} .01 \text{ ft/lb}^3 \checkmark$$

(KS12 is based on return data from hydrofoils  
and 8855.)

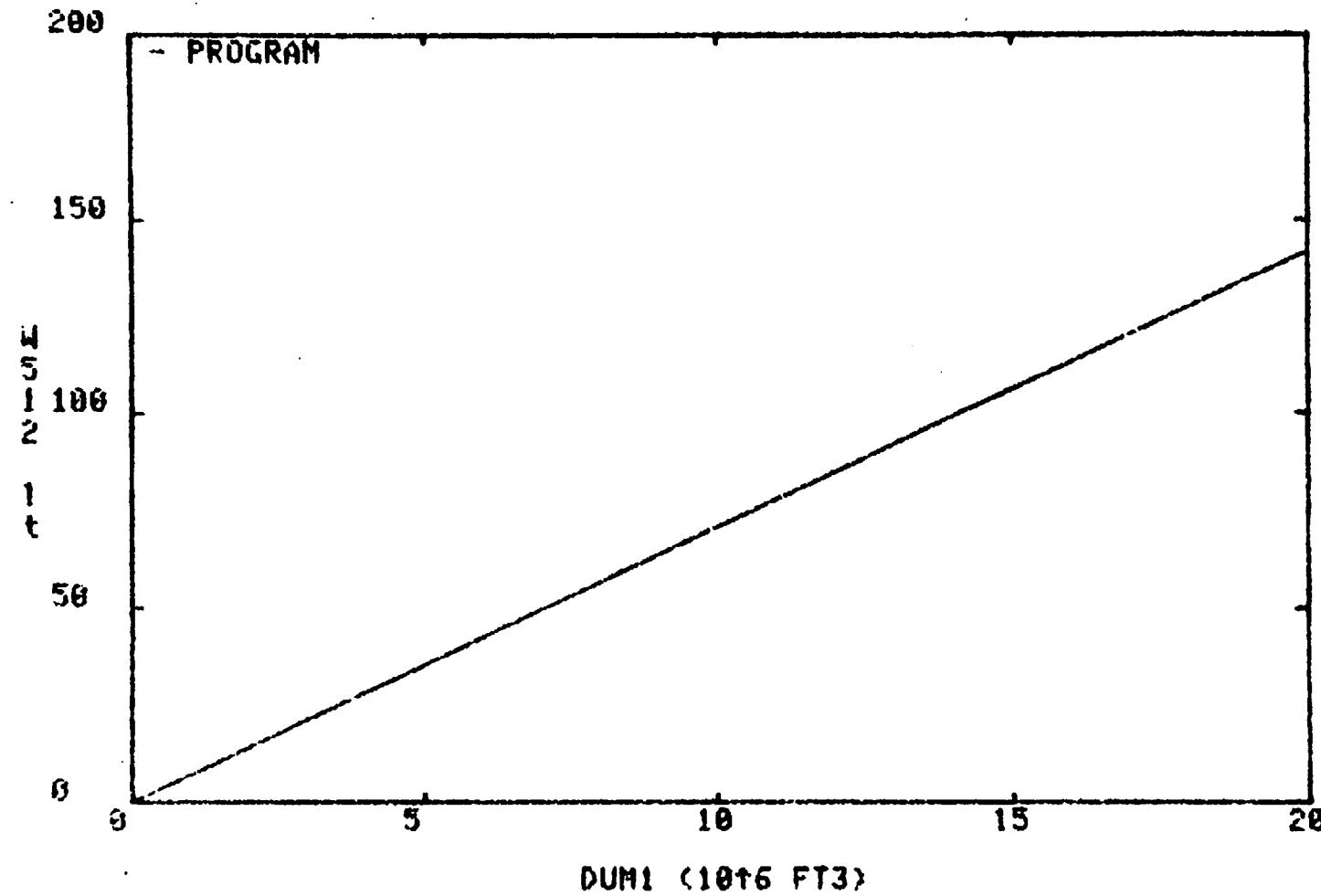
$$\text{VOLA} = \text{Total Volume} * 10^{-3}, \text{ ft}^3$$

The algorithm is the same as ASSET

SWBS GROUP W512 VENTILATION SYSTEM



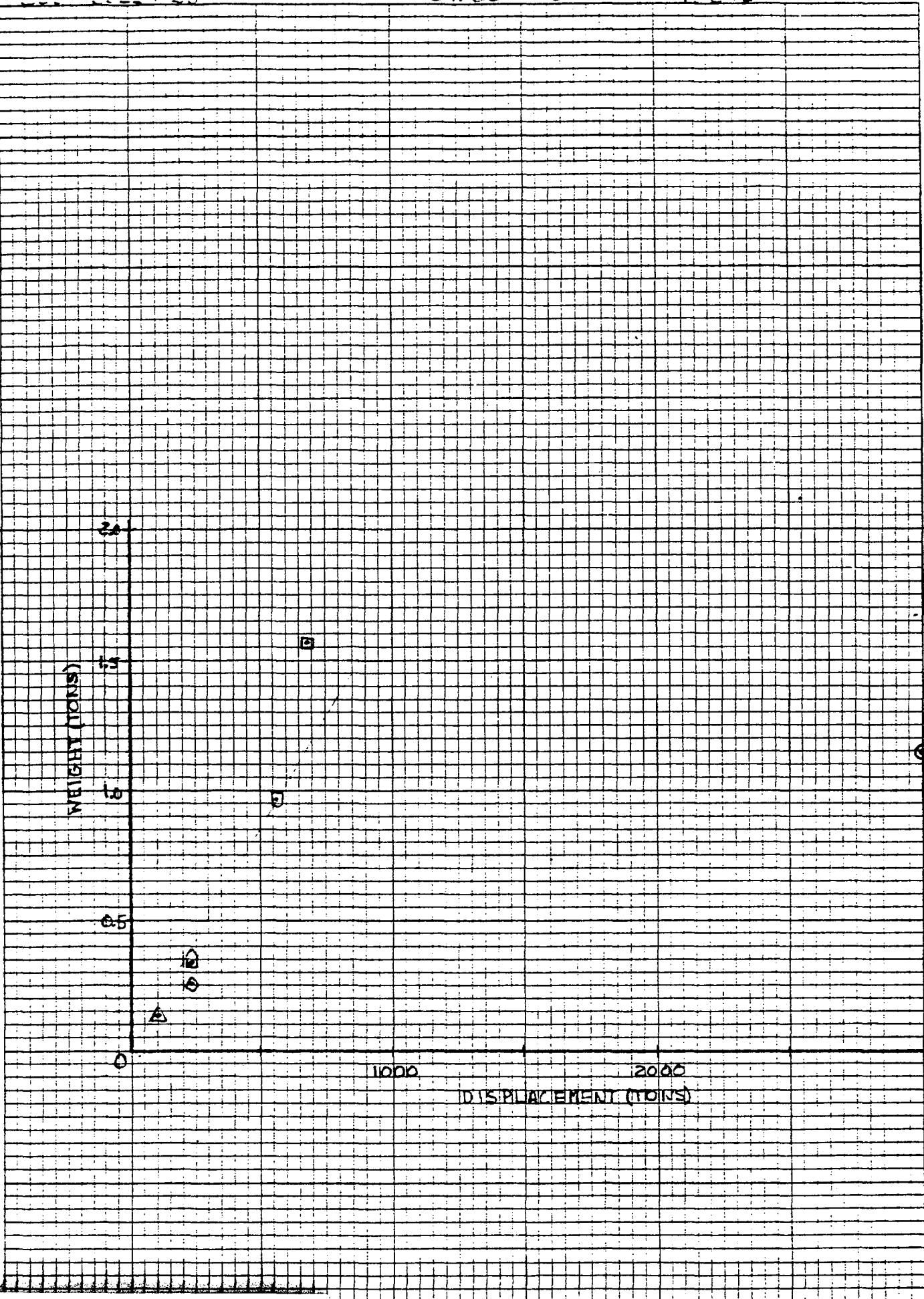
W512 VS DUM1 AS OF 10/27/83



SEE 3005-50

SWE G-305 1512

FROM IN X TO 1 MTH  
10H LINE HEAVY



## 1513 Machinery Space Ventilation System

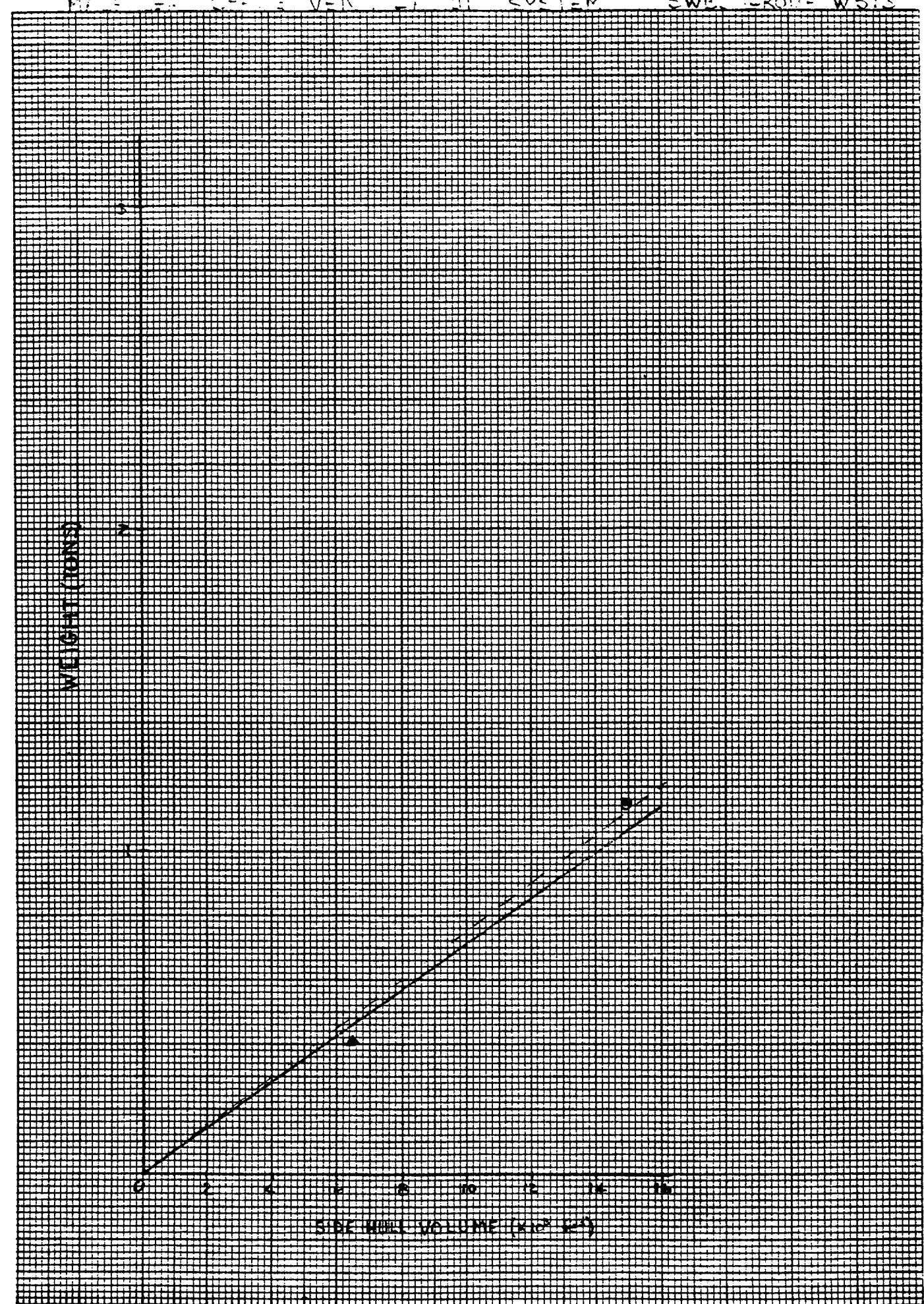
$$WS13 = KS13 \times VOLA \checkmark$$

$$\text{Where } KS13 = .008 \text{ ft/s}^3 \checkmark$$

(KS13 is a constant based on return data from hydrofoils and SSSs.)

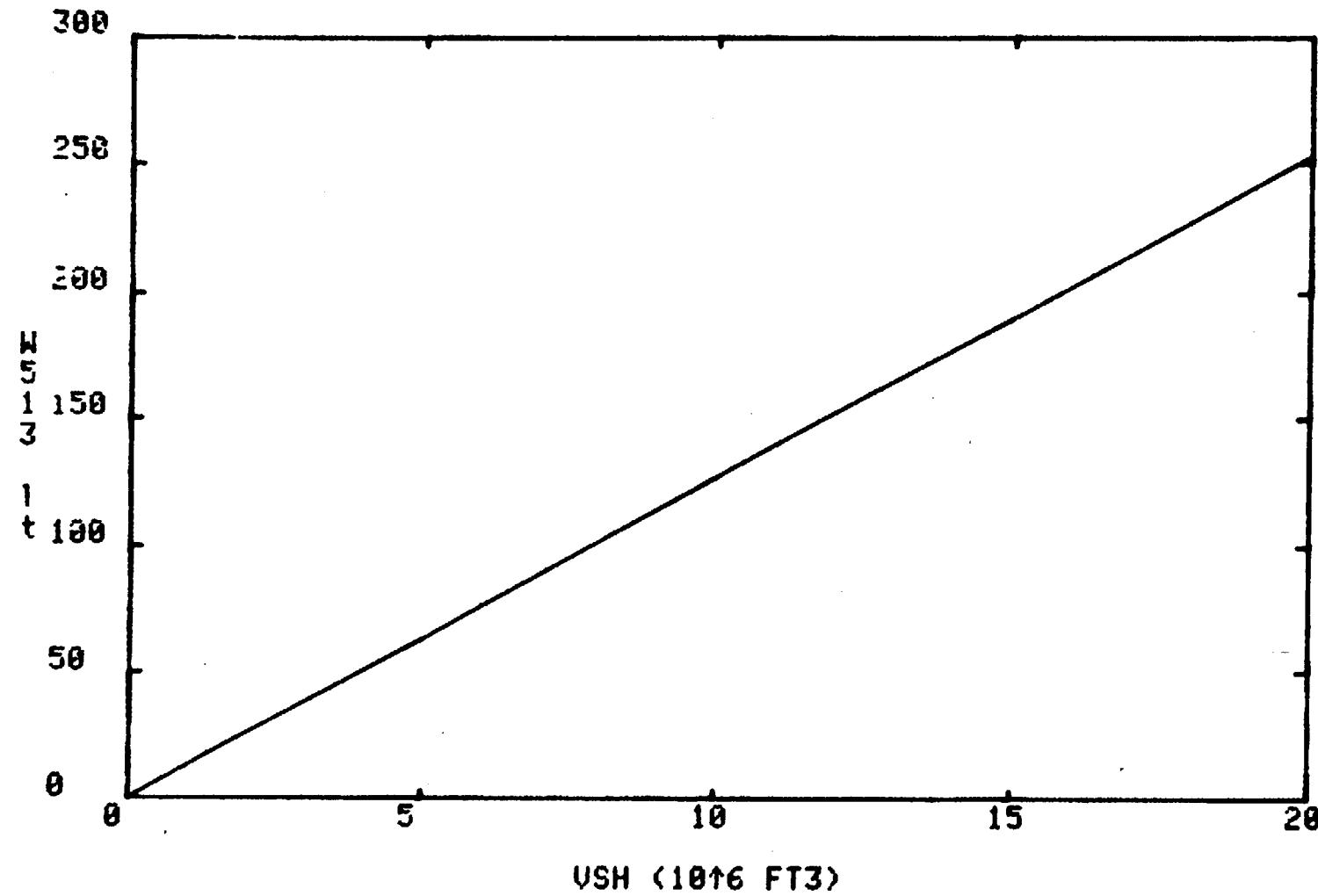
$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

The algorithm is the same as ASSET.



FPI NO. 20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED

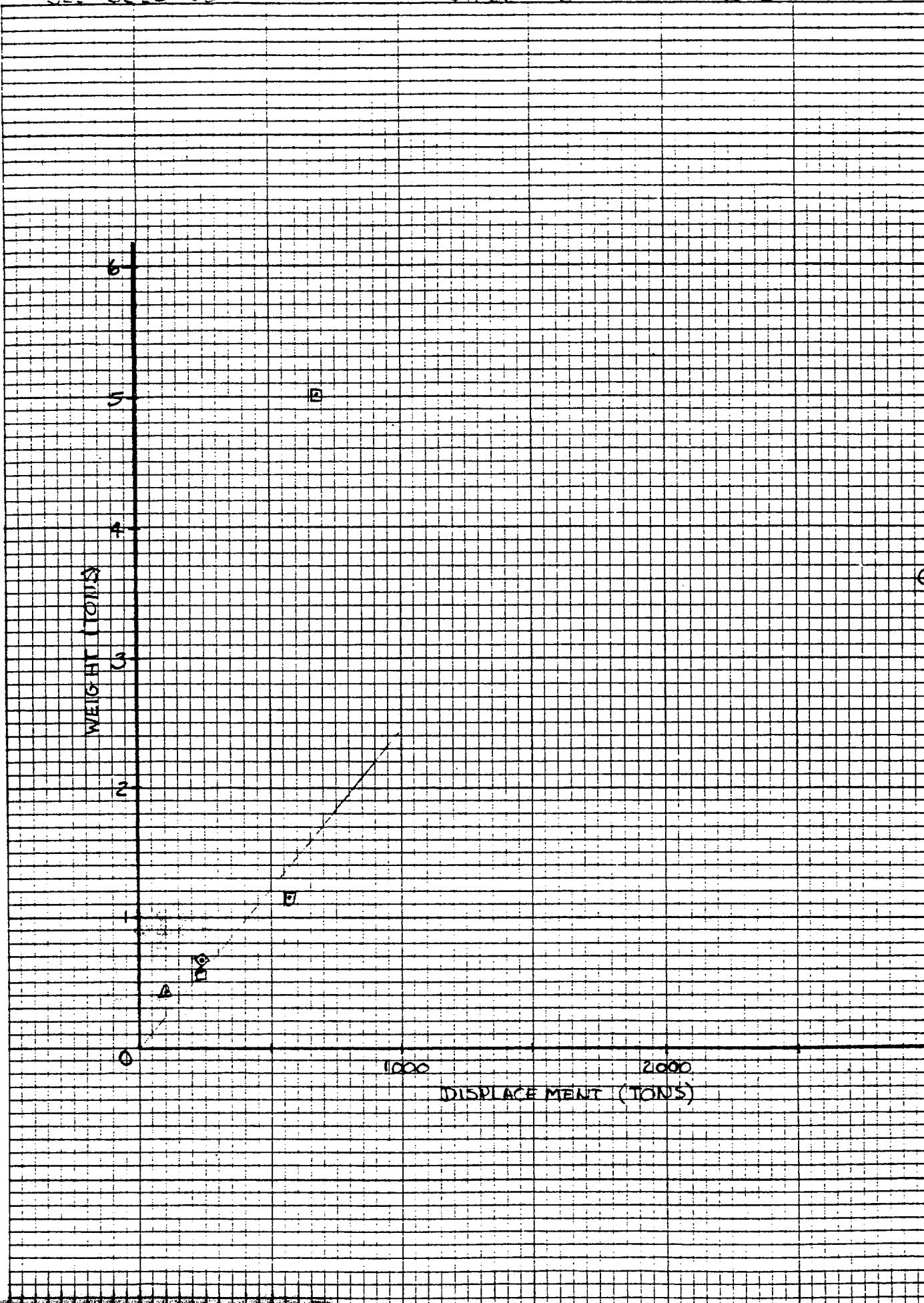
W513 VS VSH AS OF 10/31/83



SEE PAGE 50

# SUPER GROJE WISSE

1914 HISTORICAL REVIEW



## 1.514 Air Condition System

$$WS14 = K_{S14} + LS14 * VOLA + MS14 * ACOM \checkmark$$

$$\text{when } K_{S14} = .1 \text{ ft}, LS14 = .025 \frac{\text{ft}}{\text{ft}^2} + MS14 = .07 \text{ ft} \checkmark$$

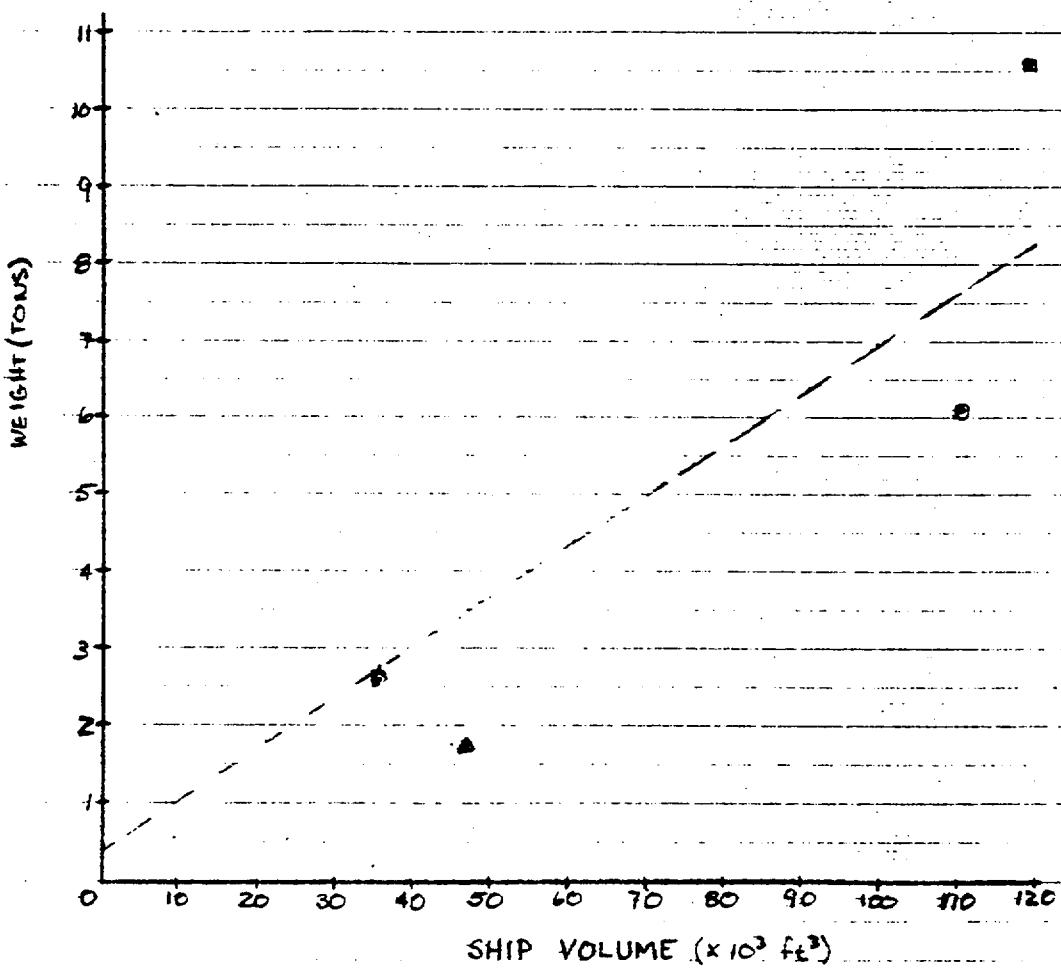
(These constants are based on return weights  
of hydrofoils and SESs.)

VOLA = Total volume  $\times 10^{-3}$ , ft<sup>3</sup>

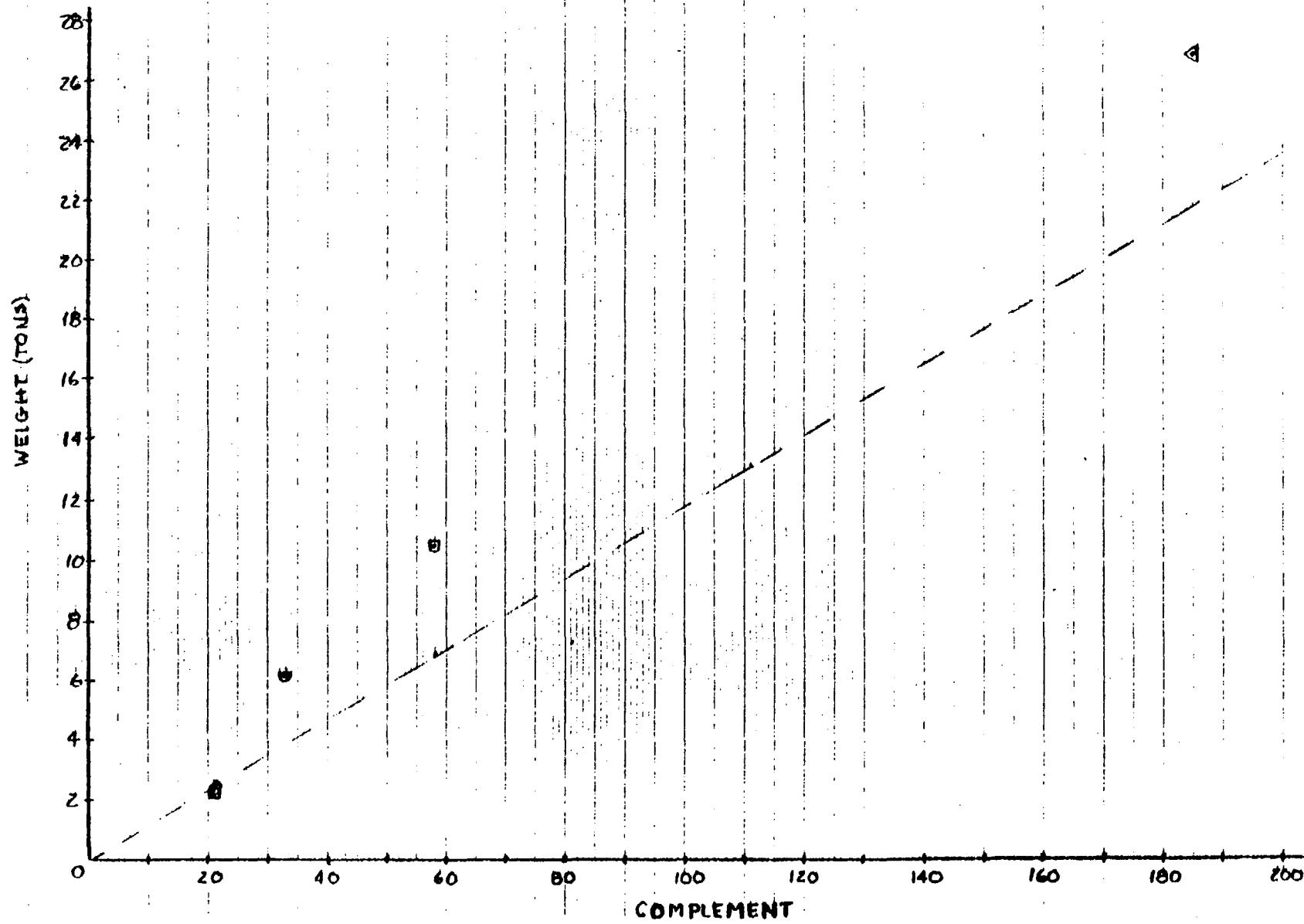
ACOM = Number of Accommodations

The algorithm is the same as ASSIST.

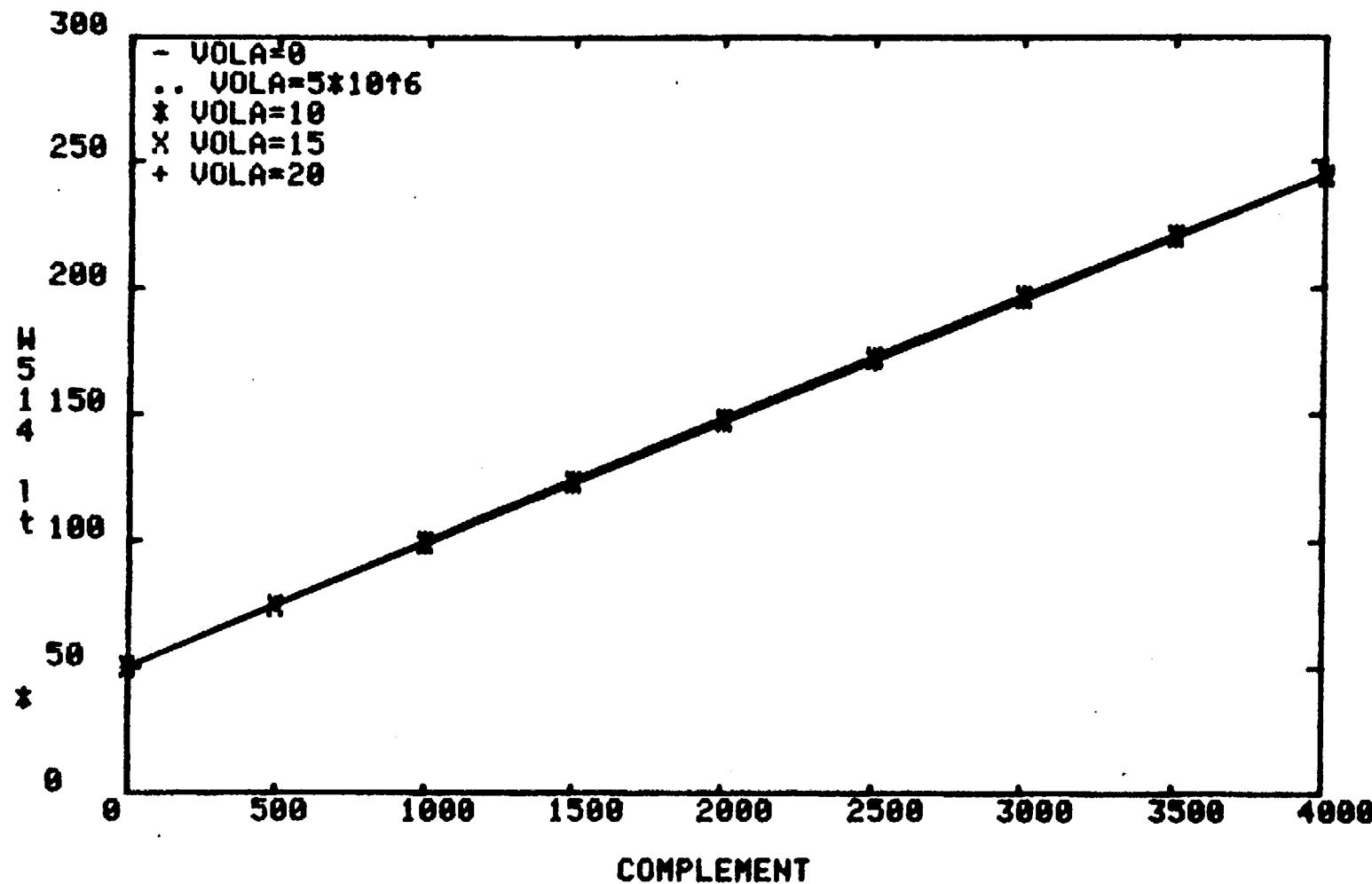
AIR CONDITIONING SWBS GROUP WS14



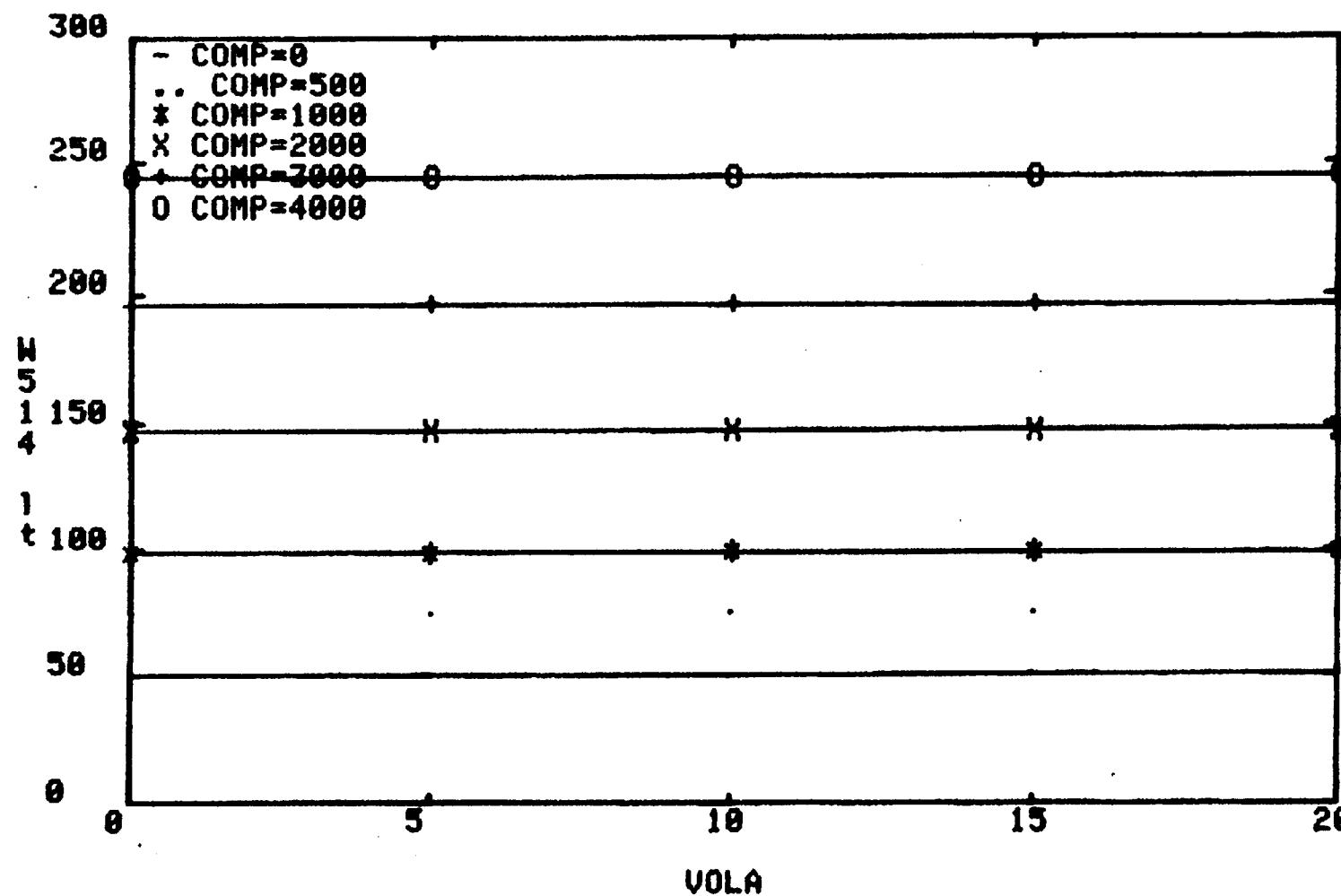
SWBS GROUP W514 AIR CONDITIONING



## CONSTANT VOLA ON W514 VS COMPLEMENT AS OF 10/27/83

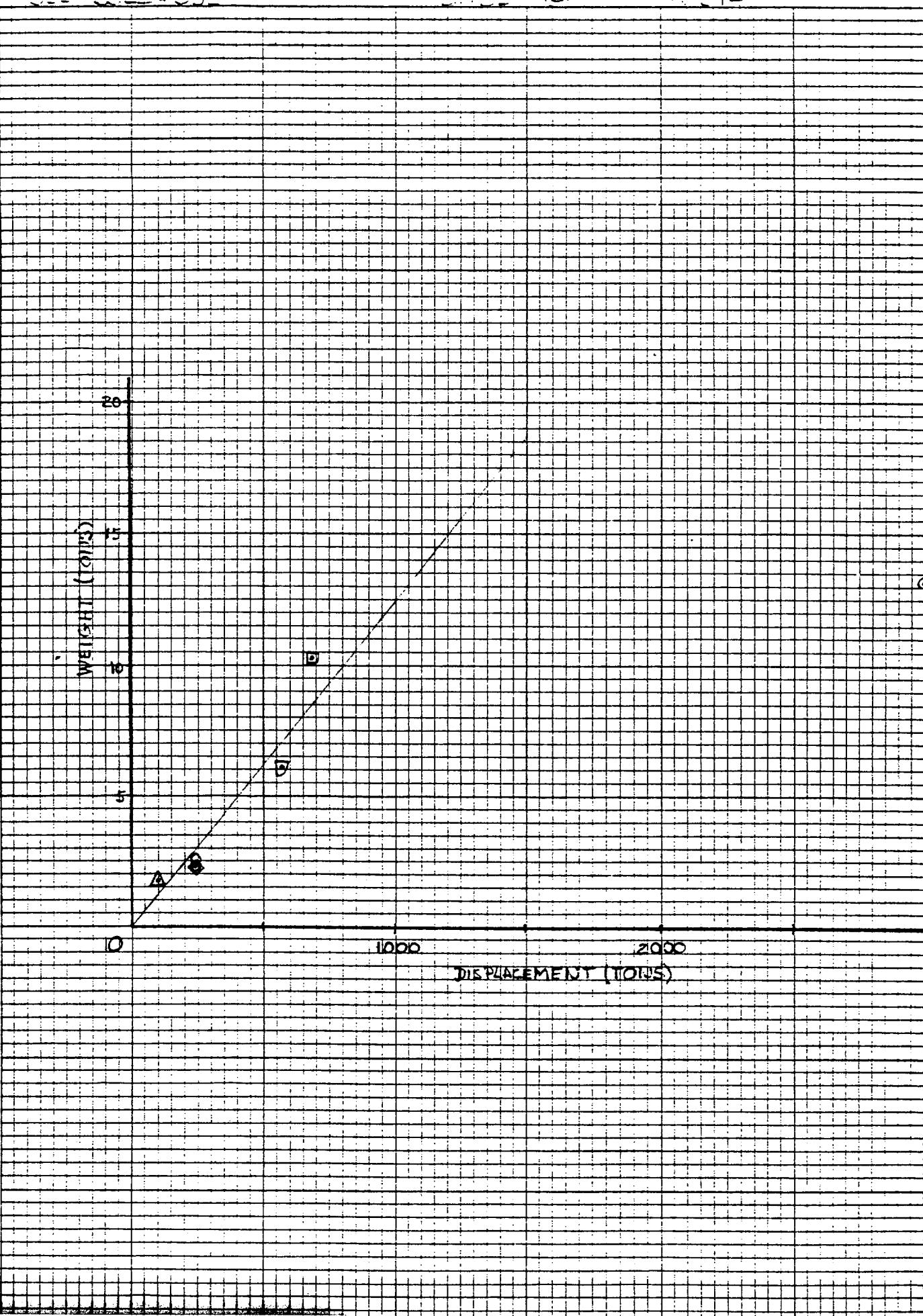


CONSTANT COMPLEMENT ON W314 VS VOLA AS OF 10/27/83



SEE PAGE 502

S.A.S. 10-1-1-1514



## 1516 Refrigeration System

$$WSIG = KSIG \times ACOM \checkmark$$

where  $KSIG = .0083 \text{ ft}^{\checkmark}$

( $KSIG$  is a constant based on victim data  
for hydrofoils and S&Ss).

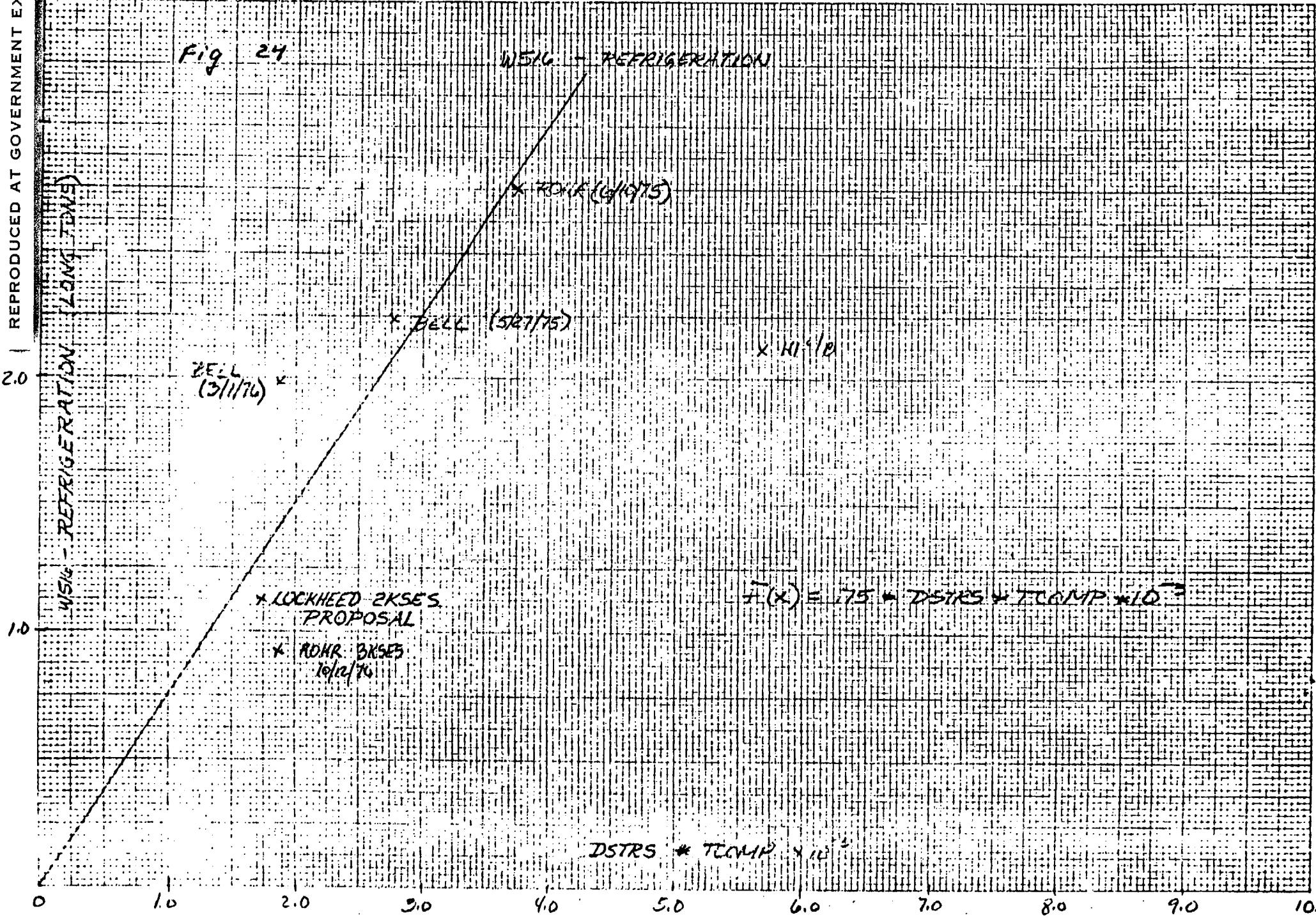
ACOM = Number of accommodations

Tentato

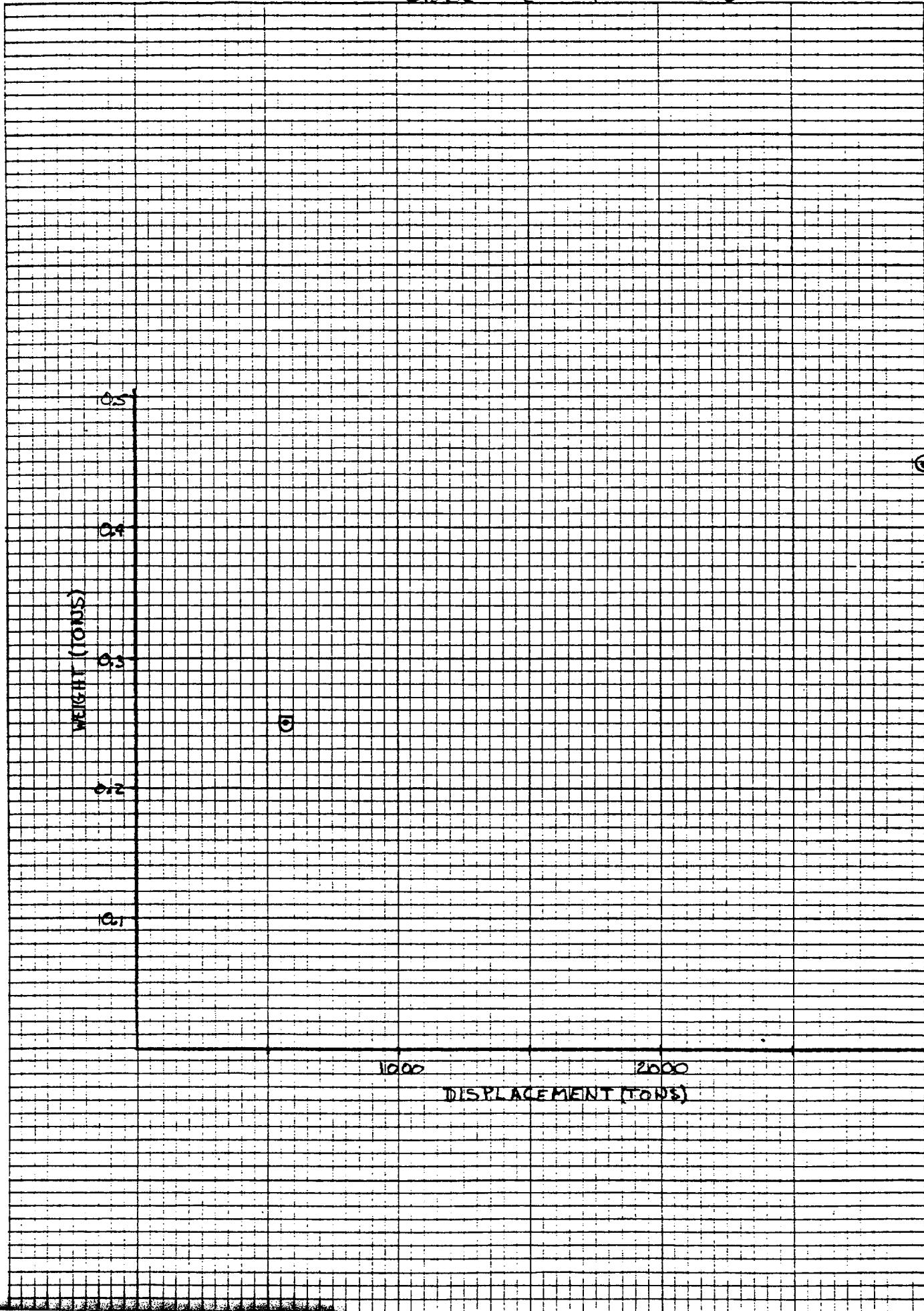
The algorithm is the same as ASSE I.

Fig 24

## W54 - REFRIGERATION



SWFS G-11F W516



521 Firemain + Sea Water Flushing System.

$$WS21 = KS21 \times VOLA \checkmark$$

$$\text{where } KS21 = .007 \text{ ft}/\text{ft}^3 \checkmark$$

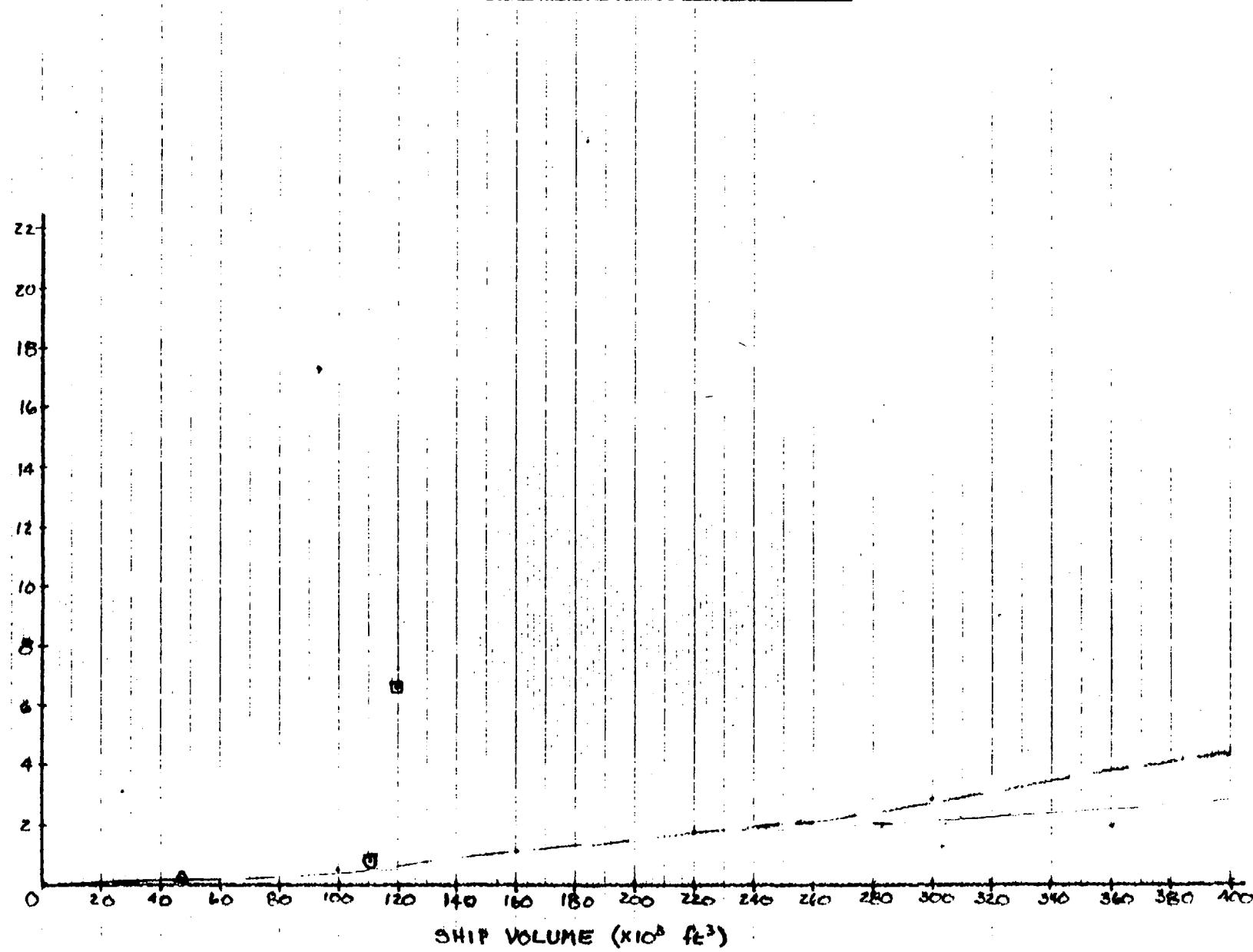
( $KS21$  is a constant based on return date  
of hydrofoils and SSSs.)

$$VOLA = \text{Total volume} \times 10^{-3}, \text{ft}^3$$

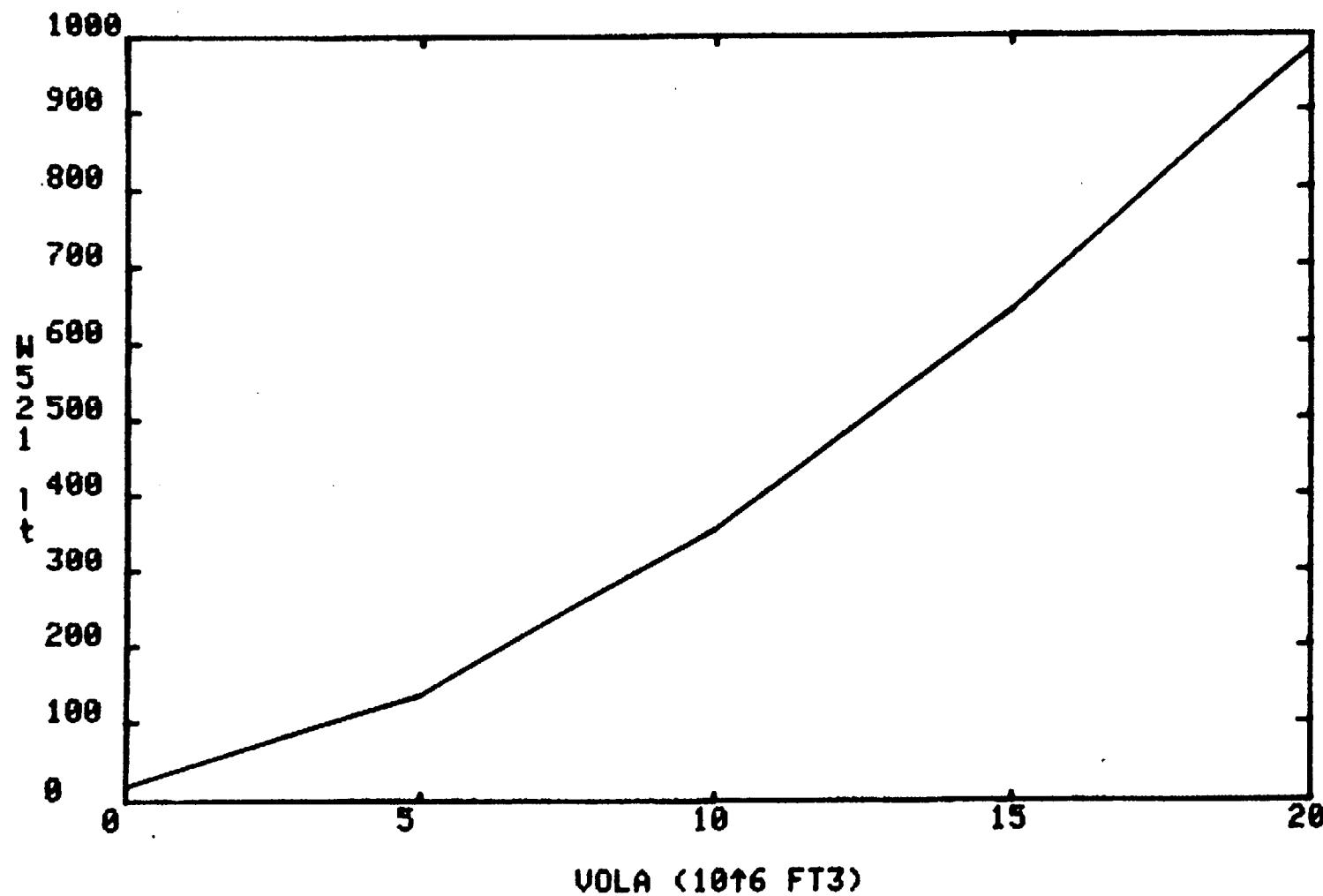
This algorithm is the same as ASSET. ✓

IT<sub>2</sub>  
FC → FA

SWDS GROUP WS21 FIREMAN AND FLUSHING SYSTEM



H521 VS VOLA AS OF 10/31/83



## ✓ 522 Sprinkler System

$$WS22 = KS22 * VOLA \checkmark$$

$$\text{where } KS22 = 6t \times 10^{-3} \text{ ft}/ft^3 \checkmark$$

(KS22 is a constant based on return weight  
of hydrants and SSES.)

$$VOLA = \text{Total Volume} = 10^{-3}, ft^3$$

## 1524 Auxiliary Sea Water System

$$WS_{24} = KS_{24} \leftarrow VOLA$$

$$\text{where } KS_{24} = .002$$

( $KS_{24}$  is a constant based on return data from hydrofoils and SESs.)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

The algorithm was created for this data base.

SEE PAGE 506

SURE CERT - WES

20

15

10

5

0

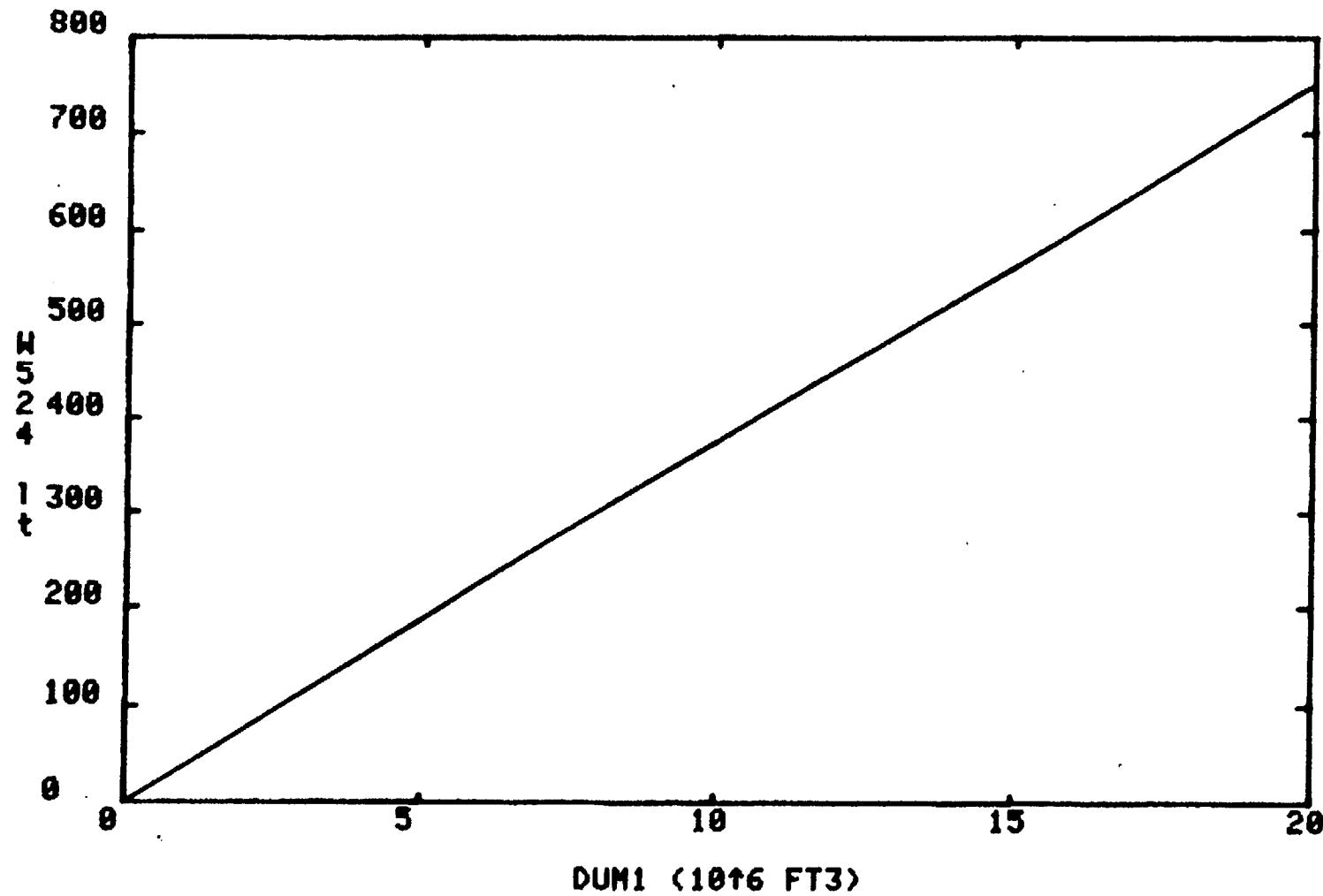
6

5

1000

2000

W524 VS DUM1 AS OF 10/31/83



SEE 36-1-52

SWELL G-1 W524

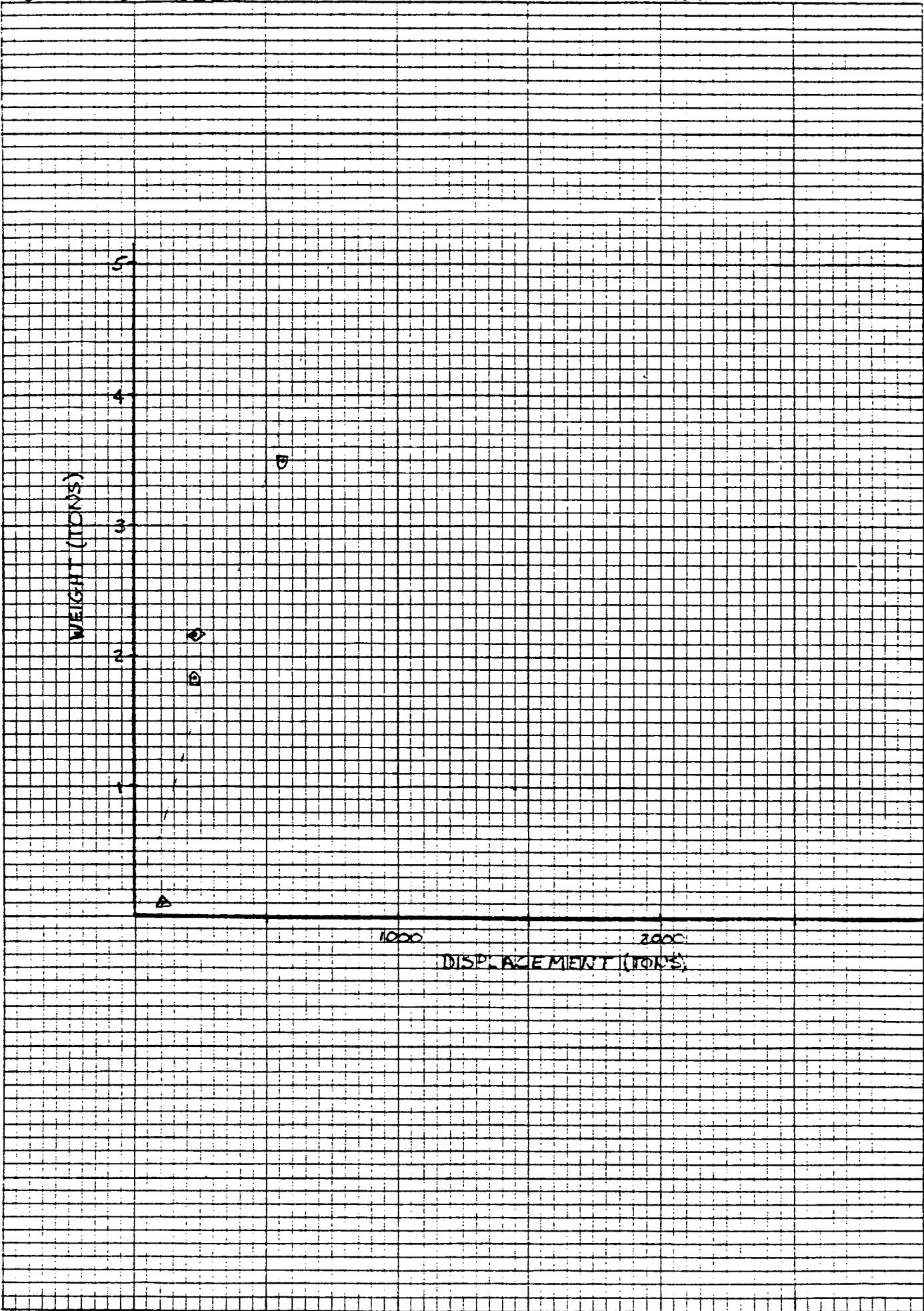


PHOTO IN IN 101 HEAVY  
10TH TIME HEAVY

J526 Scuppers + Deck Drains.

$$WS2G = K_{526} \times LCUE \times BOA \checkmark$$

$$\text{where } K_{526} = 1.15 \times 10^{-5} \text{ ft/s}^3 \checkmark$$

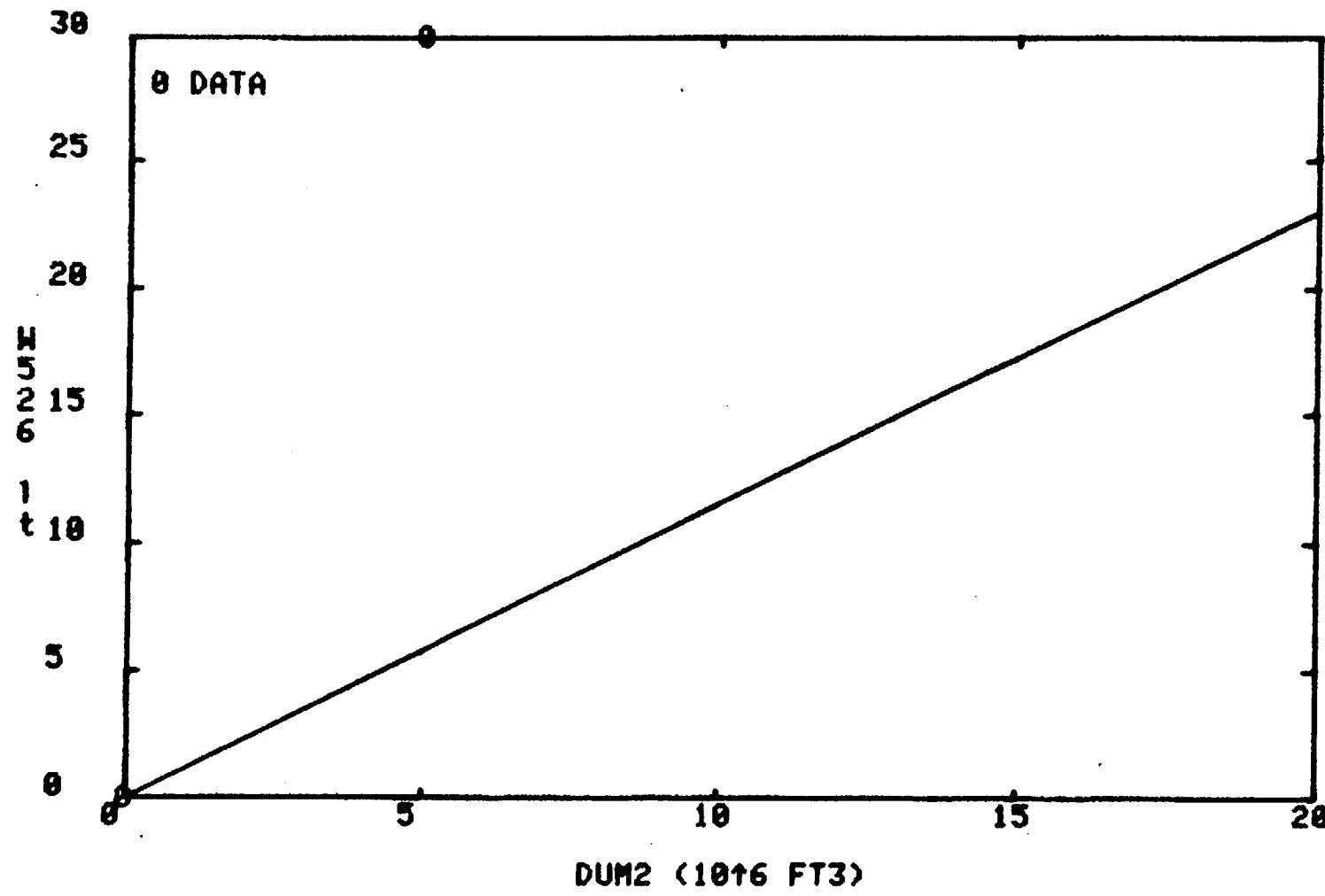
( $K_{526}$  is a constant based on return data from hydrofoils and SESs.)

~~LCUE~~ = Cumulative length, ft

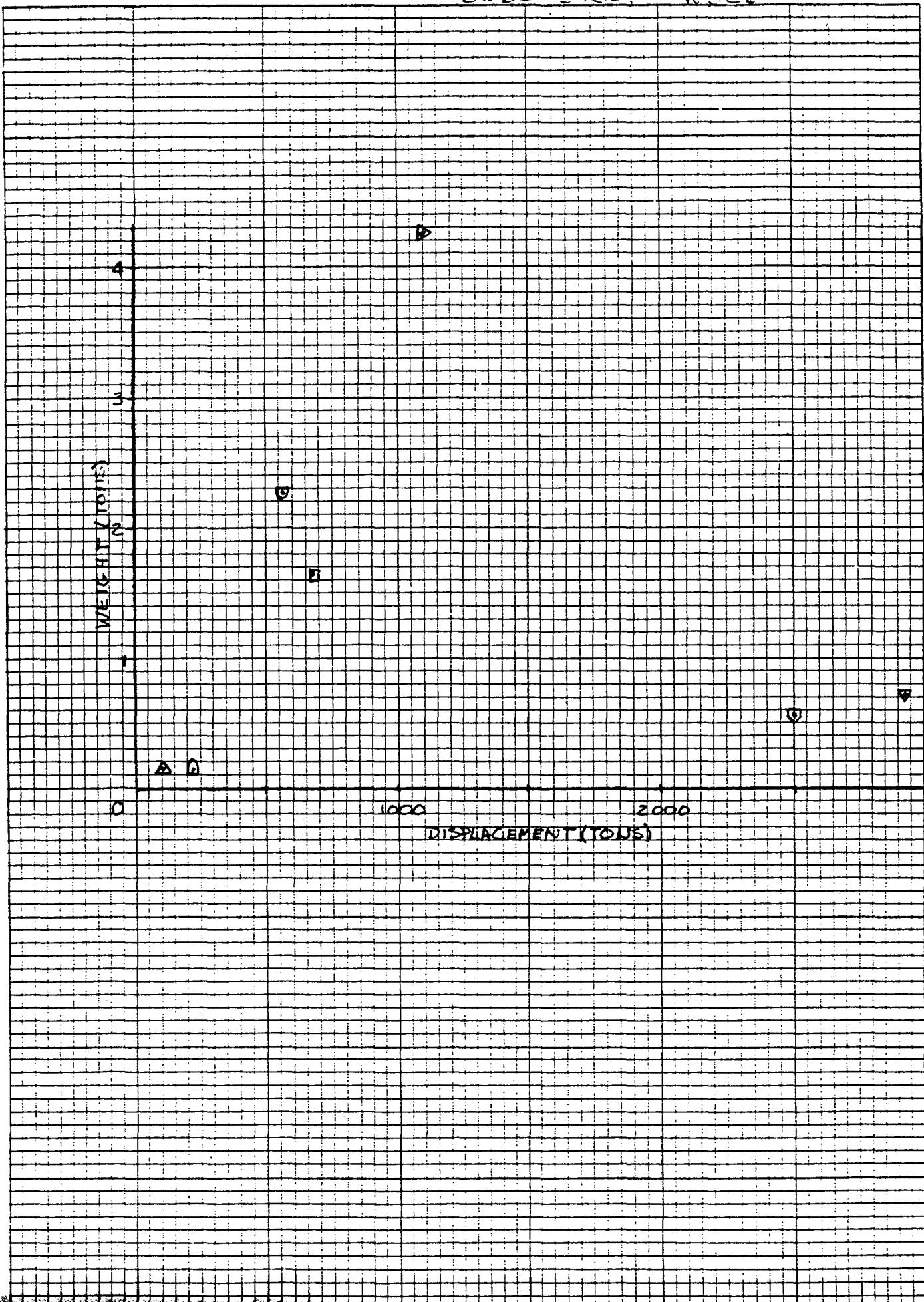
BOA = Beam Overall, ft

The algorithm is the same as ASSET.

H526 VS DUM2 AS OF 10/31/83



SWES GROUP WELD



↓ 528 Plumbing Drainage

$$WS28 = KS28 \times VOLA$$

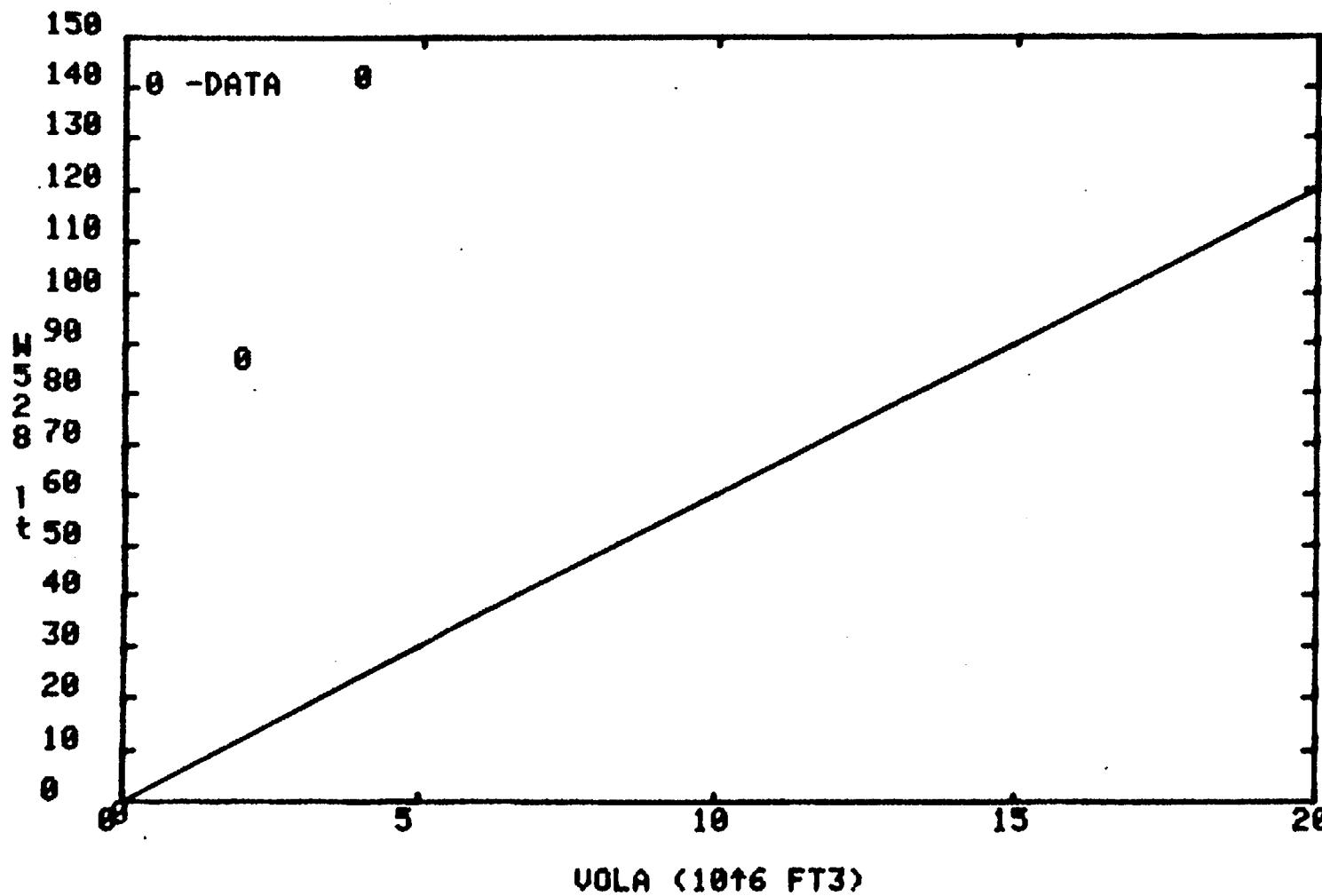
$$\text{where } KS28 = .014 \text{ ft/f}^3 \checkmark$$

( $KS28$  is based on return data from hydrofoils and SSTs)

$$VOLA = \text{Total volume} \times 10^{-3}, \text{ ft}^3$$

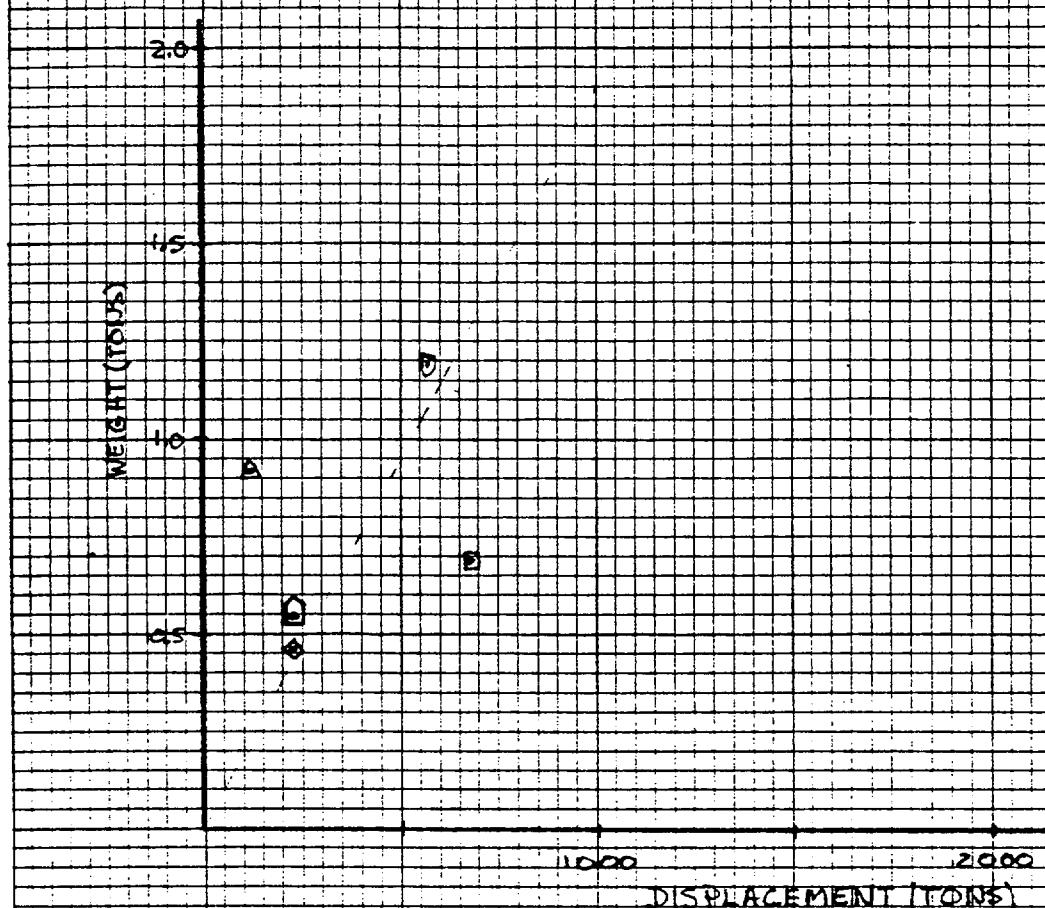
This algorithm is the same as ASSET. ✓

N528 VS VOLA AS OF 10/31/83



SEE REVERSE SIDE

SUMMER - 1952



REPRODUCED BY GOVERNMENT EXPENSE  
IN THE INTEREST OF PUBLIC SAFETY

✓ 529 Draining + Ballasting System

$$W_{529} = K_{529} * VOLA \checkmark$$

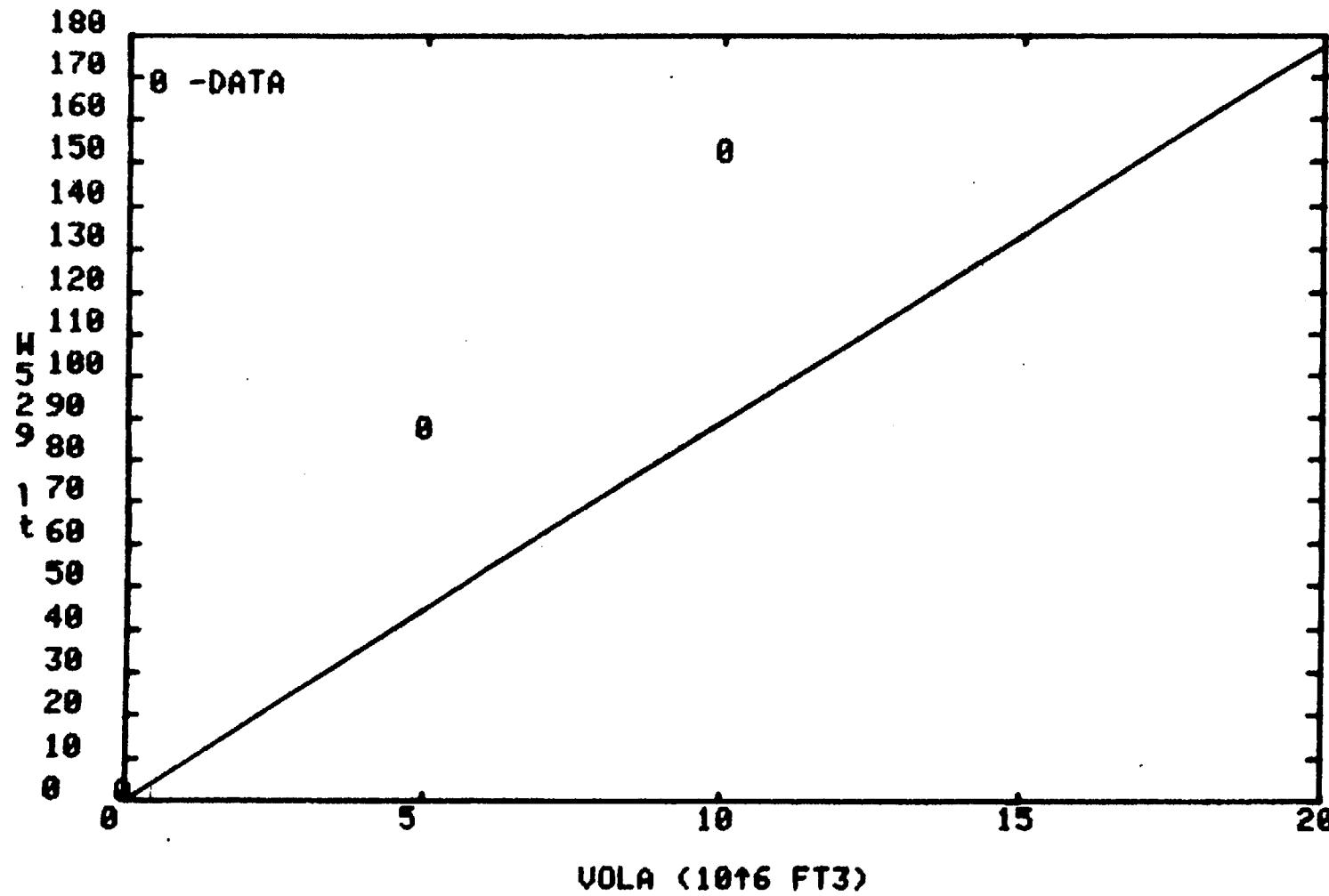
where  $K_{529} = .0045 \text{ ft}/\text{ft}^3$

( $K_{529}$  is based a constant based on return  
data of hydrofoils and SBSs).

$VOLA = \text{Total volume} \times 10^{-3}, \text{ ft}^3$

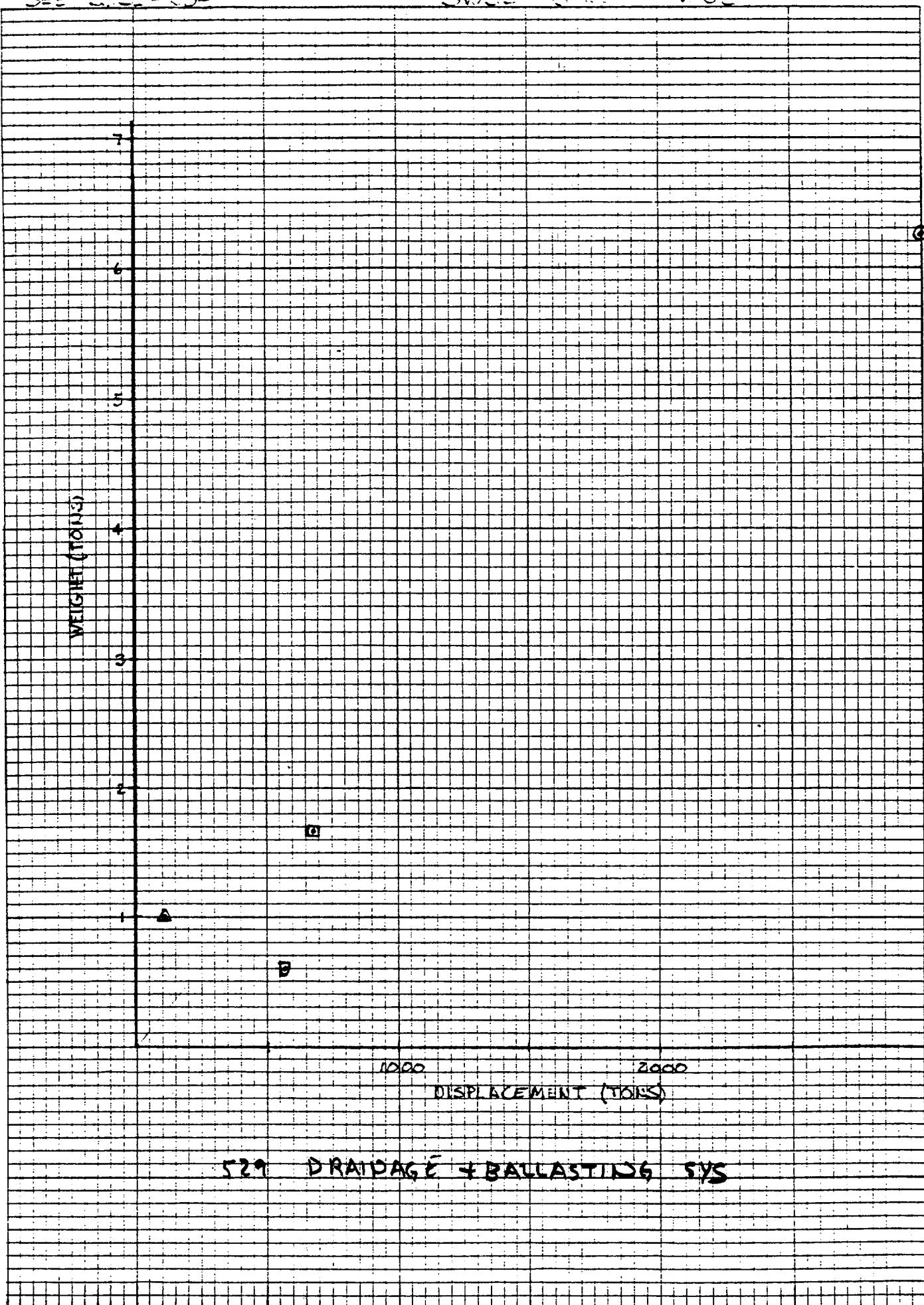
This algorithm is the same as ASSET. ✓

W529 VS VOLA AS OF 10/31/83



SEE PAGE 502

SWISS GEAR V 520



529 DRAWDOWN + BALLASTING SY

# $\sqrt{531}$ Distilling Plant

$$WS31 = \frac{KS31}{\text{ACOM}} \downarrow$$

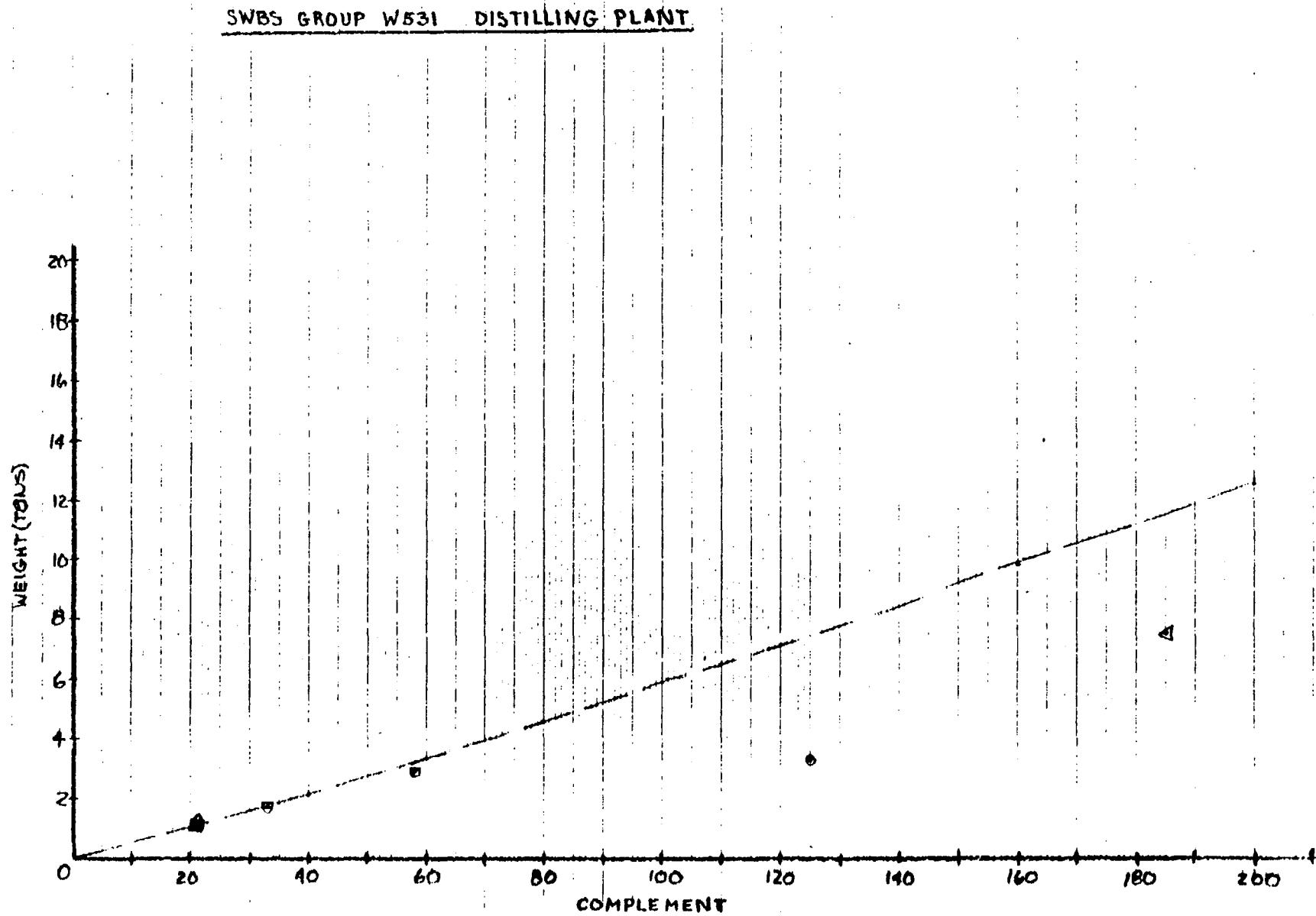
where  $KS31 = .054 \text{ ft} \downarrow$

( $KS31$  is a constant based on return data  
of hydrofuels and SESs.)

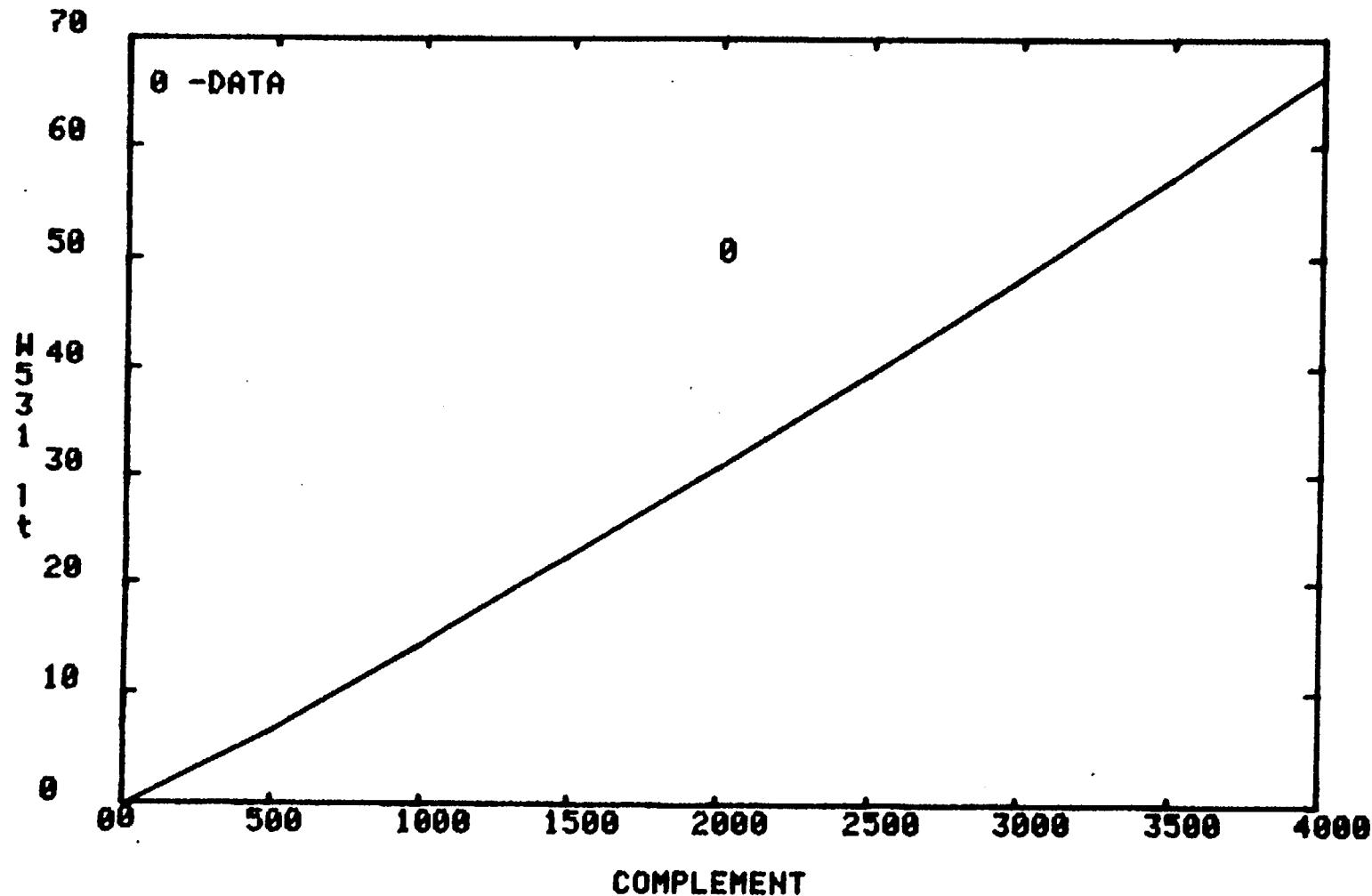
$ACOM = \text{Number of Accommodations}$

This algorithm is the same as ASSET,  $\checkmark$

ITEN  
 $EC \rightarrow EA$

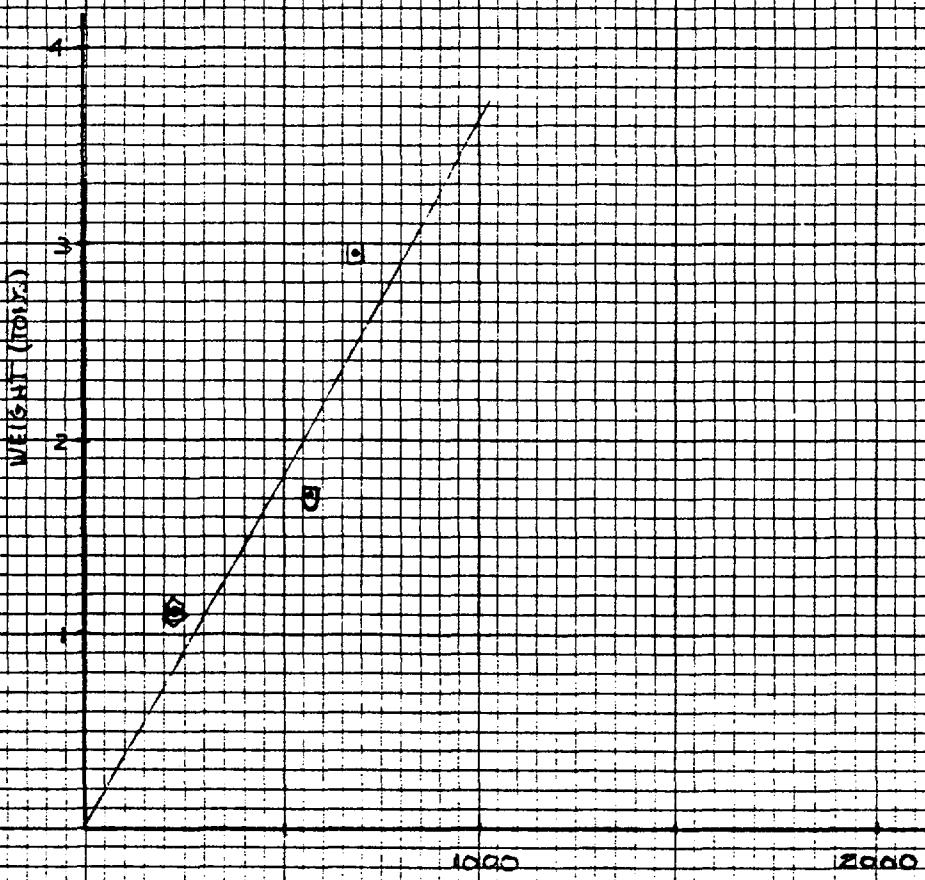


W531 VS COMPLEMENT AS OF 10/31/83



SEE I - E-57

SWE: ERNST WES



✓S32 Cooling Water

$$WS32 = KS32 * W400 \checkmark$$

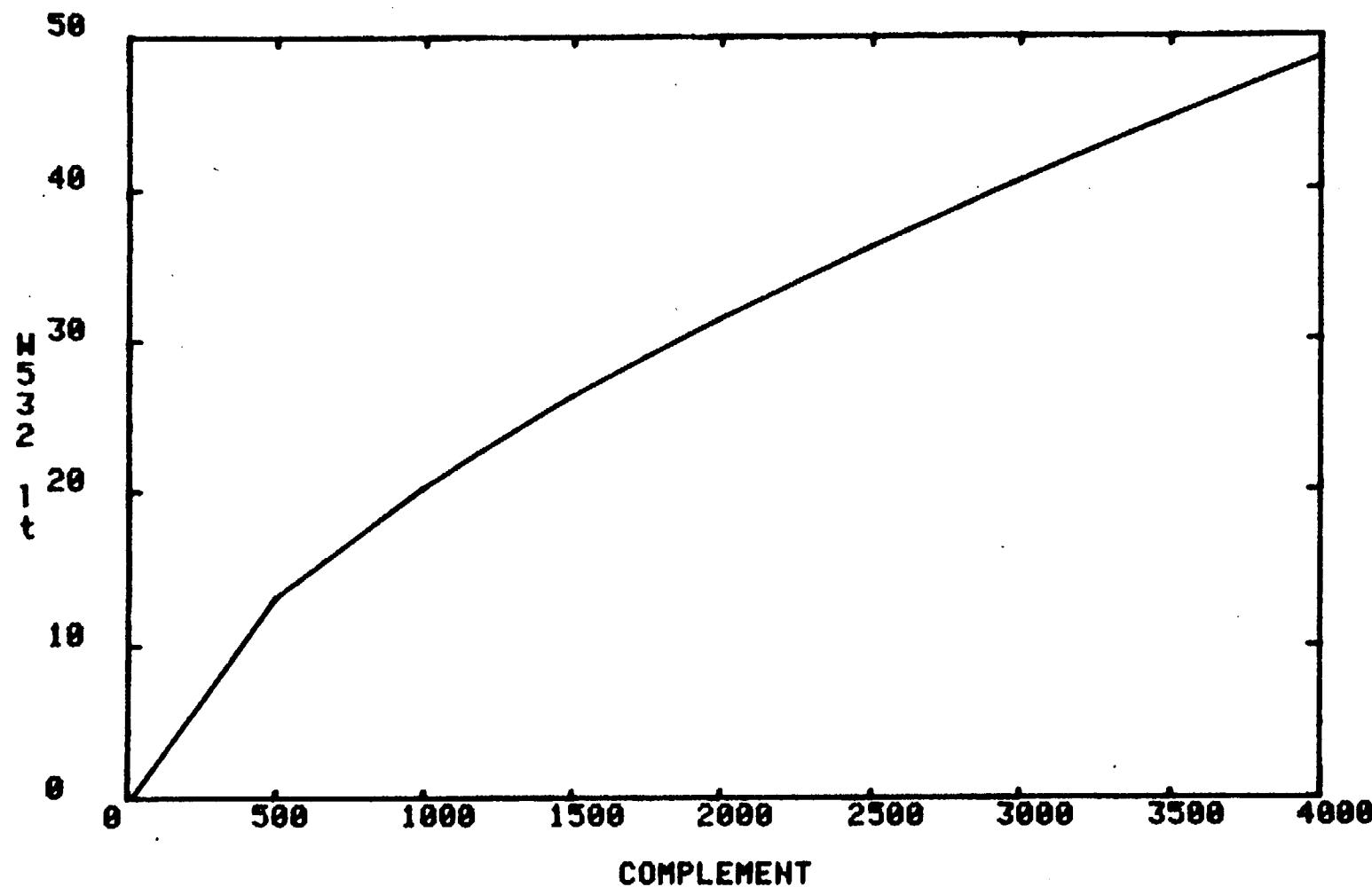
where  $KS32 = .04 \checkmark$  (ASSET)

$W400 = \text{Command + Surveillance Weight, lb}$

This algorithm is the same as ASSET,

ITENY  
 $\epsilon C \rightarrow \epsilon A$

W532 VS COMPLEMENT AS OF 10/31/83



SWES GROVE W 532

WEIGHT (TONS)

10

1000

2000

FROM ONE TO 1 INCH  
THIN LINE DRAWING

## S33 Potable Water

$$W_{S33} = K_{S33} \times A_{COM}$$

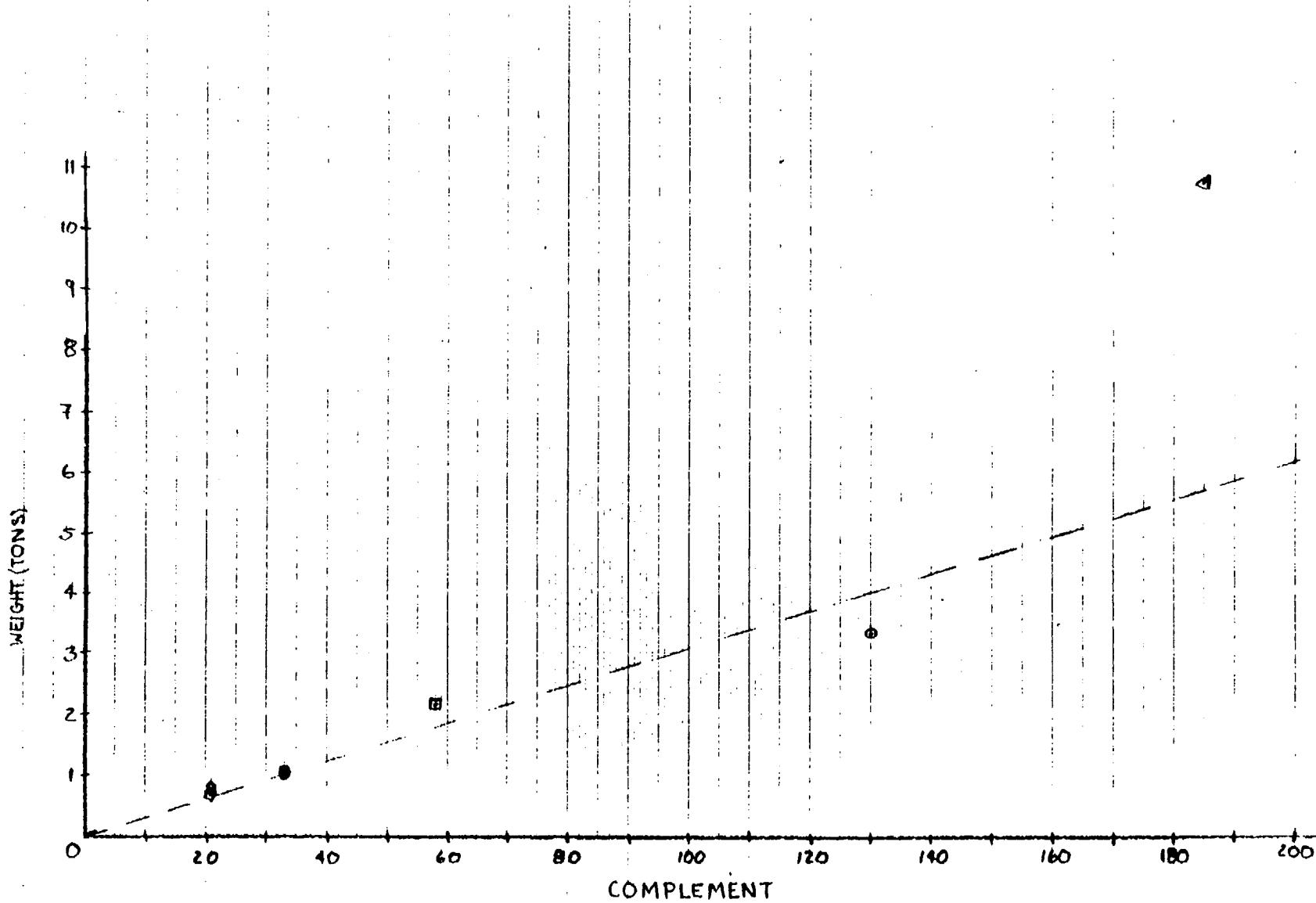
where  $K_{S33} = 1.03$  &  $A_{COM}$  ~~( $\sqrt{A_{COM}}$ )~~

$A_{COM}$  = Number of Accommodations

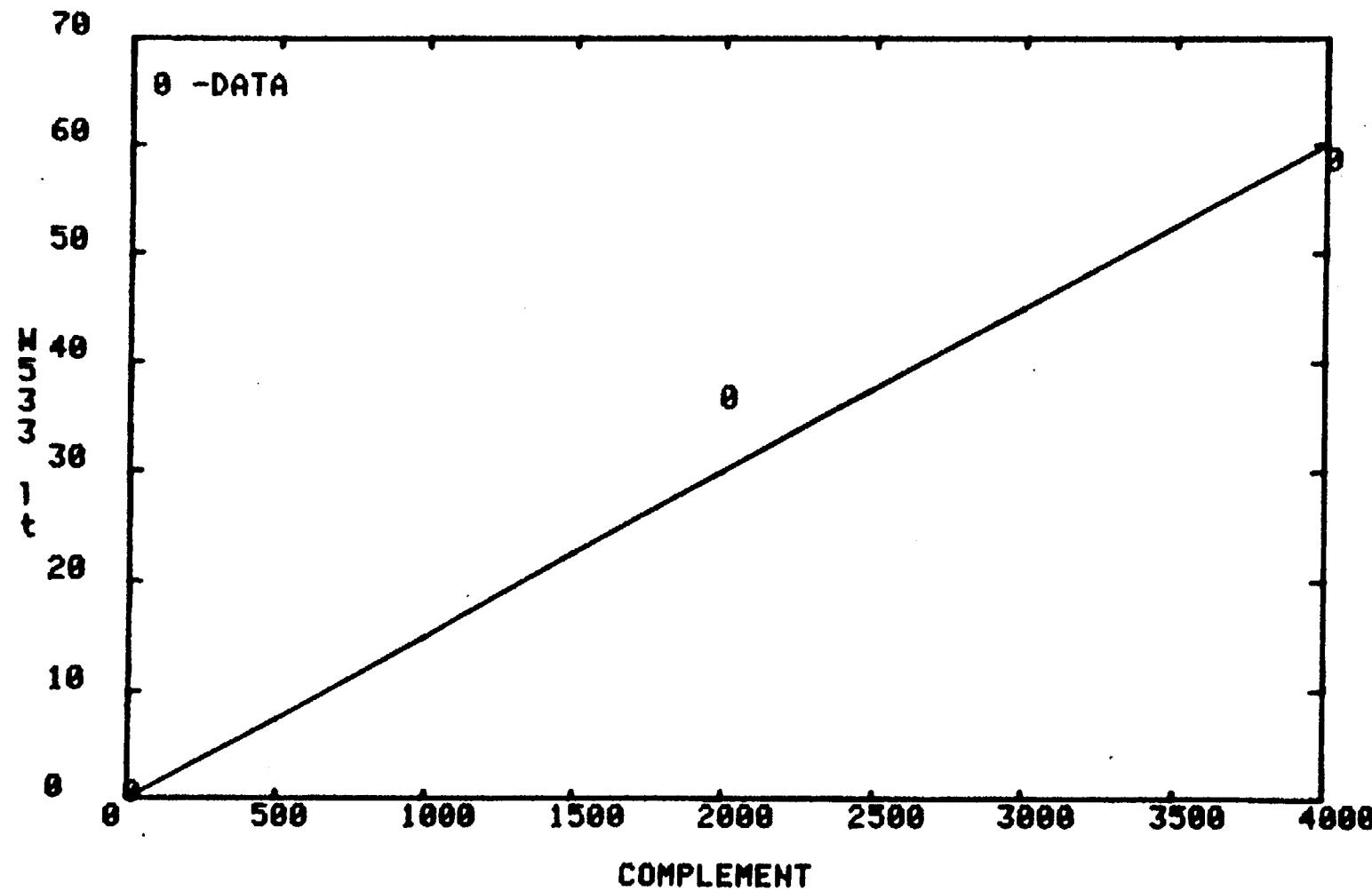
The algorithm is ~~the same as~~ ASSET,

The constant ( $K_{S33}$  is a constant based on return data of hydrofoile and SSS.)

SWBS GROUP W533 POTABLE WATER

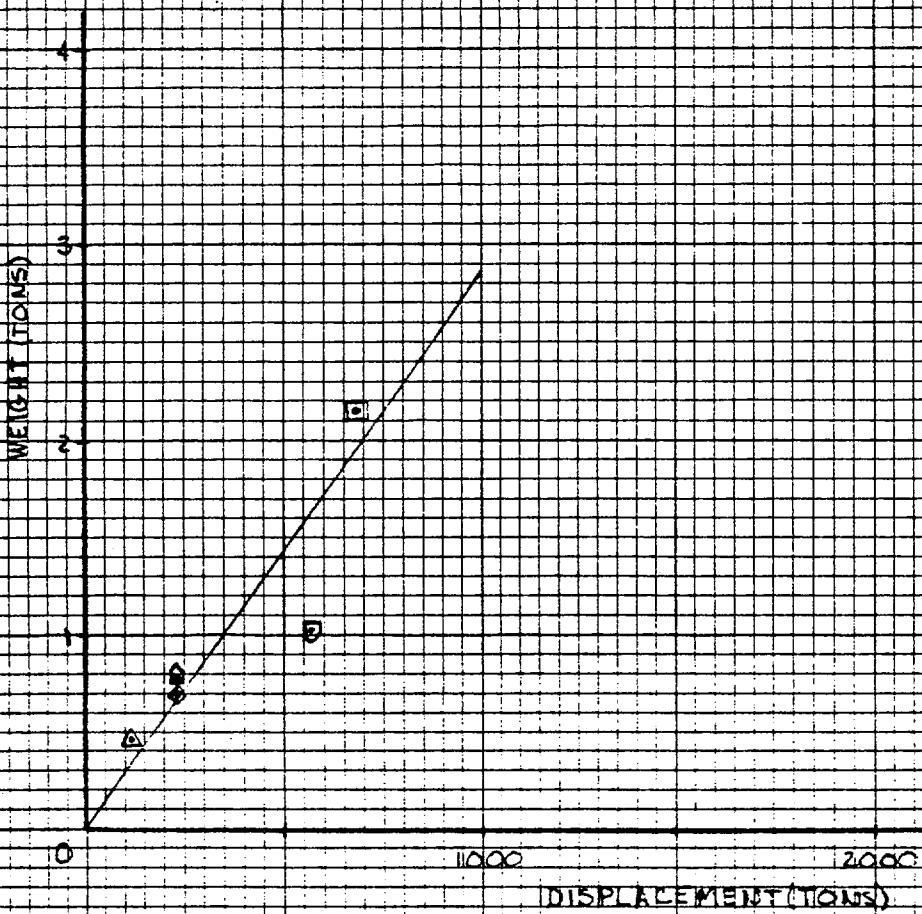


W533 VS COMPLEMENT AS OF 10/31/83



SEE BL  $\angle = 50^\circ$

SWES SPOTTE W533



FROM 10 TO 1 INCH  
WITH THE HEAVY

## 1541 Ship Fuel & Fuel Compensating System

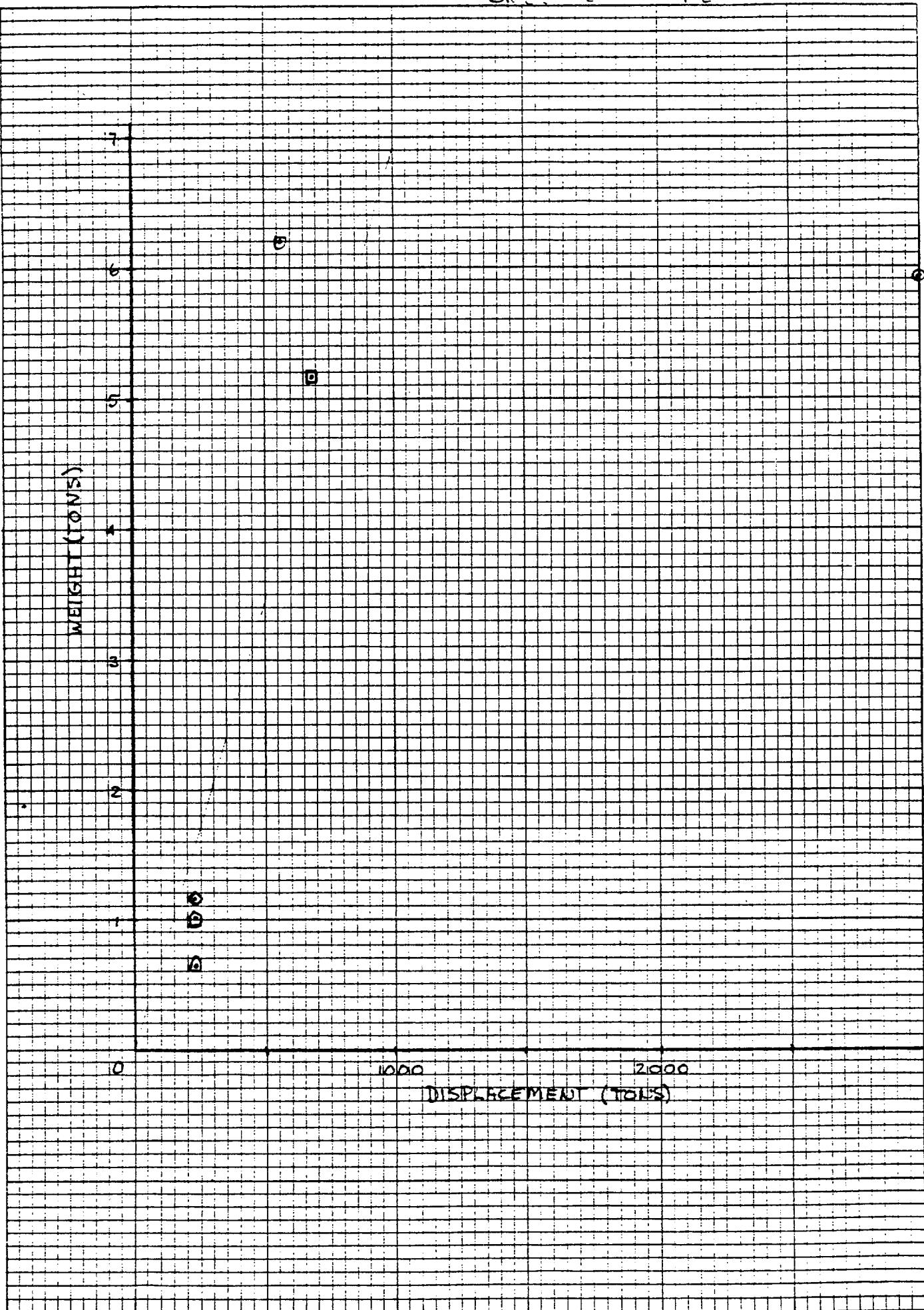
$$WS41 = KS41 \bullet WF41 \checkmark$$

where  $KS41 = .05V$

(  $KS41$  is a constant based off return data from hydrofoils and SESs.)

$WF41$  = Endurance Fuel Level, lt

The algorithm is the same as ASSET. ✓



✓ 542 Aviation + General Purpose Fuels

$$WS42 = KS42 * WF42 \checkmark$$

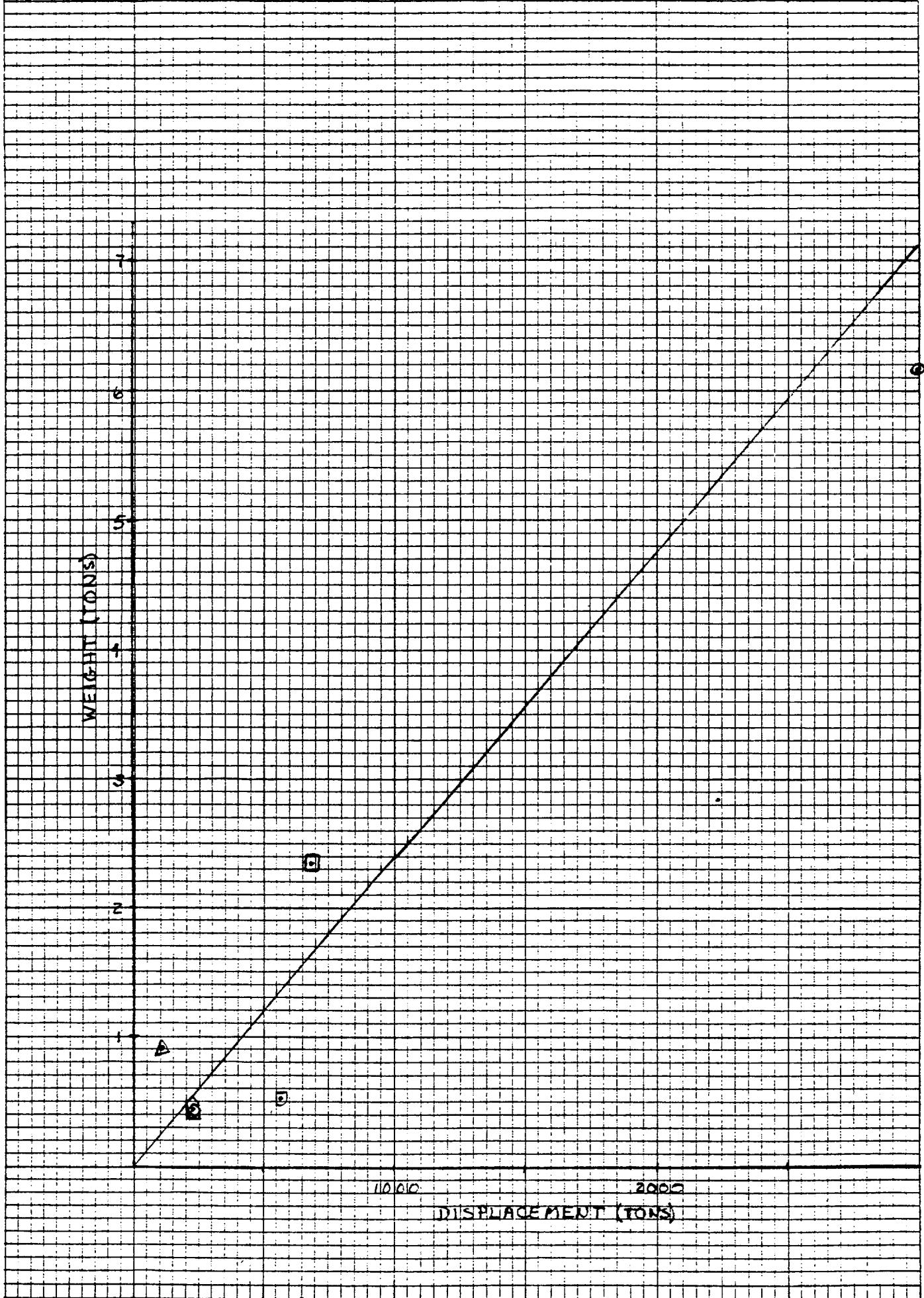
where  $KS42 = .049$  ✓ (ASSET) ✓

$WF42 = \text{Aviation Fuel Load, lt}$

The algorithm is the same as ASSET, ✓

SEE : SITE

SWEET SITE WSC



COMPRESSED AIR SYS

## SSI Compressed Air System

$$WSSI = \underline{KSSI} \cdot VOLA$$

where  $KSSI = .0244 \frac{\text{ft}^3}{\text{ft}^2}$  (ASSET)

$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$

The algorithm is same as ASSET.

KSSS Fine Extinguishing System

$$W_{SSS} = KSSS \times VOLA$$

where  $KSSS = .027 \text{ ft/s}^3$  (ASSET)

$VOLA = \text{Total Volume} \times 10^{-3}, \text{ft}^3$

The algorithm is the same as ASSET,

SWE-455 - 555

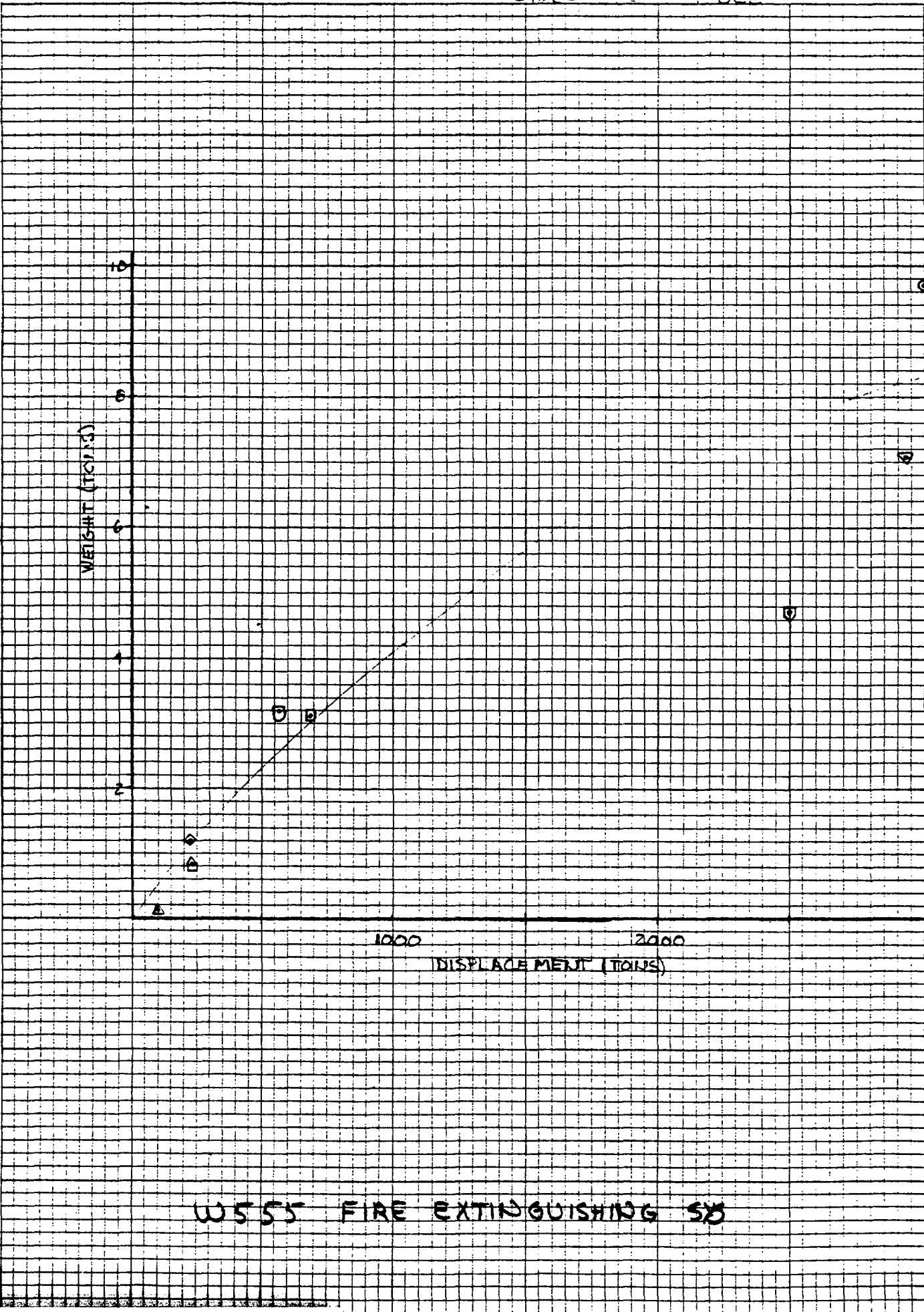
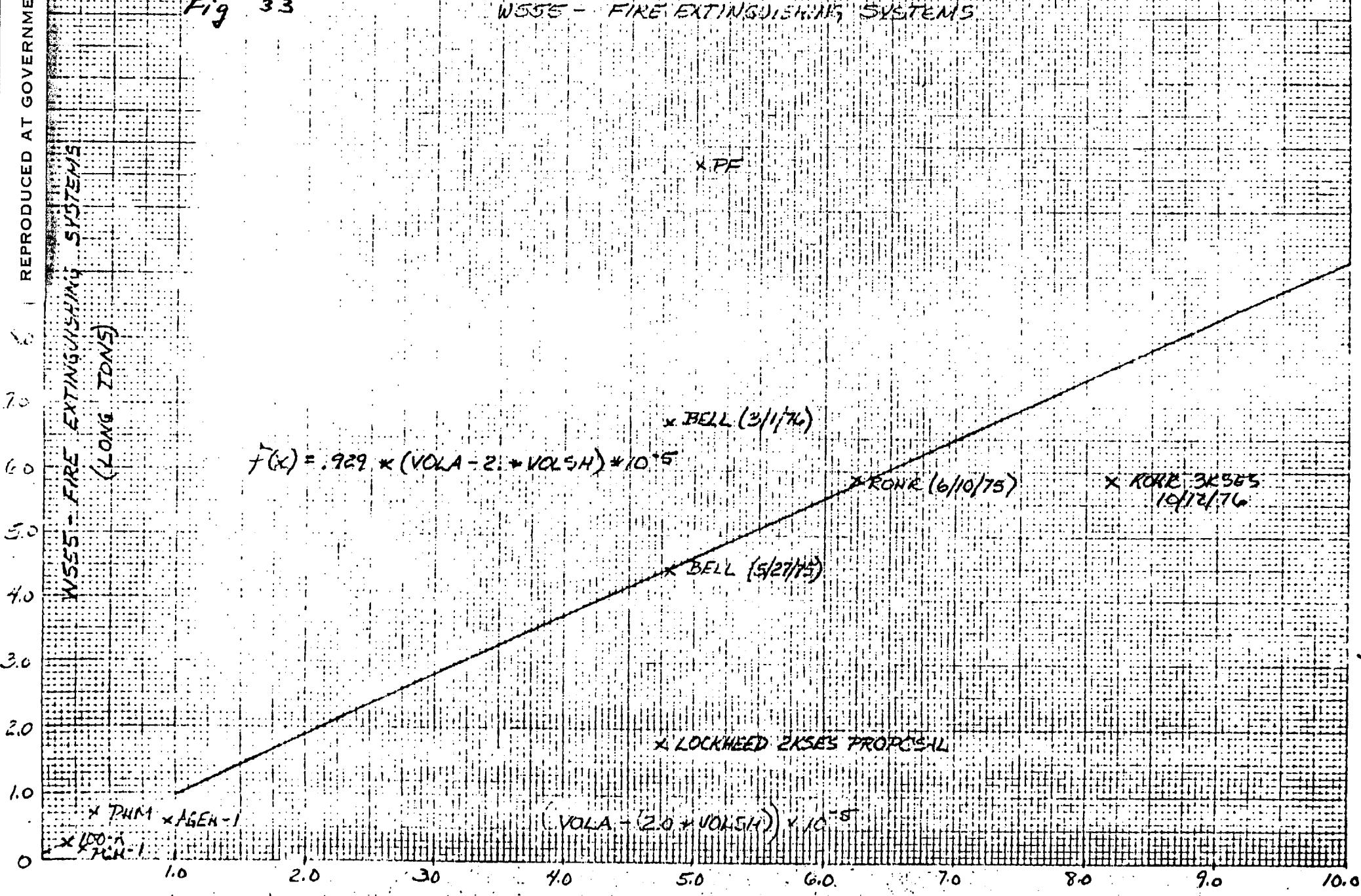


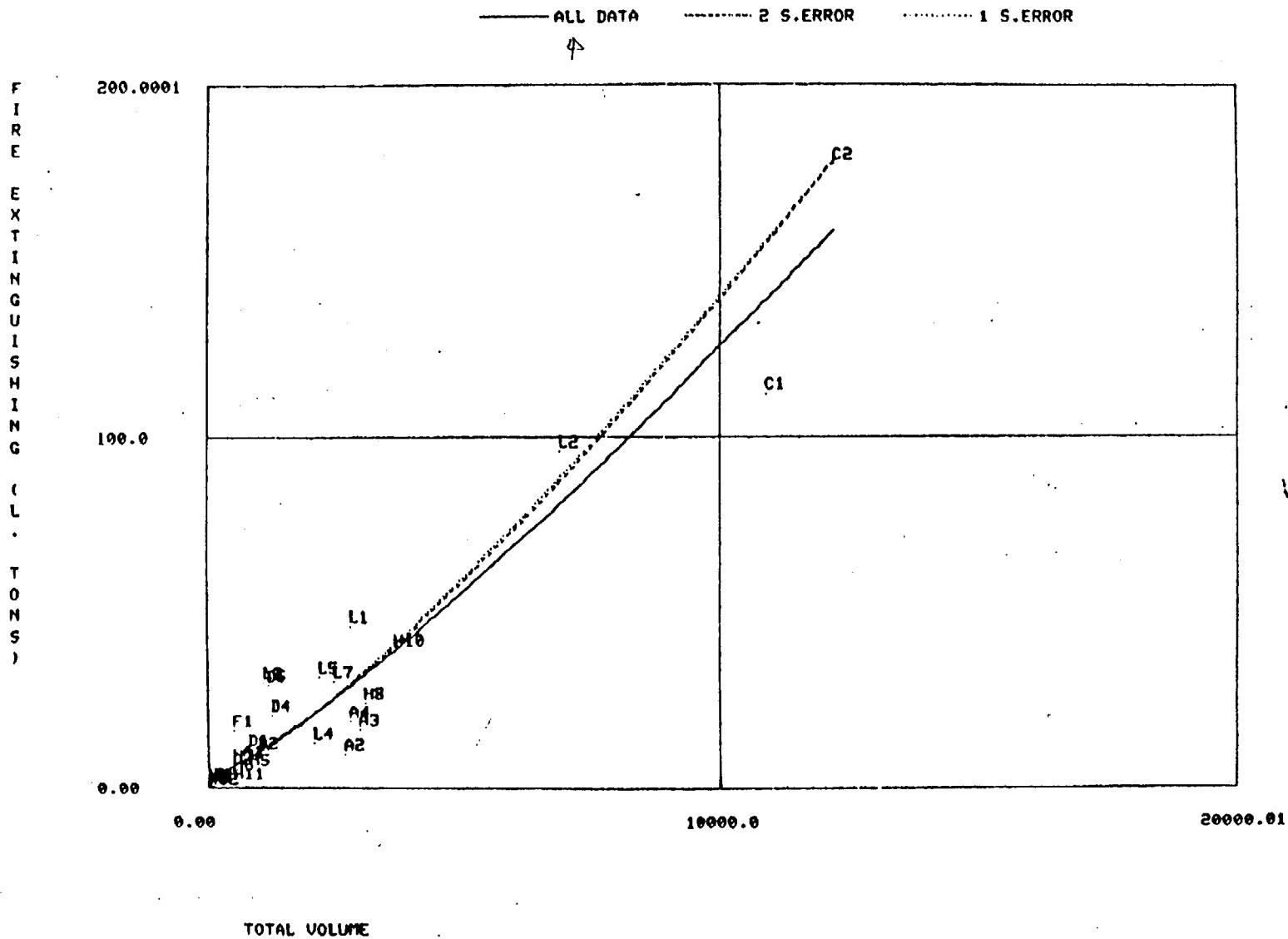
Fig. 33

## W505 - FIRE EXTINGUISHING SYSTEMS

X K1 4/B



PAUSE 'PRESS (RETURN) TO CONTINUE'  
SUBS 555 FIRE EXTINGUISHING SYSTEMS (BSCI 507)



W556 - HYDRAULIC FLUID SYSTEM  
(LONG TONS)

Fig. 34

W556 - HYDRAULIC FLUID SYSTEM

LOCKED PLATES  
PROPOSAL

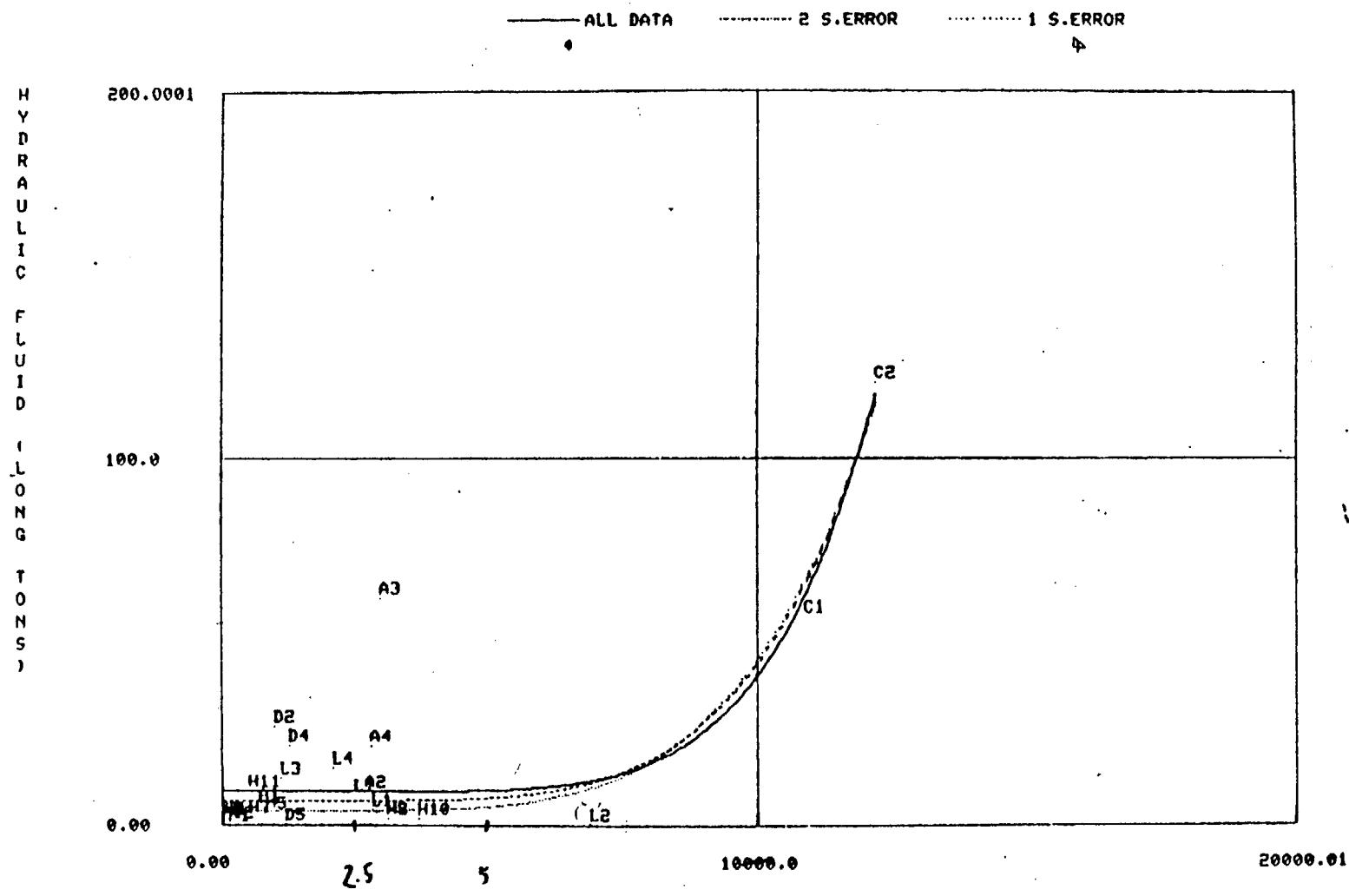
X H/HB  
X ROHR (6/075) X ROHR 3/085  
X BBL (3/175)

$$F(x) = 16 + 1453 * (\tan 1 - 2.0 * \cos x) * 10^{-5}$$

XSES-1001  
2MM

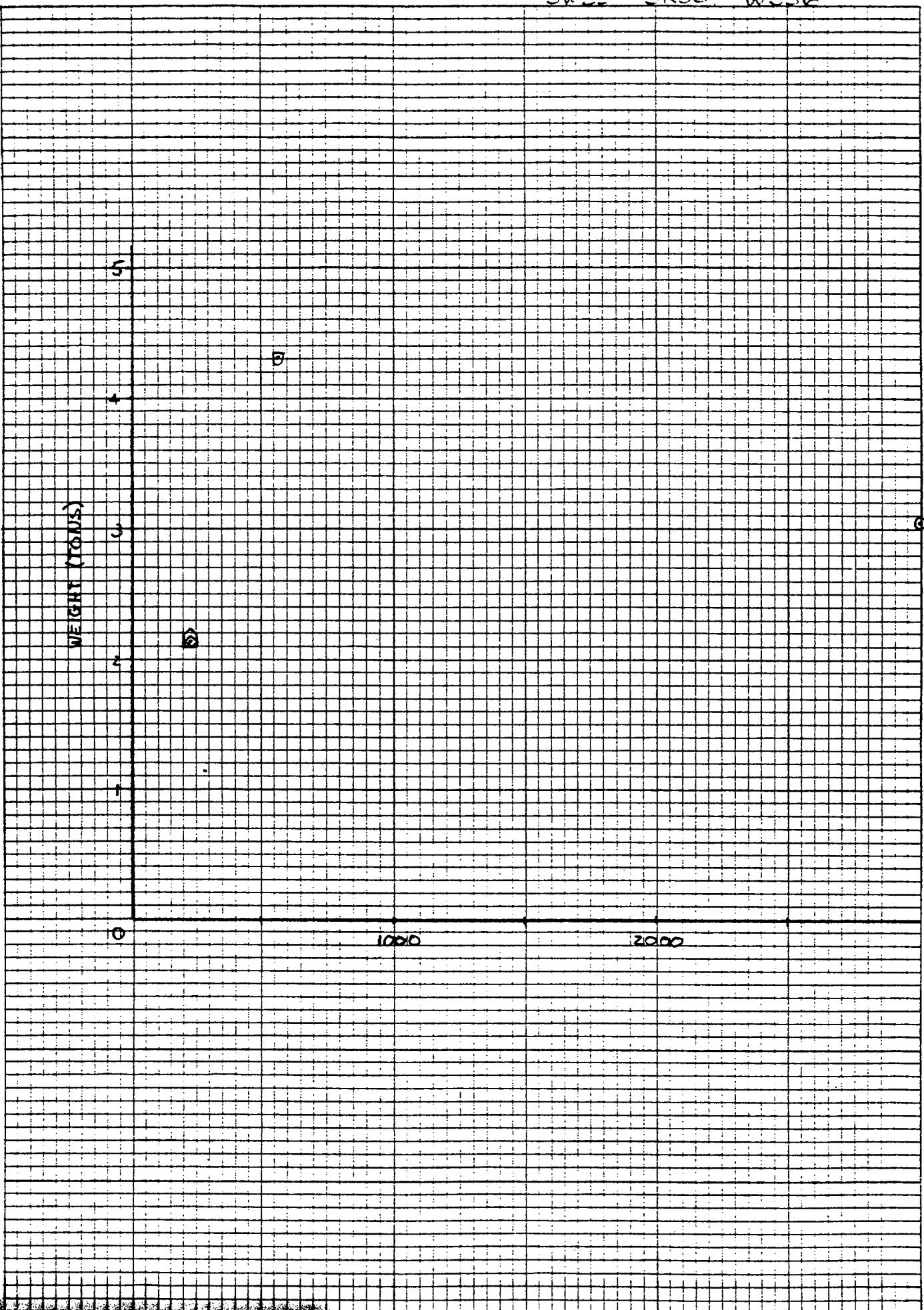
10.0 9.0 8.0 7.0 6.0 5.0 4.0 3.0 2.0 1.0 0.0  
10.0 9.0 8.0 7.0 6.0 5.0 4.0 3.0 2.0 1.0 0.0

## SUBS 556 HYDRAULIC FLUID SYSTEM (BSCI 516)



-6  
x10

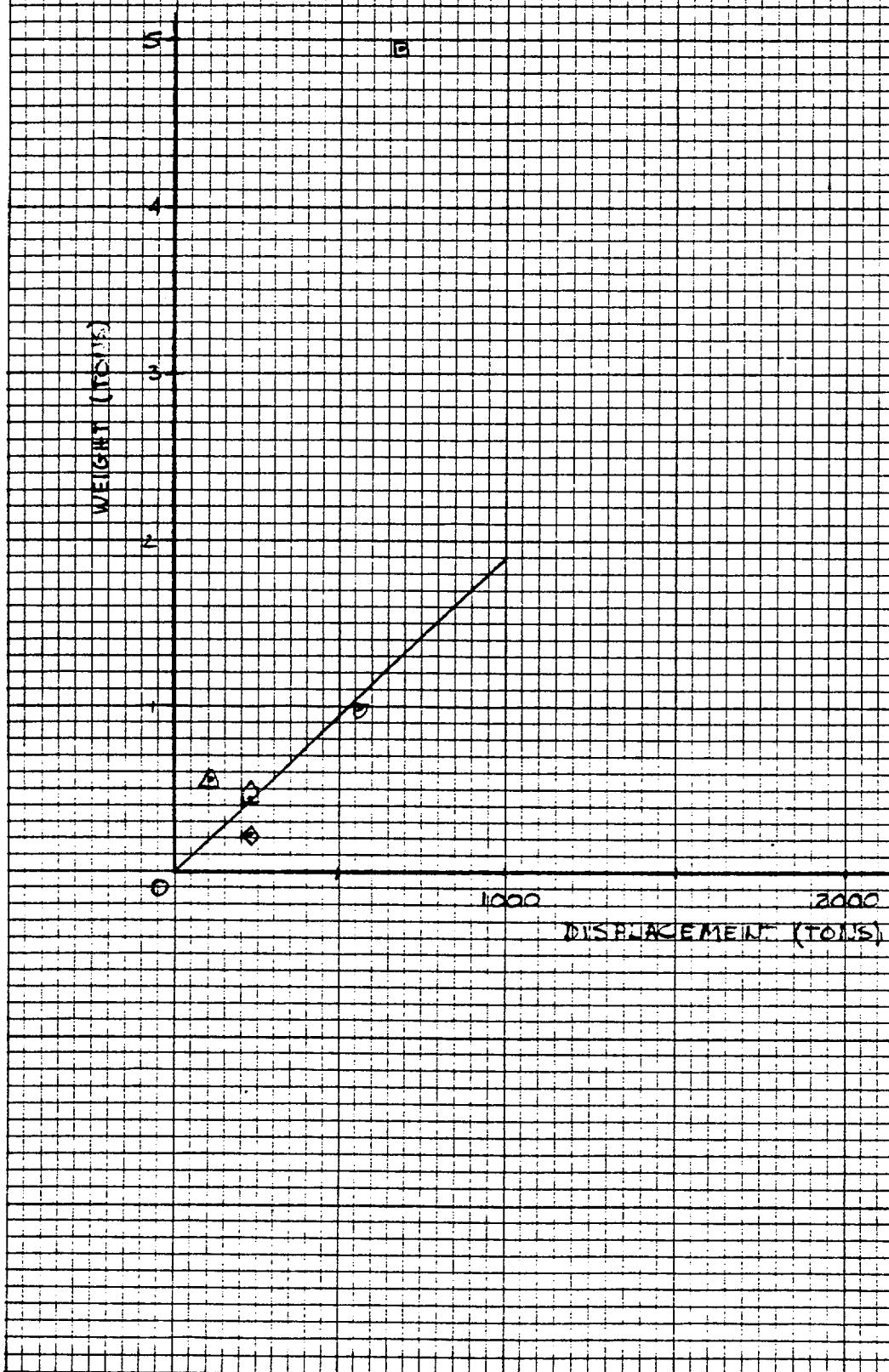
SWEET GROUSE W556



PRINTED ON X TO 1 INCHES  
10TH LINE HEAVILY

SEE

SWB ERODE W 56



## SG1 Steering Systems

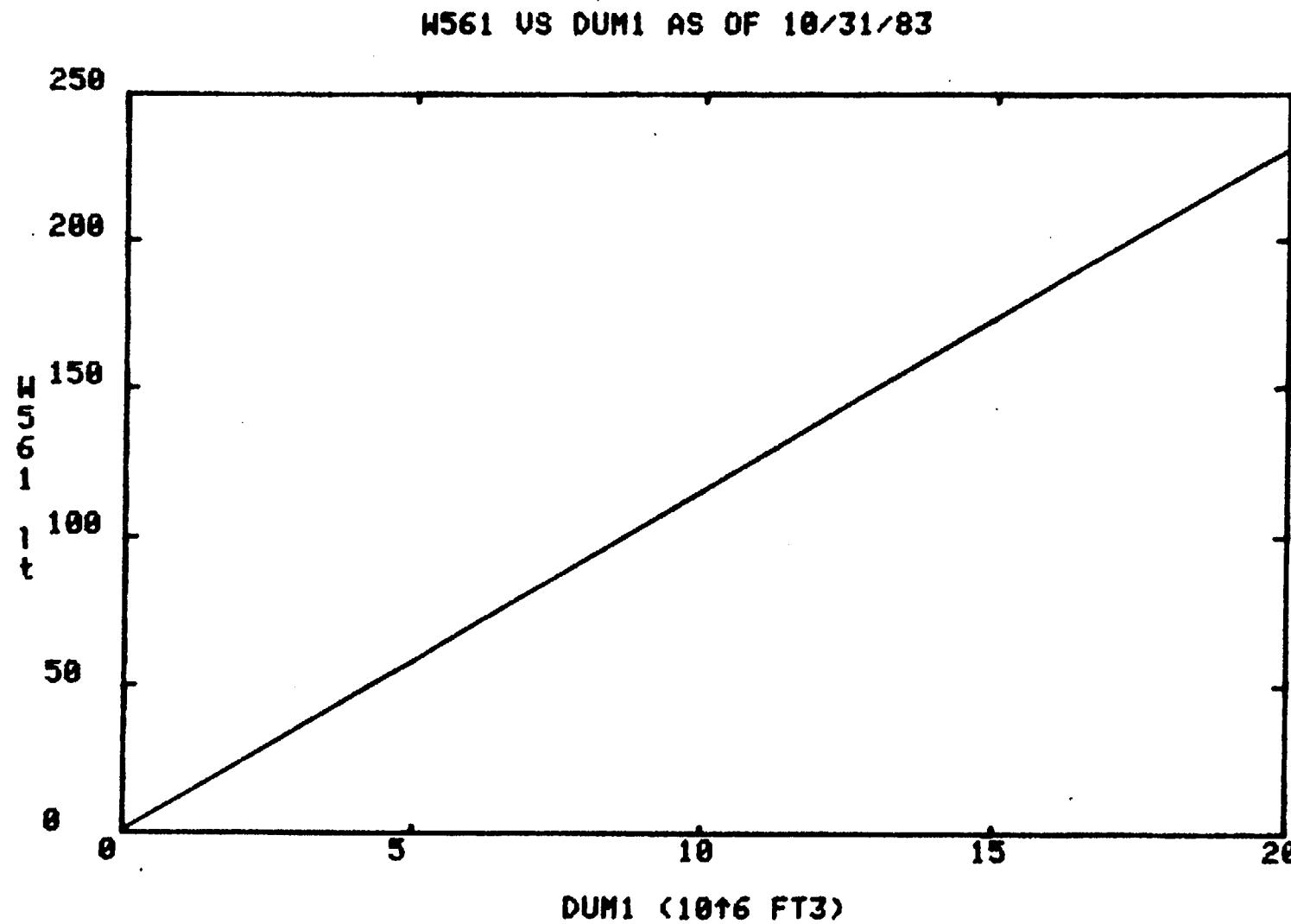
$$WSG1 = KS61 * VOLA$$

where  $KS61 = .0075 \text{ lb/ft}^3$

( $KS61$  is a constant based on return weight of hydrofoils and SESS.)

$$VOLA = \text{Total volume} \times 10^{-3}, \text{ ft}^3$$

This algorithm is ~~the same as~~ based on weight resolution of CONFORM designs.



562 Rudder -

$$WSL = KS62 \times VOLA$$

$$\text{where } KS62 = .0079 \frac{\text{ft}}{\text{ft}^3}$$

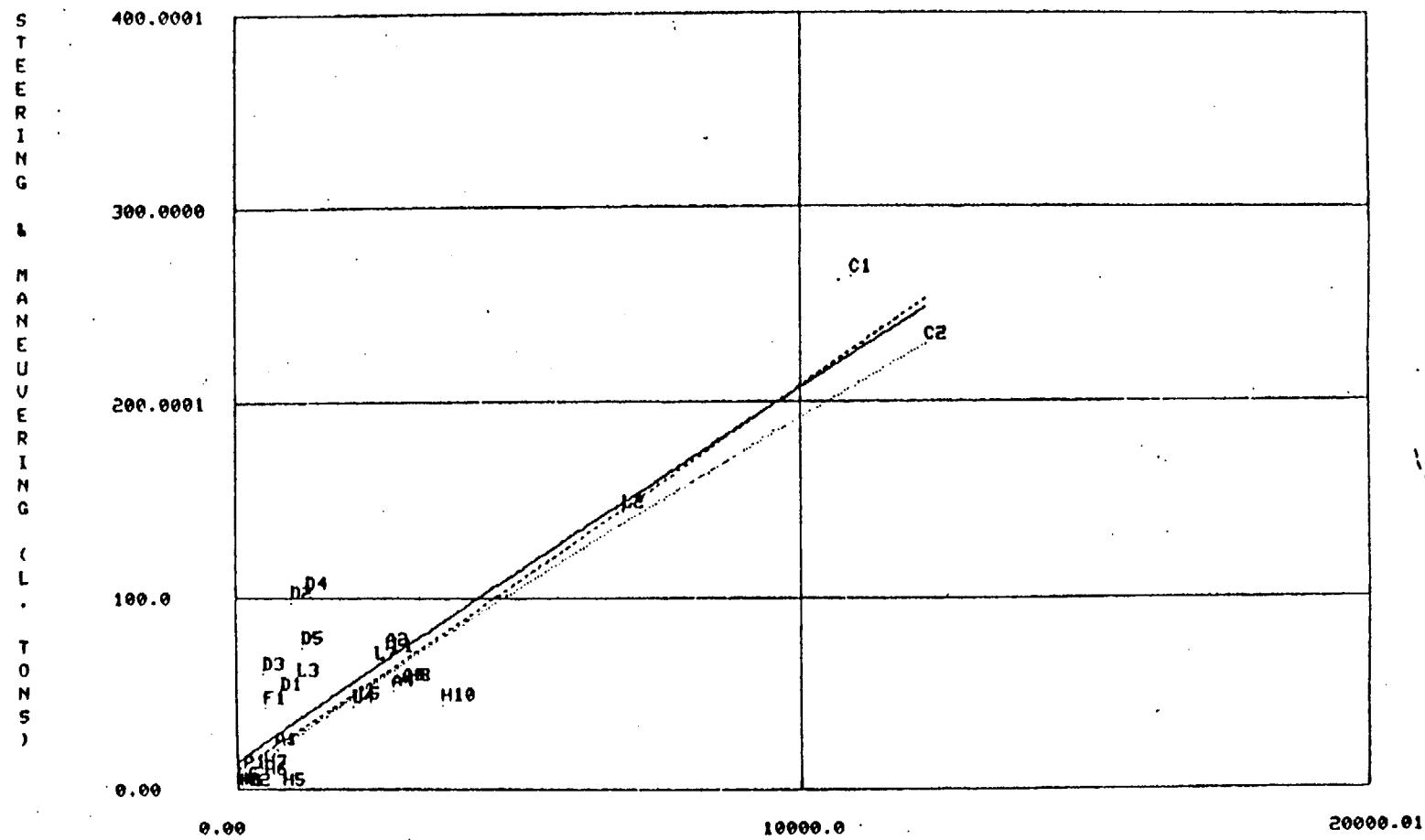
(KS62 is a constant based on recommendations of hydrofoils and STSS.)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ft}^3$$

The algorithm is based on 561 algorithm.

## SUBS 561/2/8 STEERING MANEUVERING (BSC1 518/9)

— ALL DATA —— 2 S.ERROR —— 1 S.ERROR



TOTAL VOLUME

Fig. 35

WIGOL 128 + STEERING CONTROL RUDDERS, MANUFACTURING SYSTEMS

xH141b

## WATER JETS w/o RUDDERS

x BELL (3/17/70)

x EELC (5/27/75)

$$T(x) = B + 1.5 \cdot VOLA \cdot 10^{-5}$$

$$VOLA \cdot 10^{-5}$$

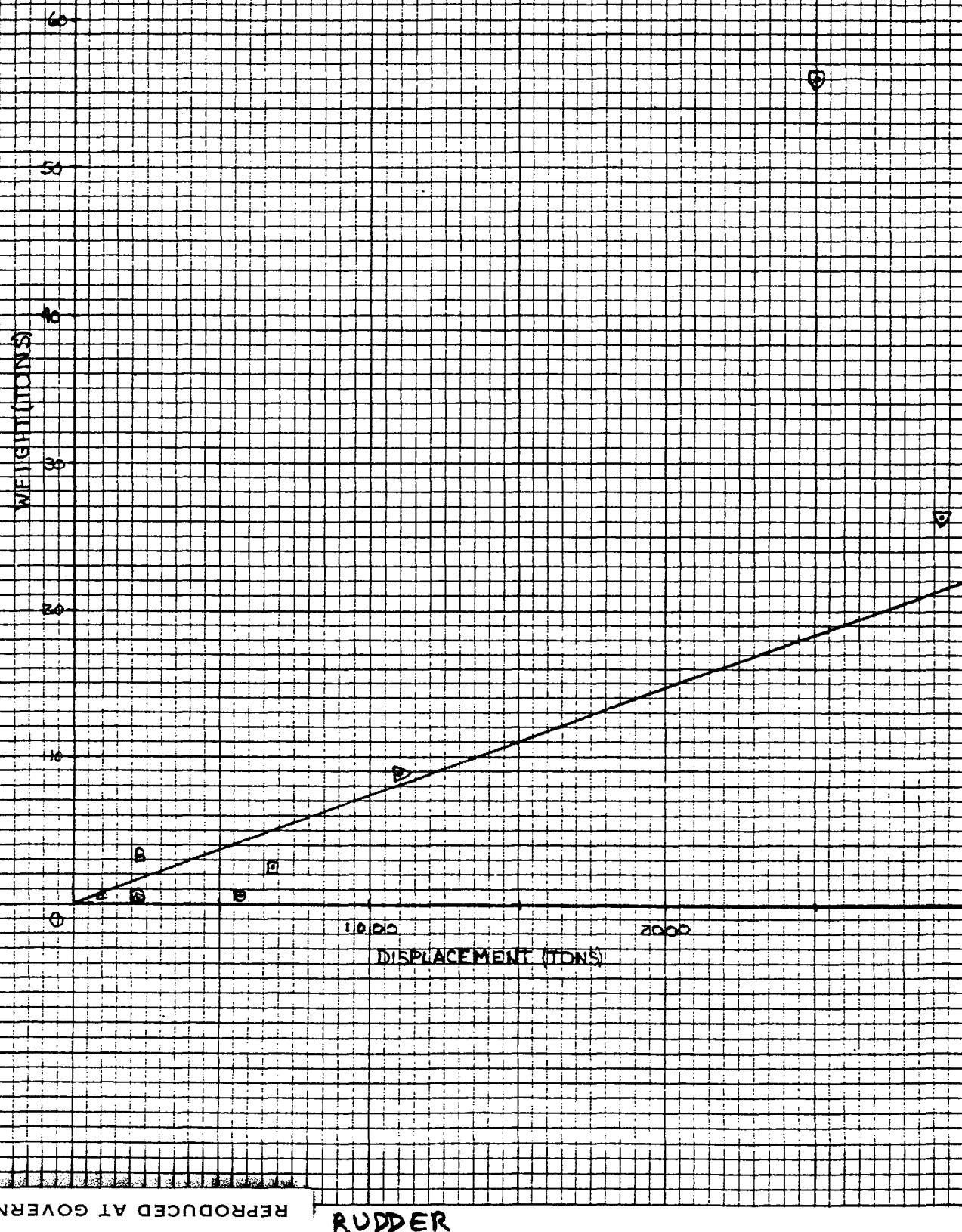
426/28 - STEERING CONTROL RUDDERS  
(LONG TONS)x SES-1001 (HYDRAULIC CONTROL IS IN  
HYDRAULIC SYSTEM)

0 1.0 2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0

x ROHR 3K505  
10/12/76

x ROHR (G/10/75)

SUPER SWELL W562



571 Replenish at Sea ✓

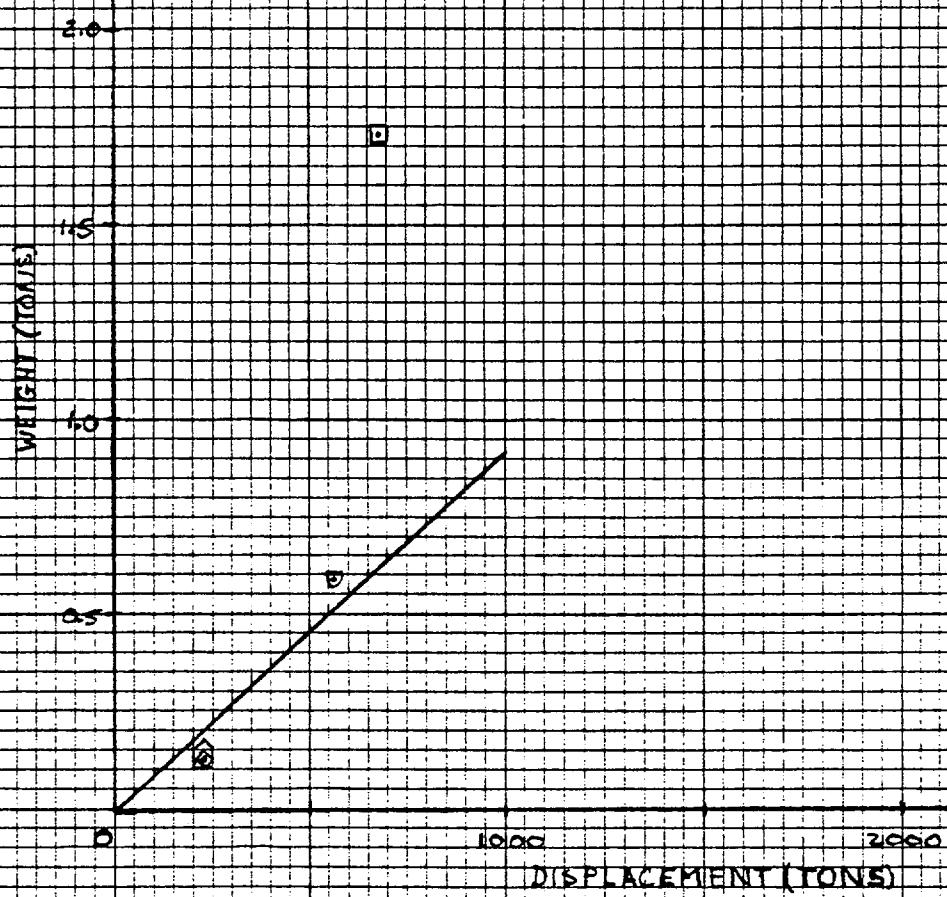
$$WS71 = KS71 * VOLA$$

where  $KS71 = 6.25 \times 10^{-3} \text{ ft/s}^3$

( $KS71$  is based on a constant based on return data of hydrofoils and SASS)

$$VOLA = \text{Total Volume} \approx 10^{-3} \text{ ft}^3$$

The algorithm is the same as ASSAT.



REPLENISHMENT AT SEA

X BELL 5/27/75

W571 - REINFORCEMENT AREA (LONG TONS)

Fig 39

W571 - REINFORCEMENT AREA

RONR 34542  
VL = 1359  
W571 = 2.3  
(10/27/76)

$$f(x) = .00058 \times WFOO$$

X RONR (6/10/75)

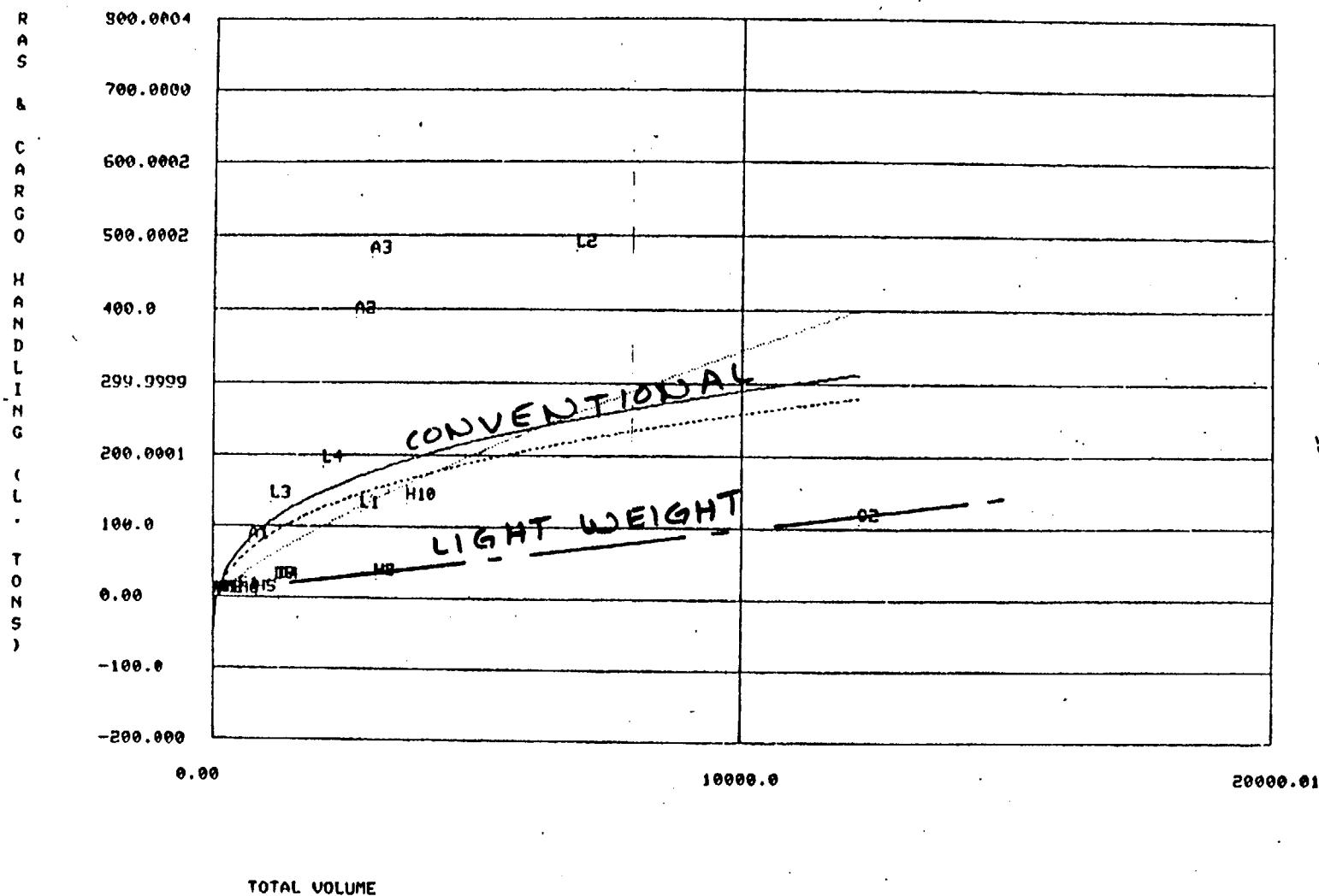
X 1750

VARIABLE LOADS (LONG TONS)

0 100 200 300 400 500 600 700 800 900 1000

## SUBS 571/3/4 RAS &amp; CARGO HANDLING (BSC1 528)

— ALL DATA —— 2 S.ERROR ..... 1 S.ERROR



1572 Ship Stores + Equipment Handling

$$WS72 = KS72 * VOLA$$

$$\text{where } KS72 = \cancel{0.625} \times 10^{-3} \text{ ft/s}^3$$

(KS72 is a constant based on return data from hydrofoils and SESs.)

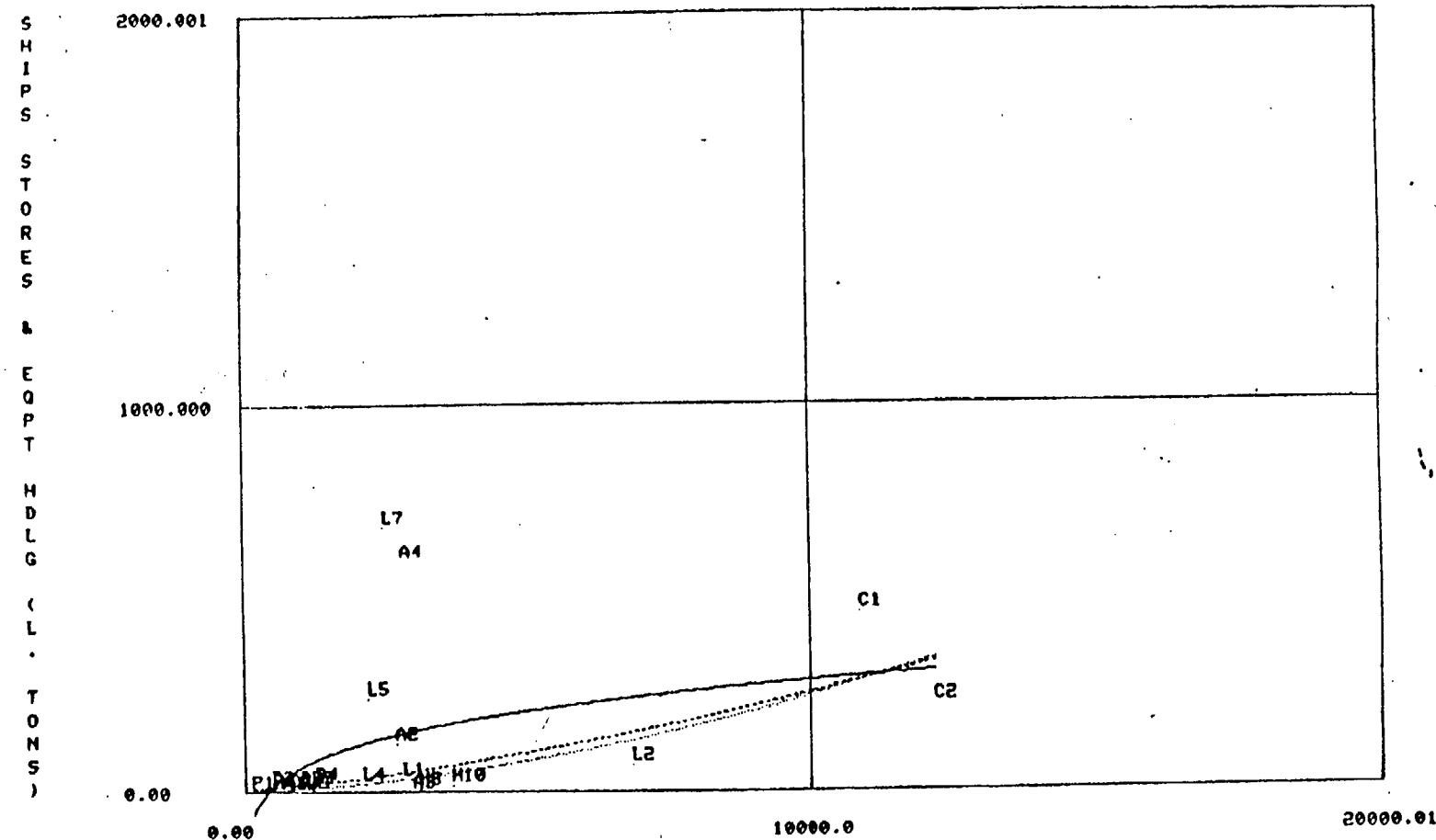
$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

The algorithm is the same as ASSET.

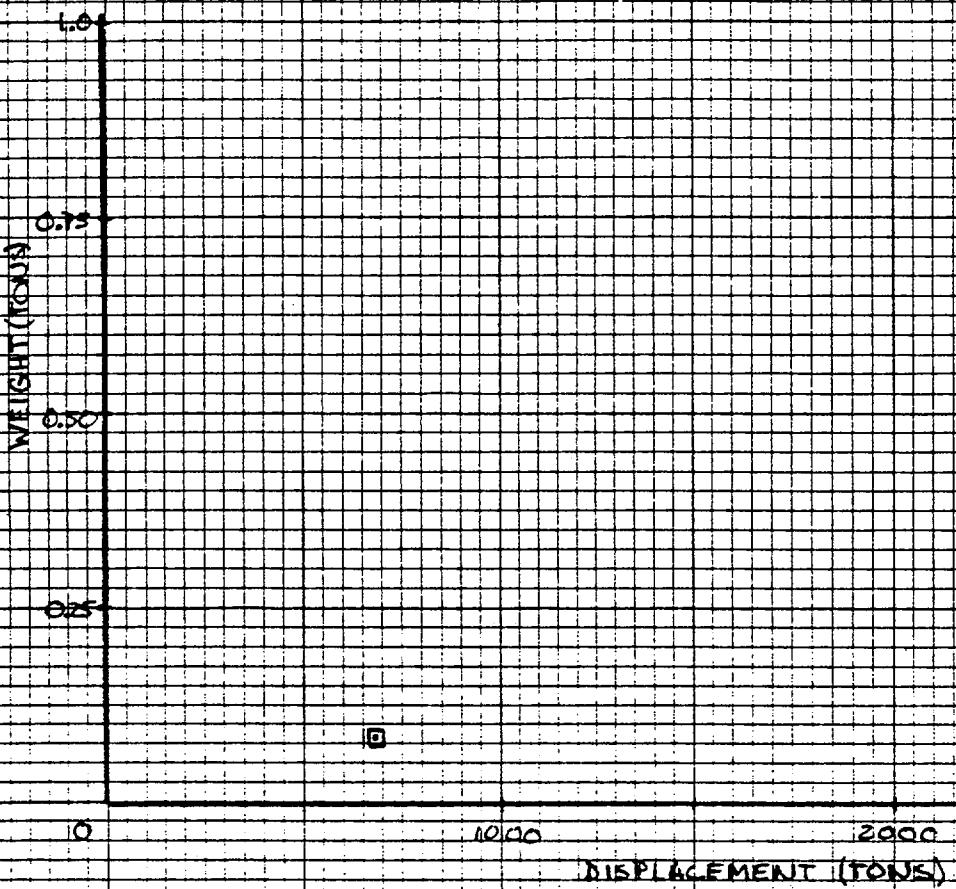
42 381 50 SHEETS 55 SQUARE  
42 382 100 SHEETS 55 SQUARE  
42 383 200 SHEETS 55 SQUARE  
42 384 300 SHEETS 55 SQUARE

## SWBS 572 SHIPS STORES &amp; EOPT HANDLING (BSC1(521))

— ALL DATA — 2 S.ERROR — 1 S.ERROR



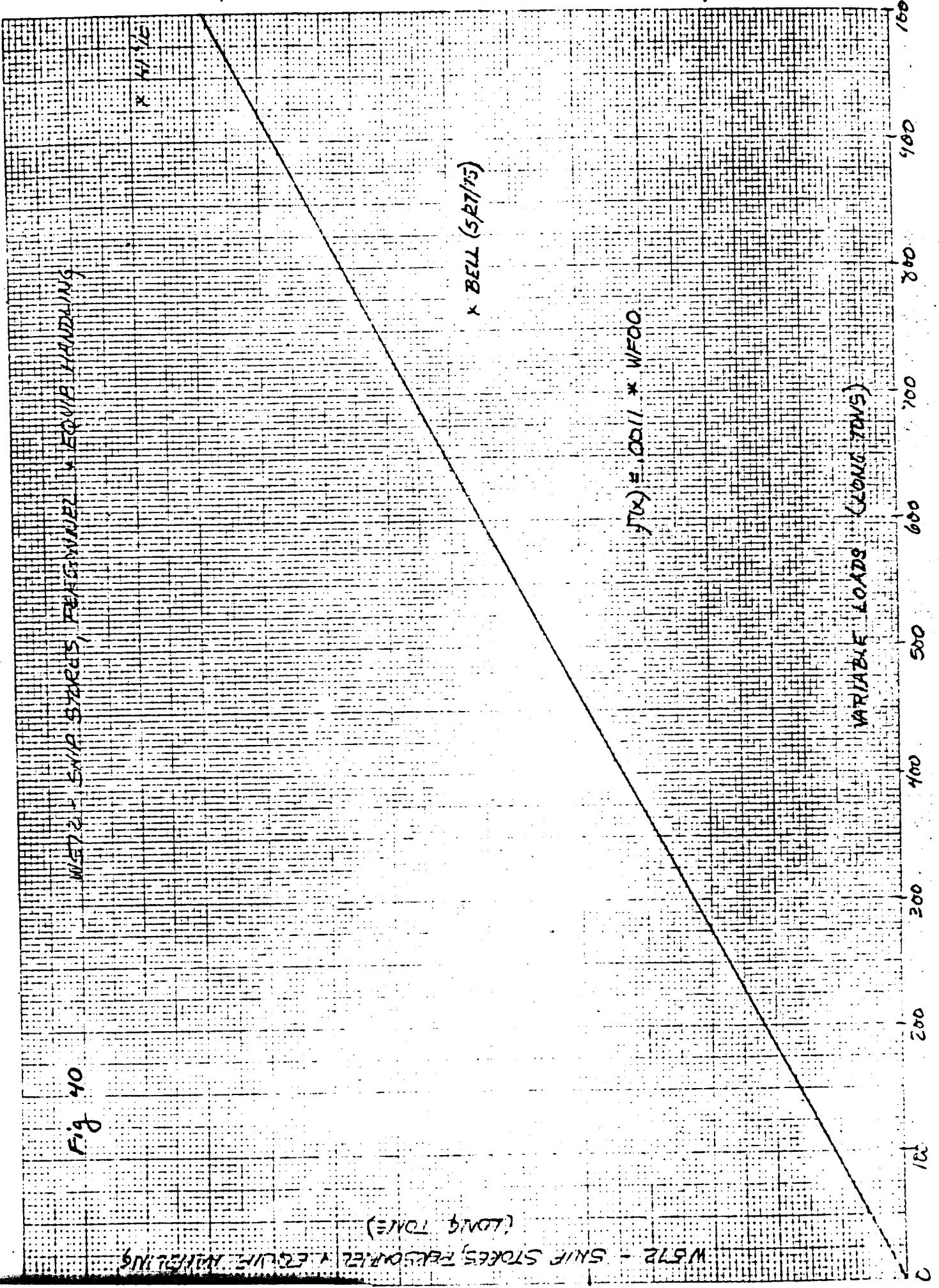
TOTAL VOLUME

10 INCHES = 1 METER  
100 MM X 10 MM = 1 CM<sup>2</sup>

卷之三

CHAMBERSBURG NO. 1827-161  
TRADING POST NO. 1827-161  
CROSS SECTION - ICKTOWA MOUNTAIN

REPRODUCED AT GOVERNMENT EXPENSE



## ✓S81 Anchor Handling + Storage Systems

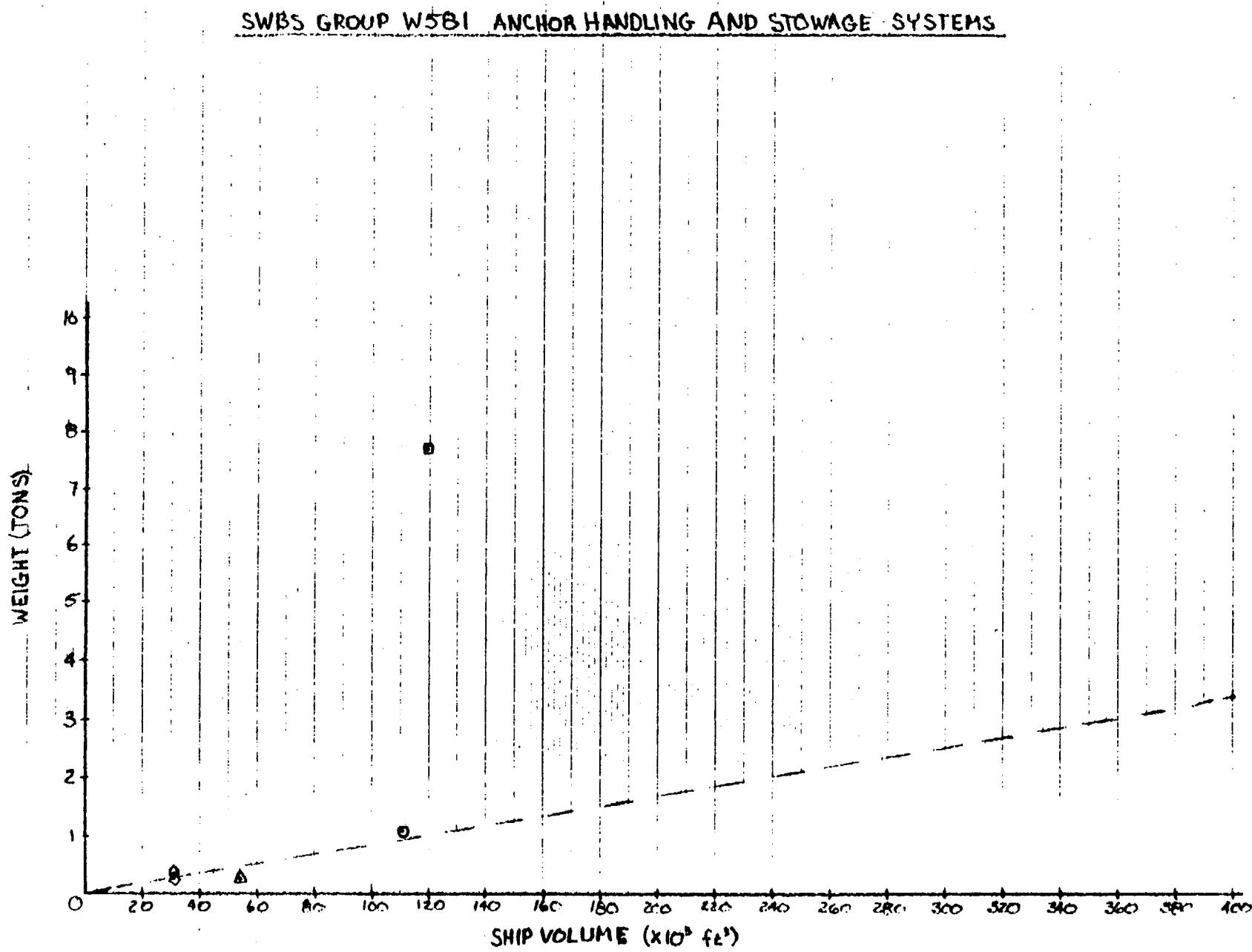
$$WS81 = KS81 \times VOLA$$

$$\text{where } KS81 = .01 \text{ lb/lft}^3$$

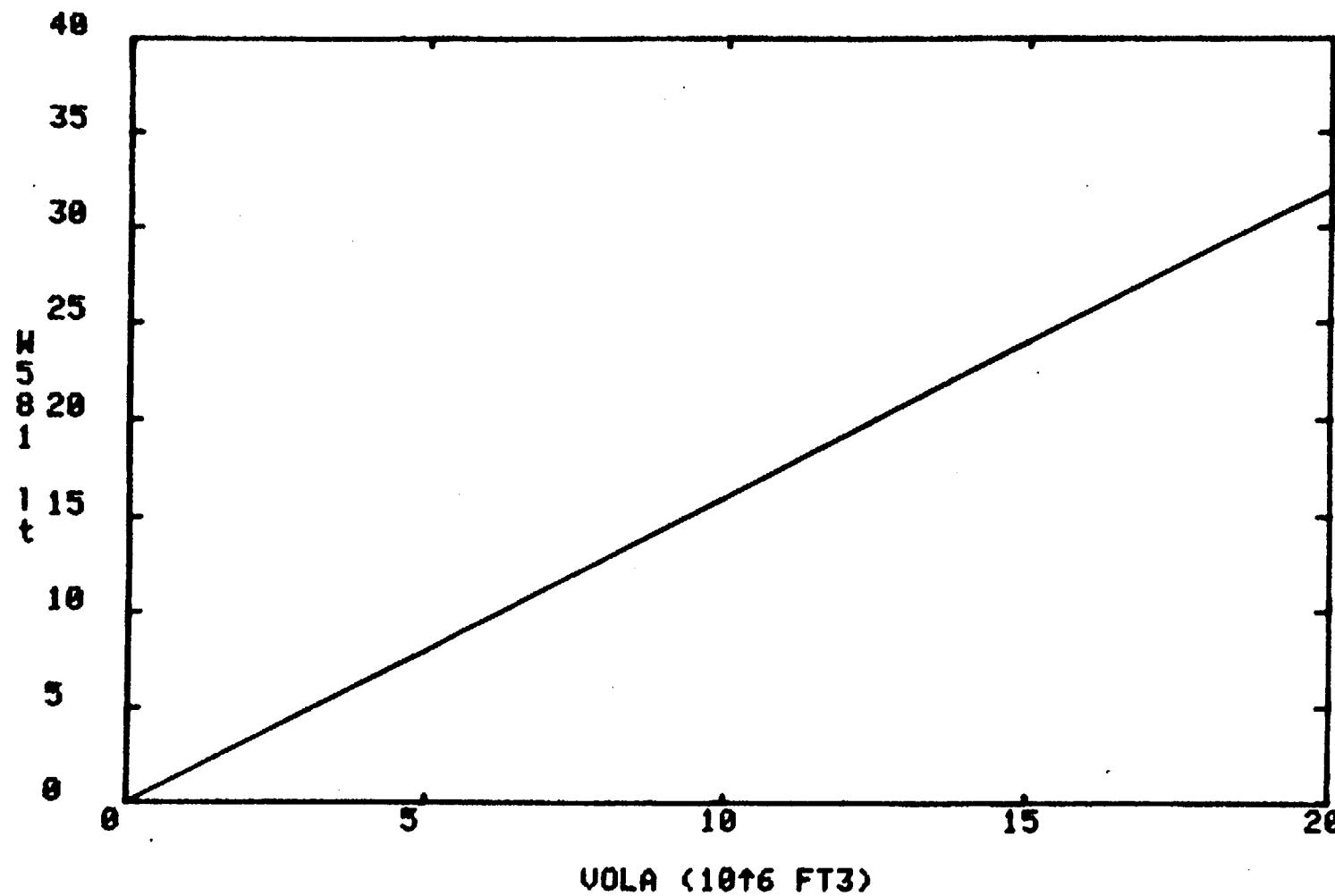
( $KS81$  is a constant based on recommendations from hydrostatic and STSS.)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

The algorithm is the same as ASSET

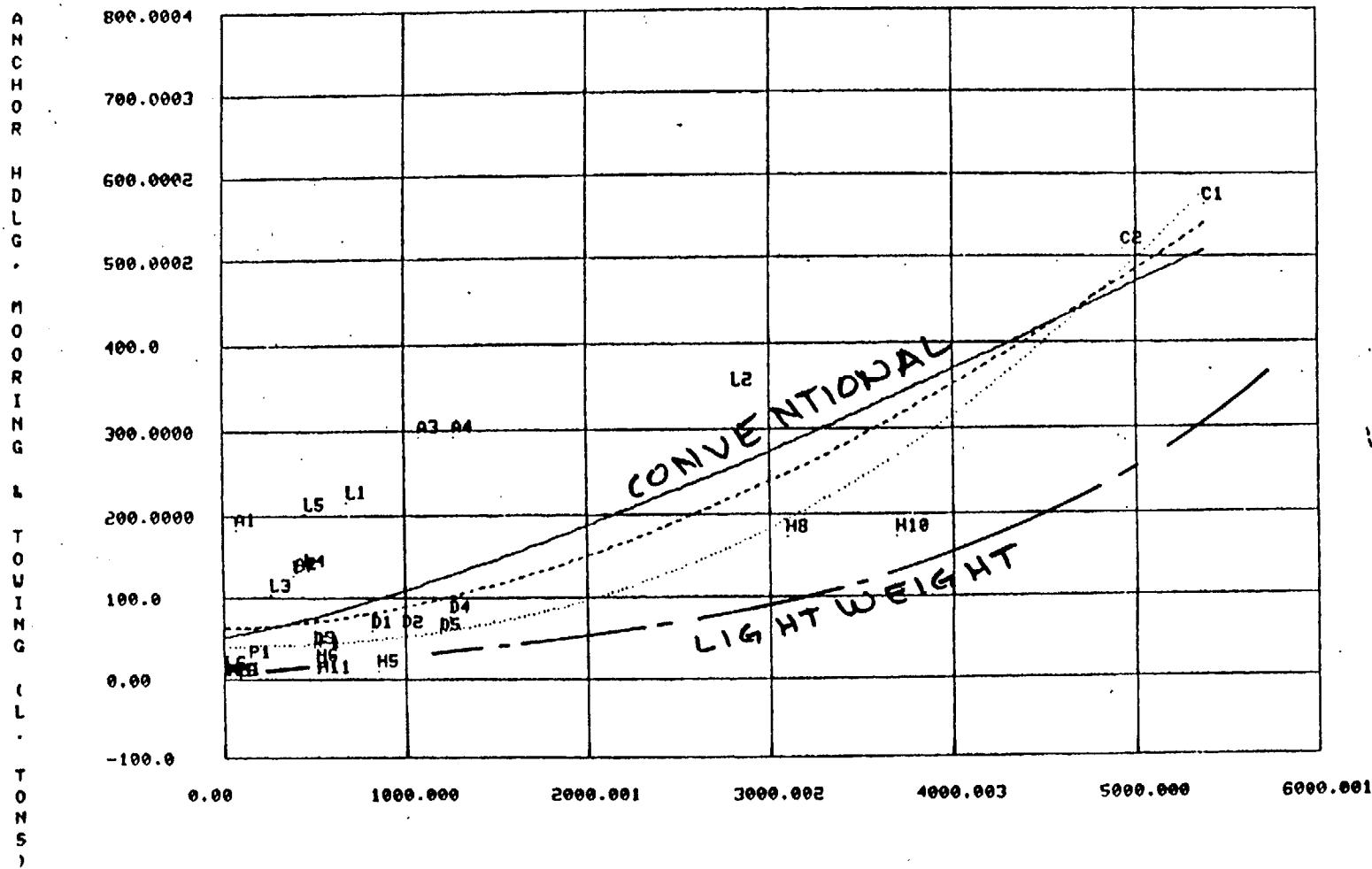


W581 VS VOLA AS OF 10/31/83



## SUBS 581/2 ANCHOR HANDLING, MOORING &amp; TOWING (BSCI 520)

— ALL DATA —— 2 S.ERROR ..... 1 S.ERROR



W587 - ANCHOR HANDLING &amp; STORAGE (Long Tons)

Fig 41

W587 - ANCHOR HANDLING &amp; STORAGE

10.0

14.0

12.0

10.0

8.0

6.0

4.0

2.0

0

VOLA  $\times 10^{-5}$ PHM  
SES-1M-1 1.0

2.0 3.0 4.0 5.0 6.0 7.0 8.0 9.0 10.0

BELL  
(5/27/75)

BELL (3/11/76)

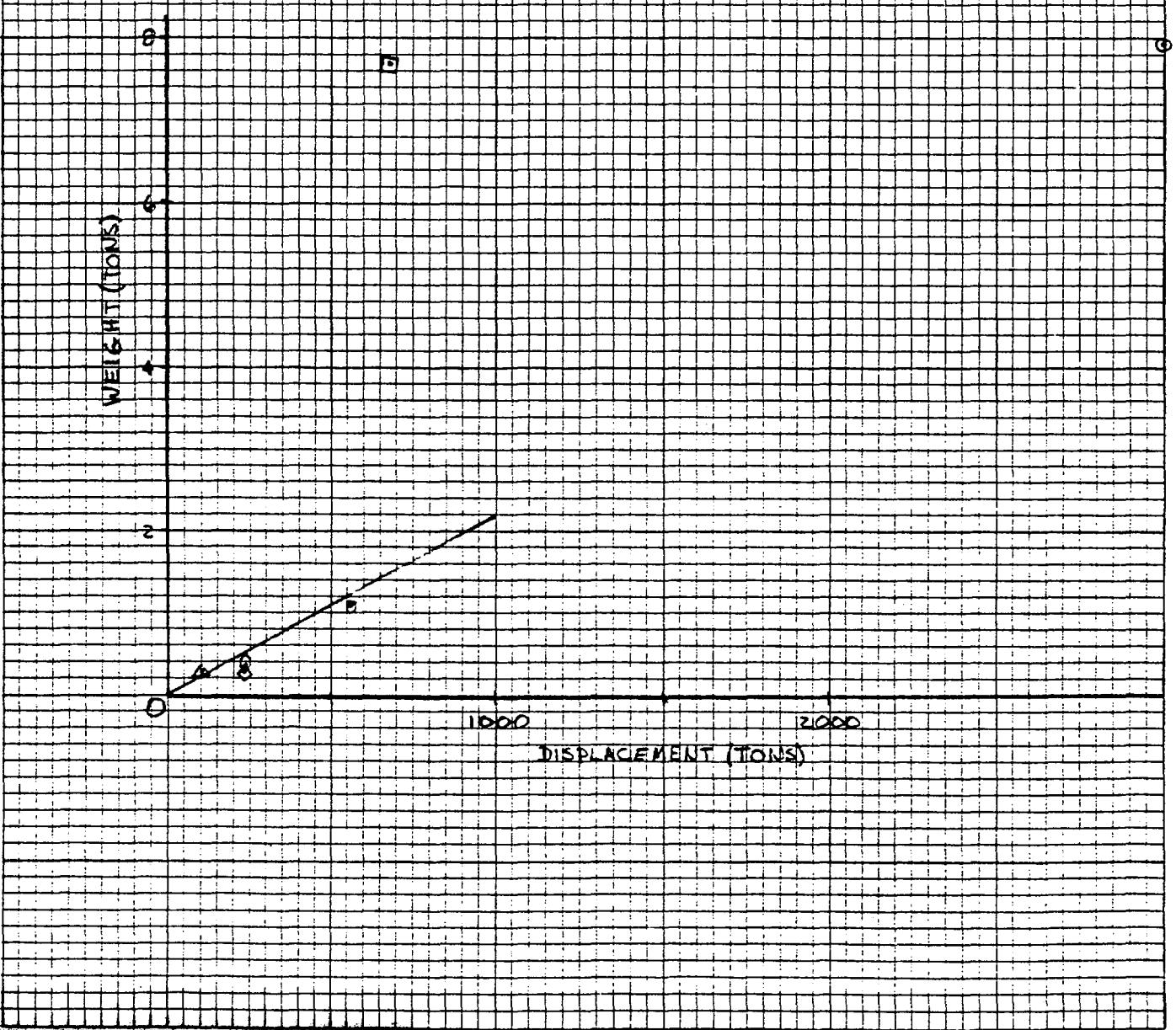
ROHR 16/10/75

X ROHR BASES  
10/12/76

$$F(x) = 1.6 \times VOLA \times 10^{-5}$$

SEE PAGE 520

SWE GRONE SB



## ✓S82 Mooring + Towing System

$$WS82 = KS82 \times VOLA$$

where  $KS82 = .01 \text{ lb/l ft}^3$

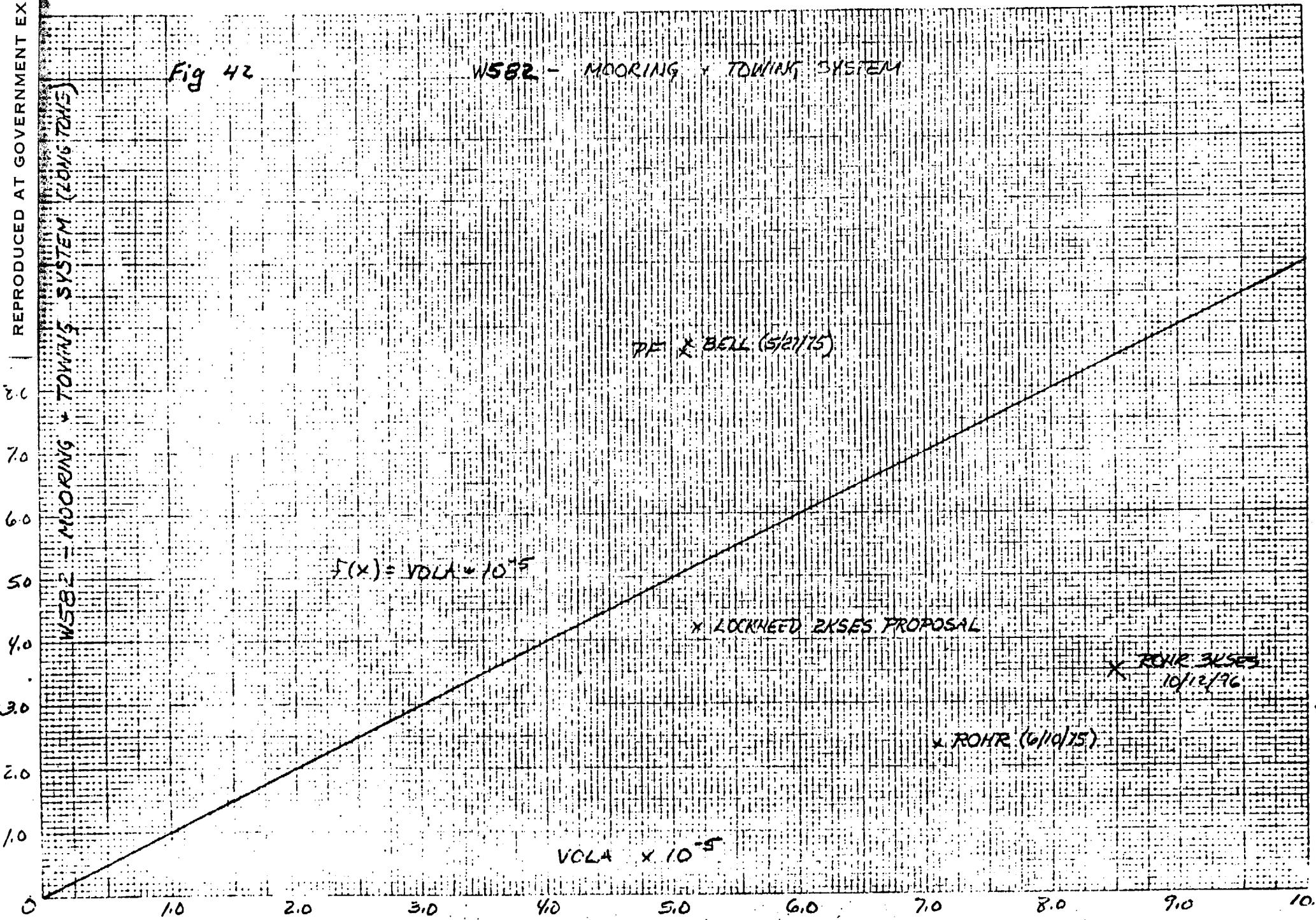
( $KS82$  is a constant based on return weight of hydrofoils and SSS.)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ft}^3$$

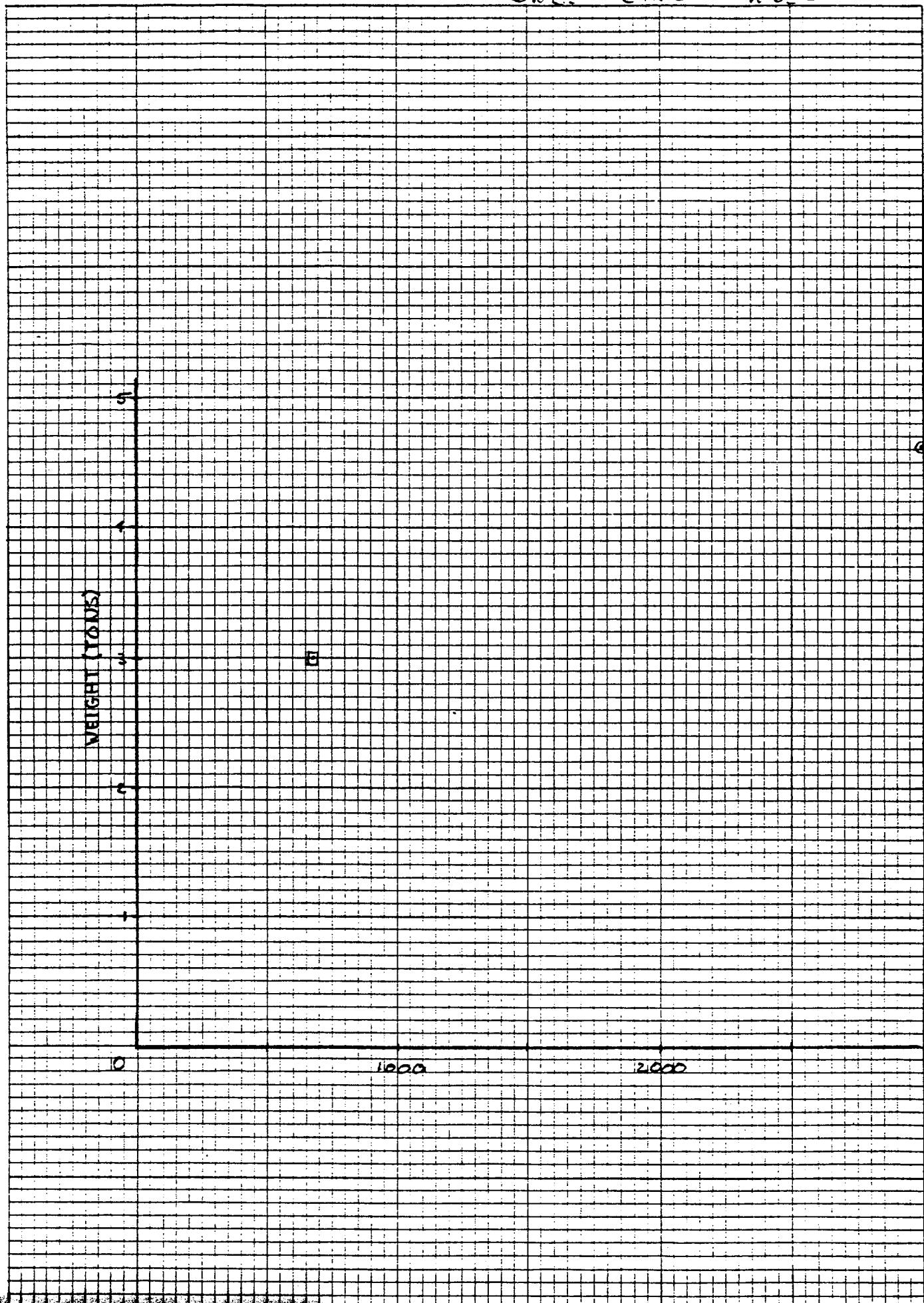
The algorithm is the same as ASSET,

Fig 42

W582 - MOORING + TOWING SYSTEM



SWE: GFOU: W552



## ✓583 Boat Handling & Storage Systems

$$WS83 = KS83 \times ACOM$$

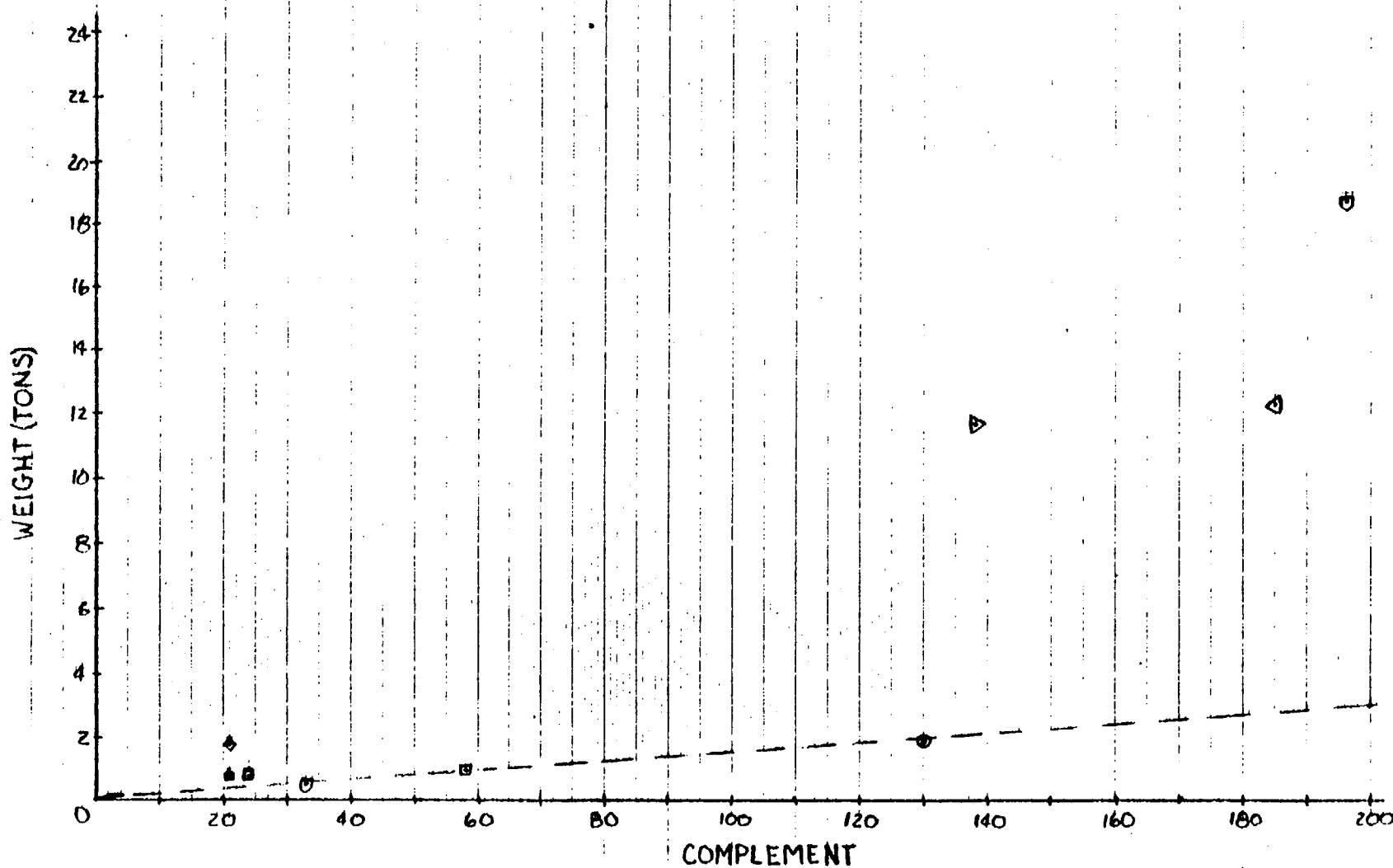
where  $KS83 = .015$  ft

( $KS83$  is a constant based on a combination of hydrofoil and SES.)

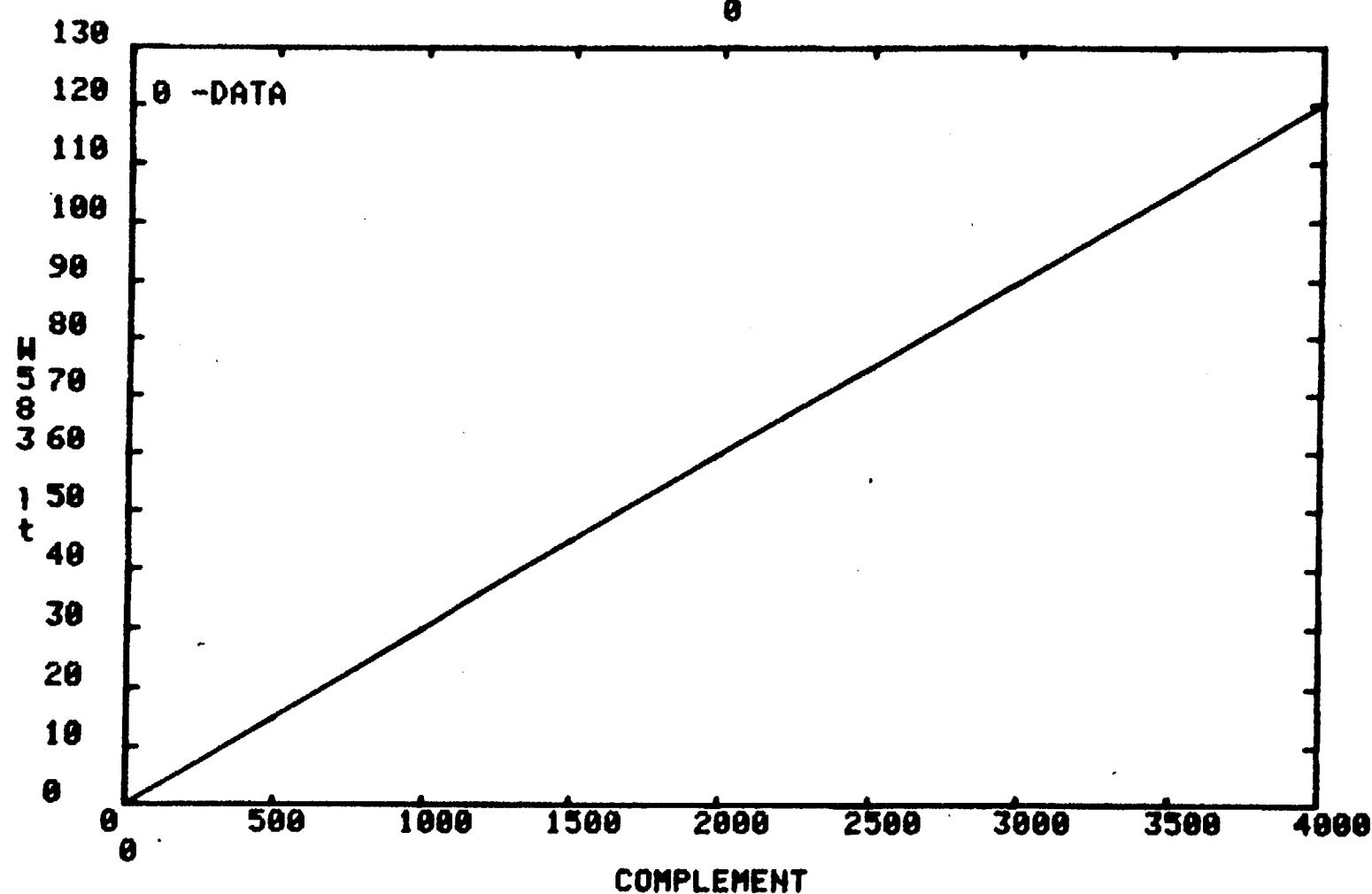
$ACOM$  = Number of Accommodation

The algorithm is <sup>the</sup> same as ASSET.

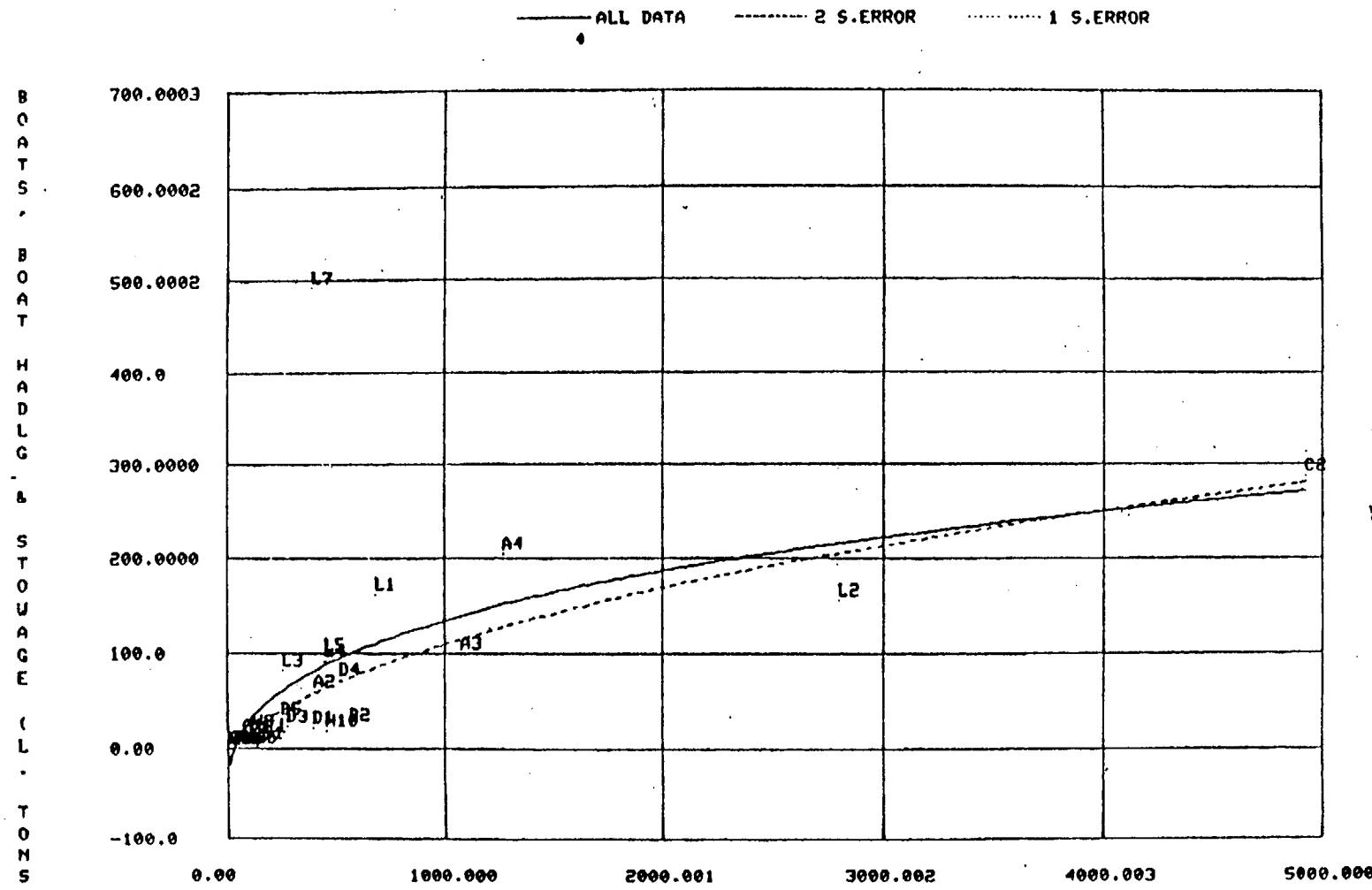
SWBS GROUP W583 BOATS, BOAT HANDLING AND STOWAGE SYSTEMS



W583 VS COMPLEMENT AS OF 10/31/83



PAUSE 'PRESS <RETURN> TO CONTINUE'  
SWBS 583 BOATS, BOAT HANDLING AND STOWAGE (BSCI 601)



TOTAL ACCOMMODATIONS

## ✓593 Environmental Pollution Control System

$$WS93 = KSS3 * ACOM$$

where  $KSS3 = .04 \text{ lt}$

( $KSS3$  is a constant based on return data from hydrofoils and SESS.)

$ACOM = \text{Number of Accommodation}$

The algorithm is the same as ASSET.

SWRS GROUP W 5E3

WEIGHT (TONS)

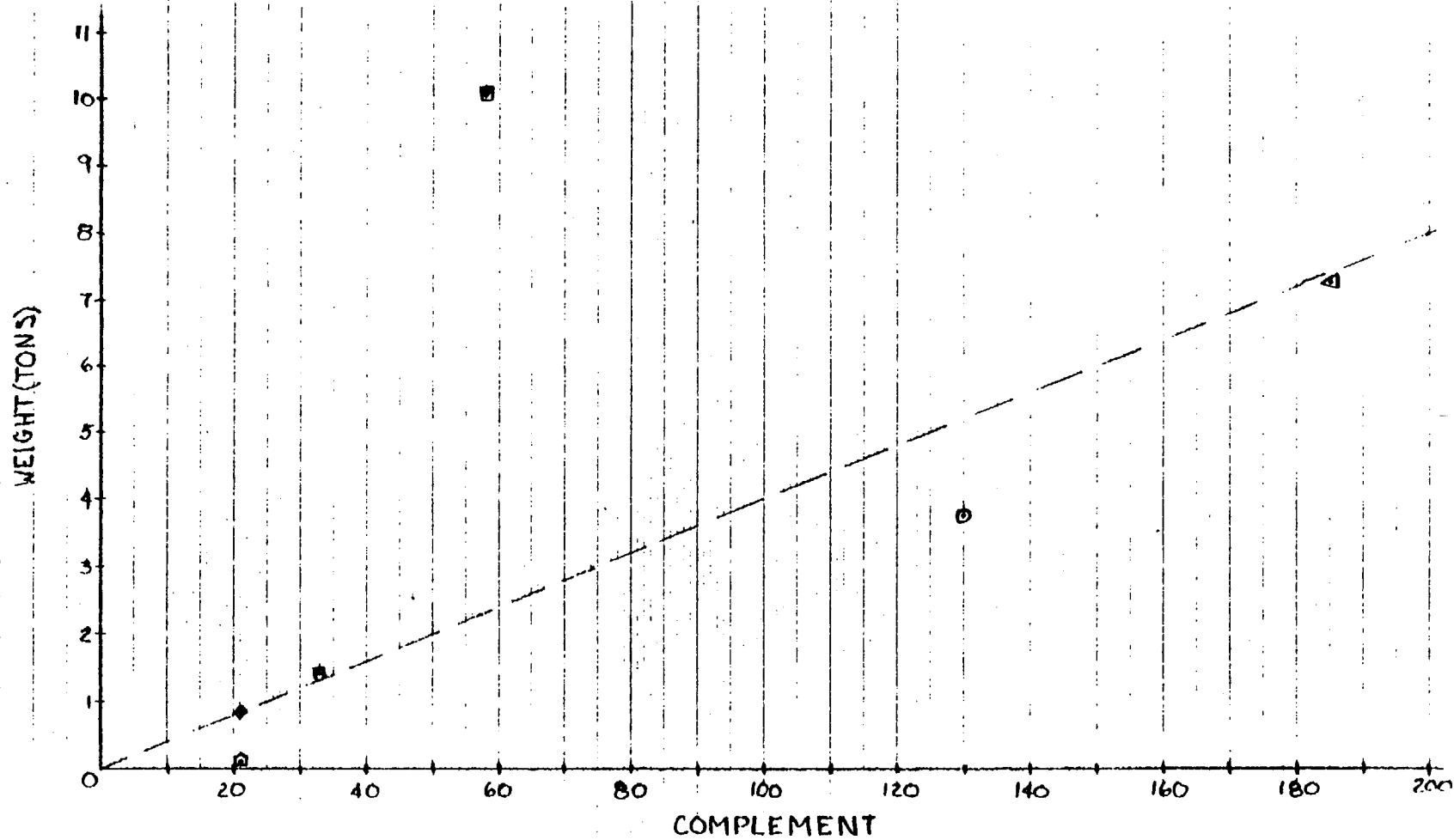
24  
22  
20  
18  
16  
14  
12  
10  
8  
6  
4  
2  
0

DISPLACEMENT (TONS)

1000 2000 3000

FPM-AI-20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCURATED

SWBS GROUP W 593 ENVIRONMENTAL AND POLLUTION CONTROL SYSTEMS



W593 VS COMPLEMENT AS OF 10/31/83

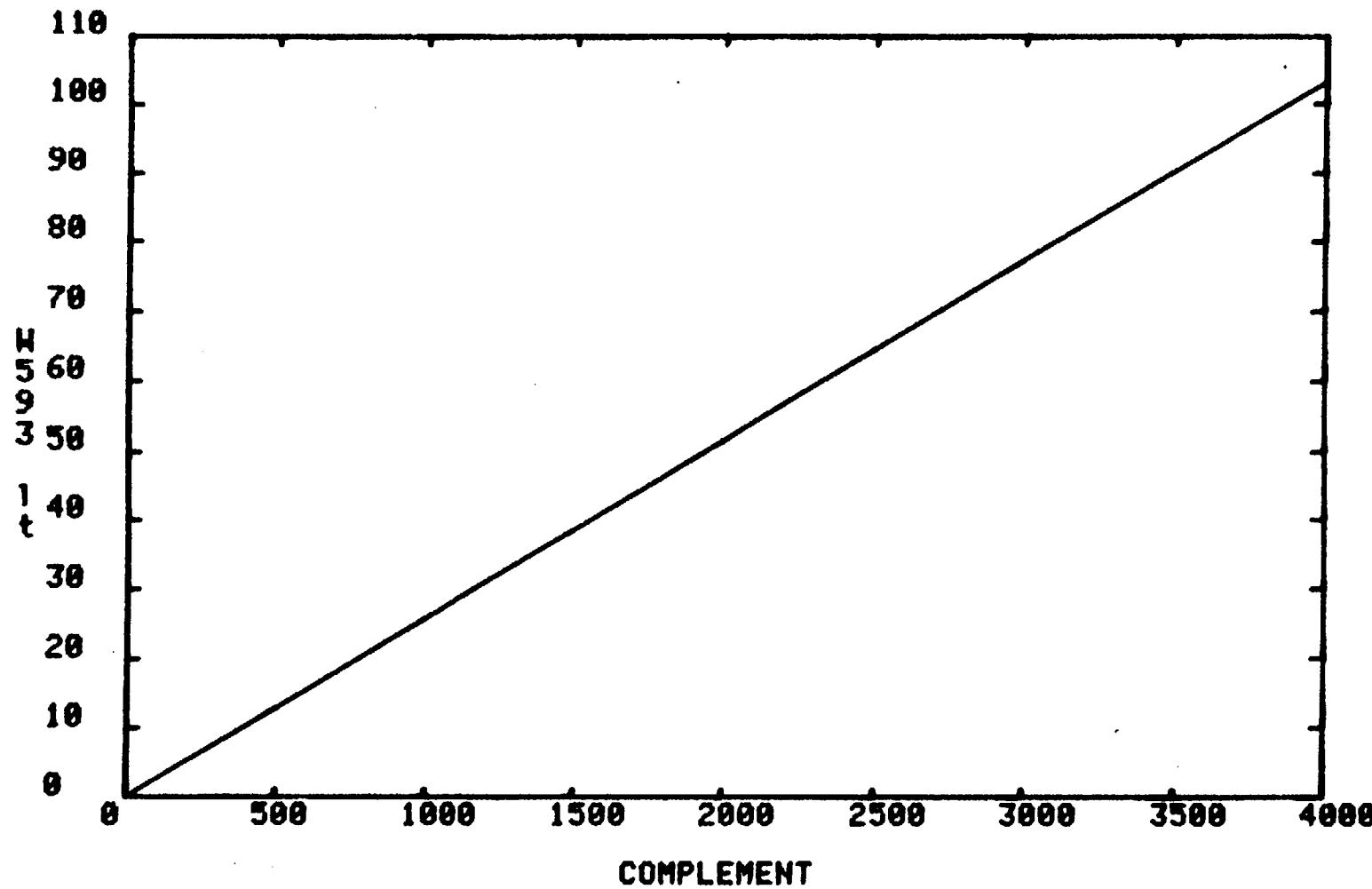


Fig 44

W593 - ALL WIREY CRIMP

PF

W593 - Full stroke cured (long tan)

8.0

7.0

6.0

5.0

4.0

3.0

2.0

1.0

0

50

100

150

TCOMP

$$t(x) = .0258 + TCOMP$$

Pill 1

X ROKR (2/2/74)

X BELL (5/27/75)

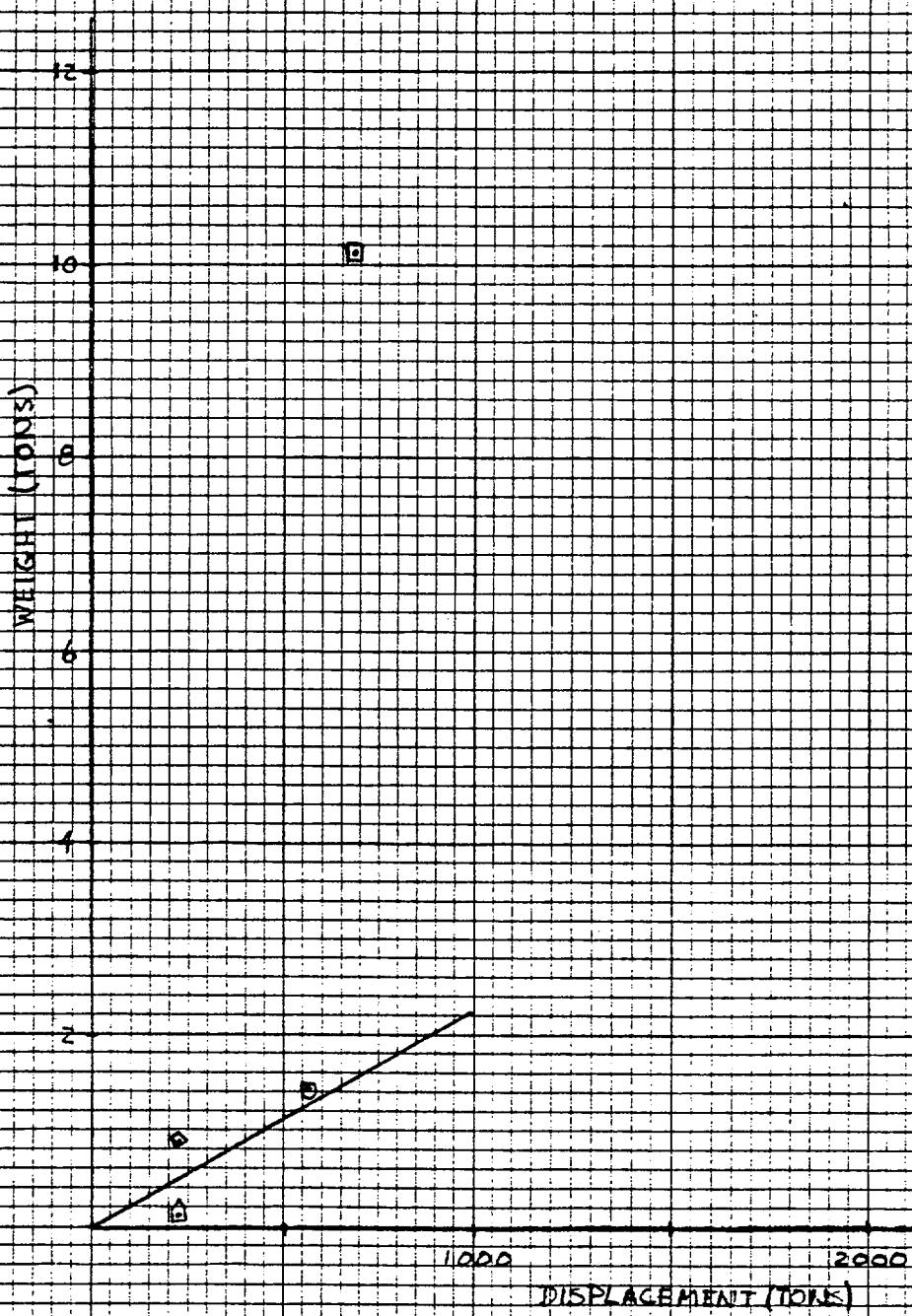
X 1<sup>ST</sup> ITERATION+ 10<sup>-4</sup>/G

X ROKR (6/12/75)

X ROKR 3KSES  
10/12/75

SEE SHEET # 502

SWBS GRADE W50?



FRICTION 10 X 10 TO 1 INCH  
TOTH THIN HEAVY

## 1598 Auxiliary System Operating Fluids

$$WS98 = K598 \cdot (WS00 - WS88 - WS99) + LS98$$

where  $K598 = .0177$  &  $LS98 = 1.23$  (ASSET)

~~WS00~~ • WS00 = Auxiliary System Weight, lt

WS88 = Auxiliary Systems Operating  
Fluid Weight, lt

WS99 = Auxiliary Systems Repair  
Parts & Tools, lt

The algorithm is the same as ASSET

## ✓599 Auxiliary System Repair Parts + Tools

$$WS99 = K599 \times \frac{(WS00 - WS88 - WS55)}{(WS00 - WS88 - WS55)}$$

where  $K599 = 5.8 \times 10^{-3}$ . (ASSET)

$WS00$  = Auxiliary System Weight, lt

$WS88$  = Auxiliary System Operating Fluid Weight, lt

$WS55$  = Auxiliary System Repair Parts + Tools Weight, lt

The algorithm is the same as ASSET.

FPI M.F. 20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED

WEIGHT (TONS)

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

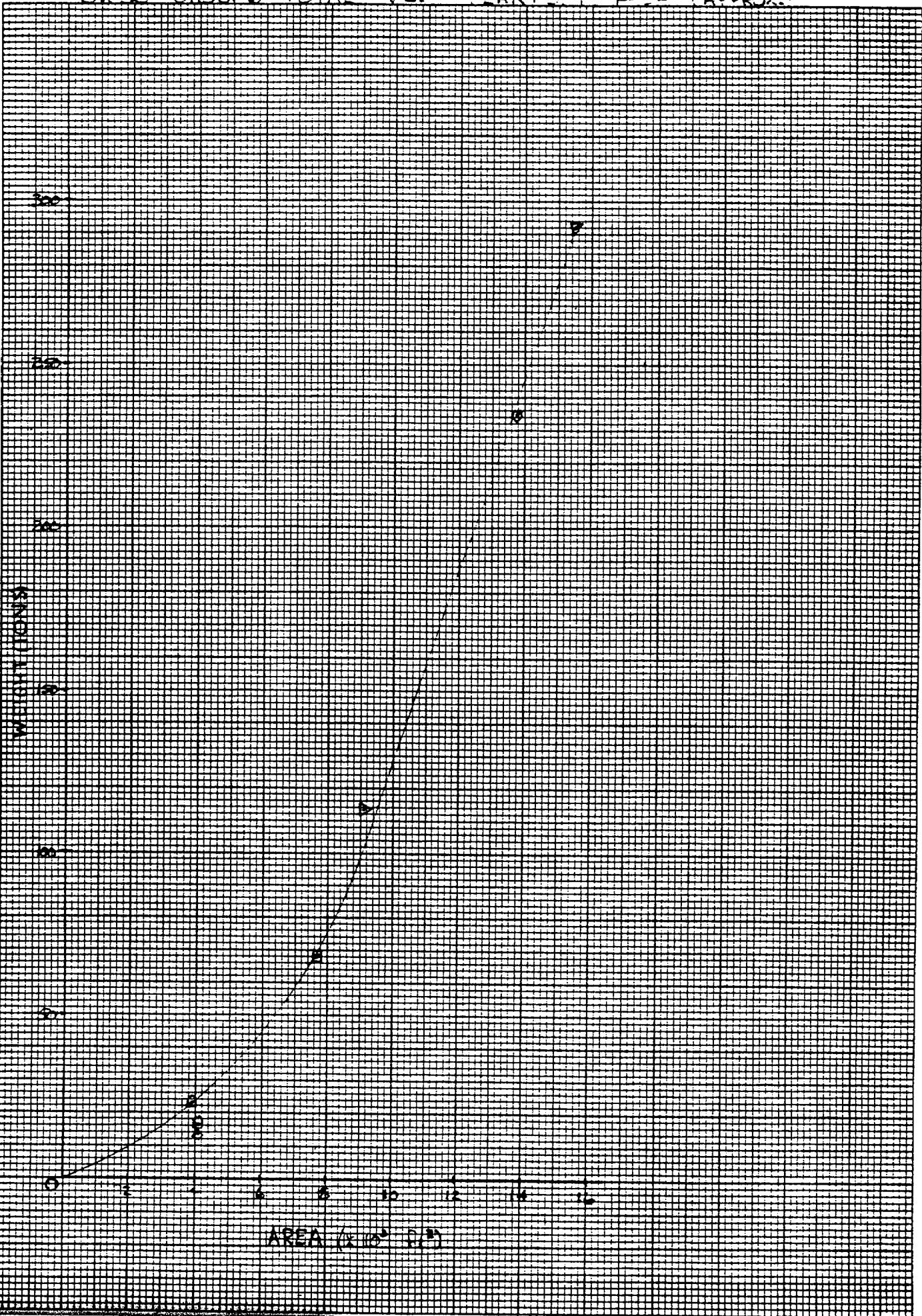
1000 1000 1000 1000

1000 1000 1000 1000

1000 1000 1000 1000

INDIA THIS IS A TEST SHEET

SWPS GROUP 6 TOTAL VS. D-LANFORN FILE (APPROX.)



EN MI 20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED

SWES GROUP 6 TOTAL VS. SUPERSTRUCTURE VOLUME

PRINT: 20 X 20 TO 1 INCH  
5TH, 10TH AND 20TH LINE PROGRESSIVELY ACCENTED

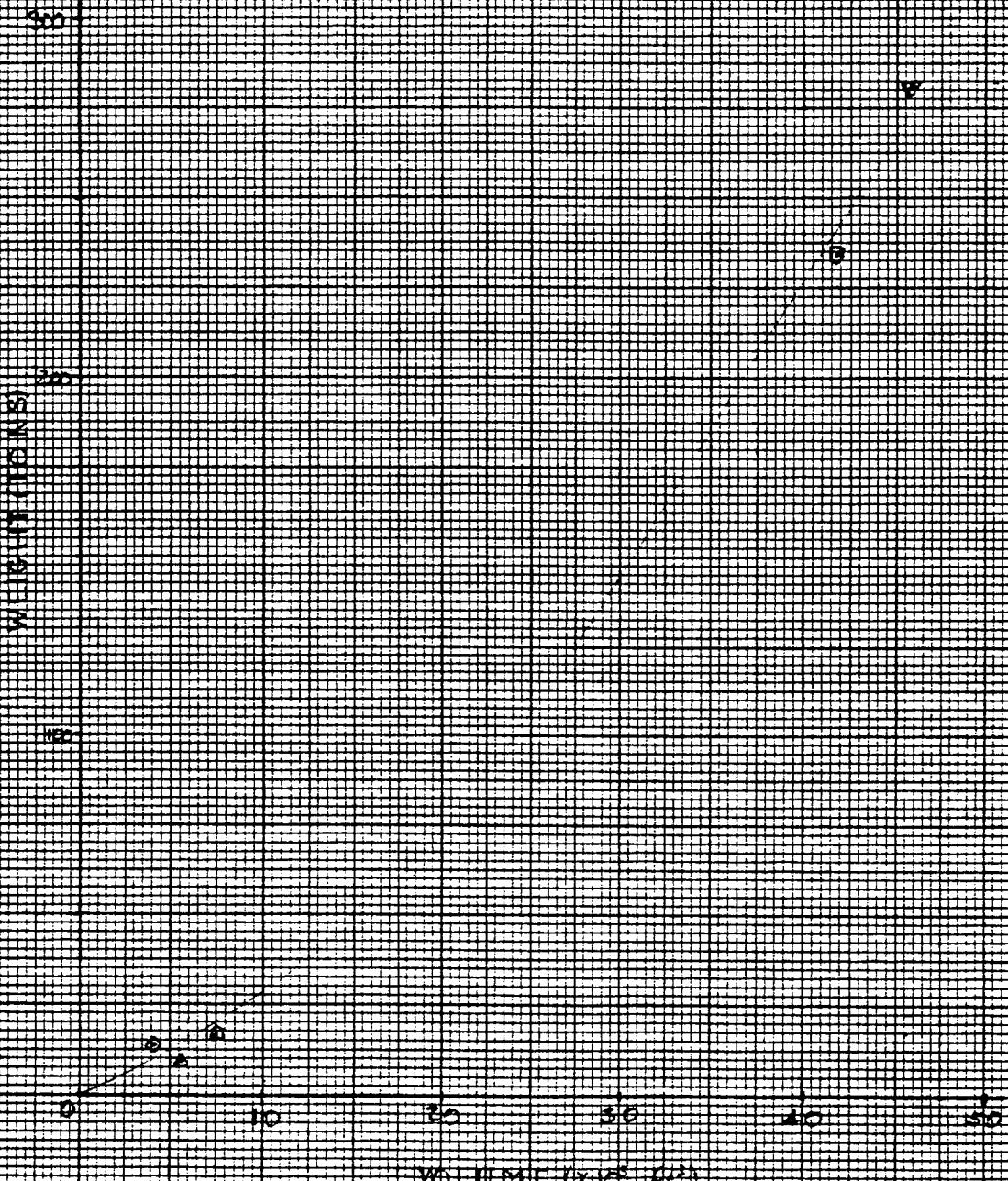


Fig 45.

WEI = NULL FITTINGS

$$W611 = 11 \times LICE * BOA$$

$$K611 = 3.442 \times 10^{-5}$$

W611

WEI - NULL FITTINGS (L<sub>1</sub> T)  
(LONG TURNS)

SES-100A

AGEH-1

PNM

TOMR 2KSES  
(6/10/75)TOMR 2KSES  
10/13/76  
BELL 2KSES  
(5/27/75)

$$XLICE * B1T * 10^{-3}$$

$$W611 = 492 * XLICE * B1T * 10^{-4}$$

4.0

3.0

2.0

1.0

0

10

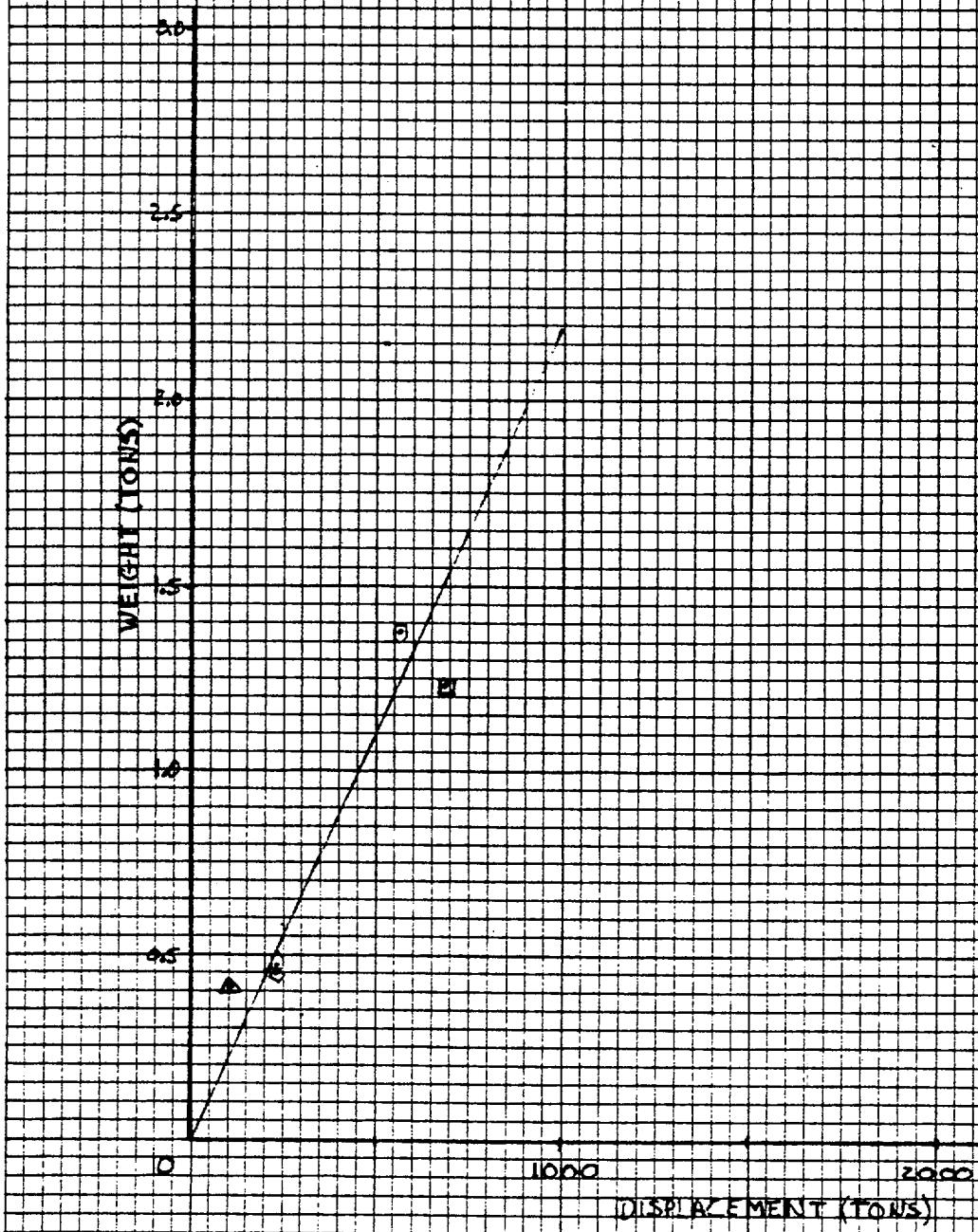
20

30

40

SEE PAGE 602

SWEET GENEVA 1612



100 FEET TO 1 INCH  
100 TONS TO 1 TON

## 6.11 Hull Fitting

$$W_{H11} = K_{H11} \times LCUE \times BOA$$

where  $K_{H11} = 4.42 \times 10^{-5}$  ft / ft<sup>2</sup>

( $K_{H11}$  is a constant based on return data from hydrofoils and SESs)

$LCUE$  = cushion length, ft

$BOA$  = beam overall, ft

Algorithm is same as ASSET and SES Design Manual.

Fig 45

W611 = ROLL FITTINGS

$$W611 = K611 * XLICE * BOA$$

$$K611 = 1.42 \times 10^{-5}$$

N18\*

WEIGHT ROLL FITTINGS (LBS)

SES-100A

AGEH-1

PHM

ROHR 2KSES  
(6/10/75)ROHR 2KSES  
(7/10/76)  
BELL 2KSES  
(5/27/75)XLICE \* BIT \* 10<sup>-3</sup>

$$W611 = 492 * XLICE * BIT * 10^{-4}$$

0

10

20

30

40

## G12 Rails, Stanchions + Lifelines

$$W_{G12} = K_{G12} \times LCUE \times BOA$$

where  $K_{G12} = 1.2 \times 10^{-4}$  ft/ft<sup>2</sup>

( $K_{G12}$  is a constant based on return data from hydrofoils and SESs.)

LCUE = cushion length, ft

BOA = Beam overall, ft

Algorithm is same as ASSET and SES Design Manual.

Fig. 46

WG12 - RAILS, STANCHIONS, LIFELINES

$$W_{G12} = K_{G12} \times C_D \times B_D A$$

$$K_{G12} = 1.2 \times 10^{-4}$$

x pp

$$K_{G12} = 1.2 \times 10^{-4}$$

x 5/10/15/79  
x ROHR 2KSES  
10/12/76

x 5/22/15  
- ROHR 2KSES (5/22/15)

$$W_{G12} = 75 \times C_D \times B_D A \times 10^{-4}$$

$$x 1.25 \times 10^{-3}$$

KSES - 100A

x AGEM-1

WG12 - RAILS, STANCHIONS, LIFELINES  
(LONG TOPS)

0

10

20

30

40

## 613 Rigging and Canvas

$$W_{613} = K_{613} \times LCUE \times BOA$$

$$\text{where } K_{613} = 1.15 \times 10^{-5} \text{ lb/ft}^2$$

( $K_{613}$  is a constant based on return data from hydrofoils and SESs)

$LCUE$  = cushion length, ft

$BOA$  = Beam Overall, ft

Algorithm is the same as ~~SES~~ of the  
SES Design Manual.

DRAWING PAPER NO. 1229-101  
TRACING PAPER NO. 1227-101  
CROSS SECTION - 10x10 TO 1 INCH

SQUARES  
MADE IN U.S.A.

NETS - TRIGGERS - CANVAS (LONG TONS)

Fig. 47

WORK - RIGGING IN CANVAS

$$W_{613} = 1.5 \times 10^3 + L_{CCE} \times B_{OA}$$

\* RONR 2K-525  
X RONR EX-525  
10/12/46

RMI 3X 1085/9

$$F(x) = 0.15 \times X^{4.2} C + B_{IT} \times 10^{-3}$$

\* R146

N PF

X AGEA-1

X 4.2 C + B\_{IT} \times 10^{-3}

0

10

.20

30

40

621 Non Structural Bulkheads

$$W_{621} = K_{621} \times VOL_A$$

$$K_{621} = .175 \times 10^{-1}$$

$$VOL_A = \text{TOTAL VOL} \times 10^{-3}$$

BASED ON ASSET FORMULA

COEFFICIENT BASED ON SMALLER  
SHIPS & USE OF NOHEX

W.G.21 - NON-STRUCTURAL BULKHEADS (4)

Fig 4.P

W.G.21 - NON-STRUCTURAL BULKHEADS

W.G.21 = K.62 \* VOLA

K.62 = 1.73

VOLA = Volume x 10

X BELL (INCLUDES SLEEVING)

X BELL (5/27/75)

\* RMI 3X  
10115779X ROHR 2SESSES 1411746  
6/10/75

$$f(x) = 1.73 * VOLA * 10^5$$

SES-1001  
X PHM

1

2

3

4

5

6

7

8

9

10

AVAILABLE VOLUME \* 10<sup>-5</sup> (FT<sup>3</sup>)

## 622 FLOOR PLATES + GRATINGS

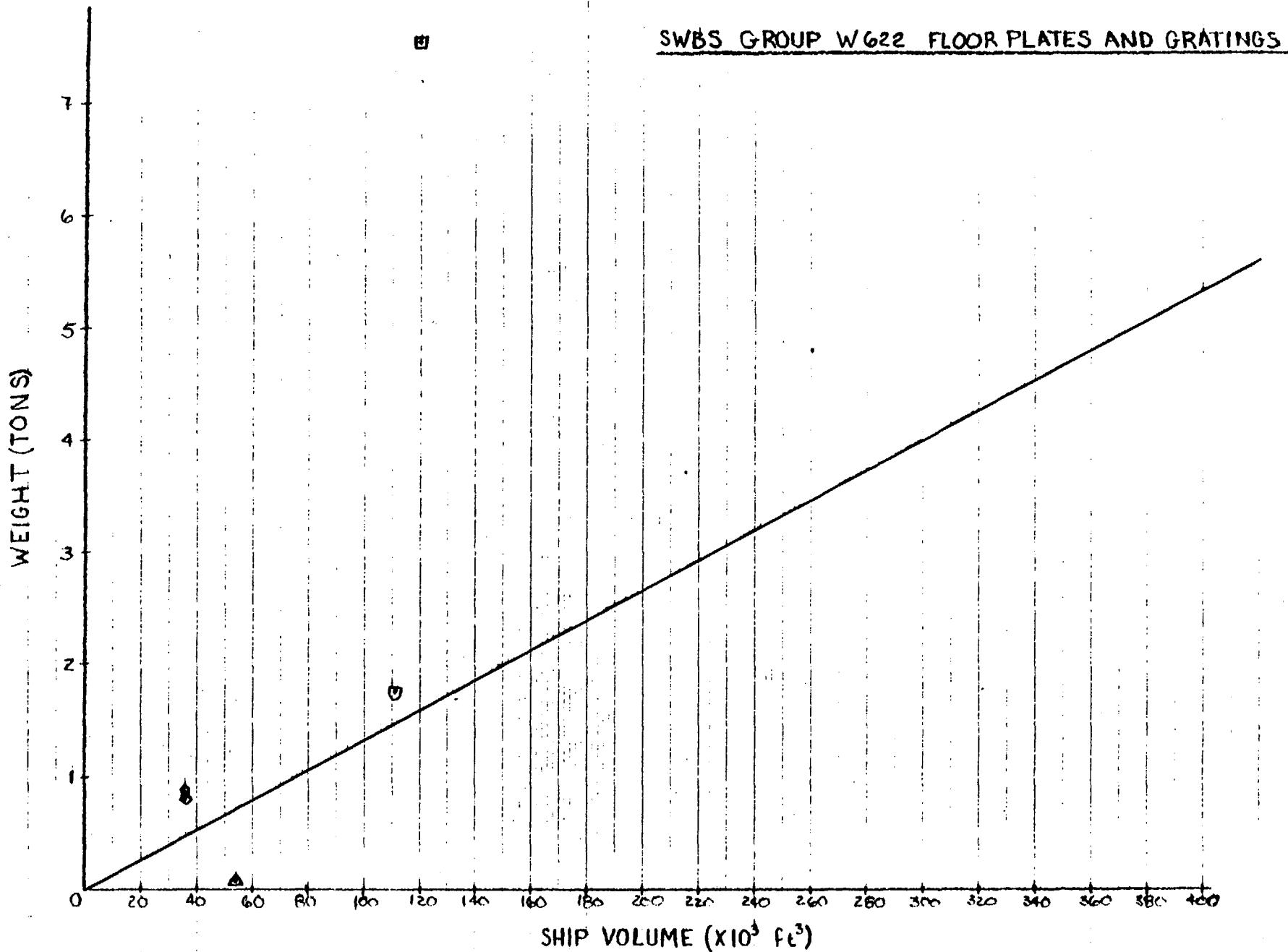
$$W_{622} = K_{622} * VOLA$$

$$K_{622} = .134 \times 10^{-1}$$

VOLA = TOTAL VOLUME / 1000

SAME FORMULA AS ASSET.

COEFFICIENT IS FIT OF SMALLER  
SHIP DATA.



## 623 Ladders

$$WG23 = \frac{K623 + L623}{\text{Total Volume}} \times VOLA$$

$$\text{where } K623 = .3 \text{ ft} + L623 = .0033 \text{ ft}/\text{ft}^3$$

(These constants were obtained from return  
data for hydrofoils and SESs.)

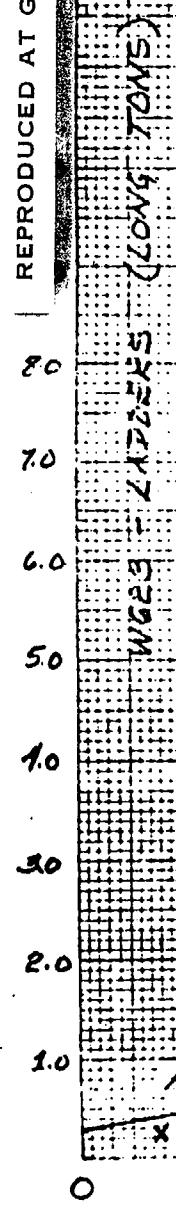
$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ft}^3$$

This algorithm is based on SES Design  
Manual.

Fig 50

W6Z3 - LADDER

$$\begin{aligned} W6Z3 &= H \times Z3 + L6Z3 * VOLA \\ K6Z3 &= .3 \\ L6Z3 &= .0033 \end{aligned}$$



PF

$$f(x) = .3 + .3x + VOLA \times 10^{-5}$$

xH17

X RORR (6/10/75) RORR 300-523  
KEY 1/10

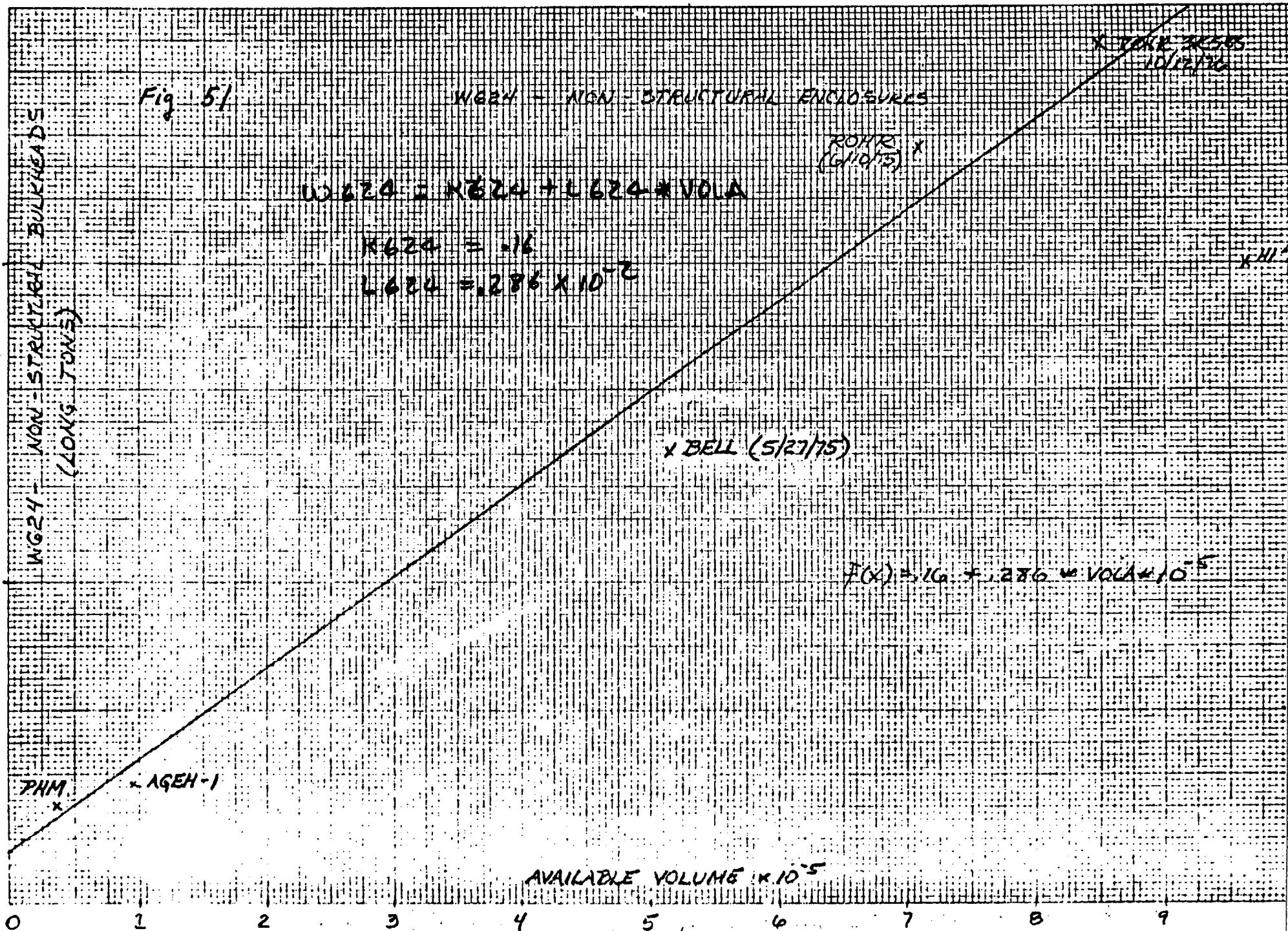
## 624 Non-Structural Closures

$$W_{624} = K_{624} + L_{624} \times VOLA$$

where  $K_{624} = .16$  & and  $L_{624} = \frac{2.86 \times 10^{-3}}{St^3}$

(These constants are based on return data  
for hydrofoils & SLESS.)

$$VOLA = \text{Total Volume } \times 10^{-3}, \text{ ft}^3$$



625 Airports, Fixed Portlights + Windows

$$W_{625} = K_{625} * VLSS$$

where  $K_{625} = .048 \text{ ft/s}^3$

( $K_{625}$  is a constant based on return data  
for hydrofoils and SESs.)

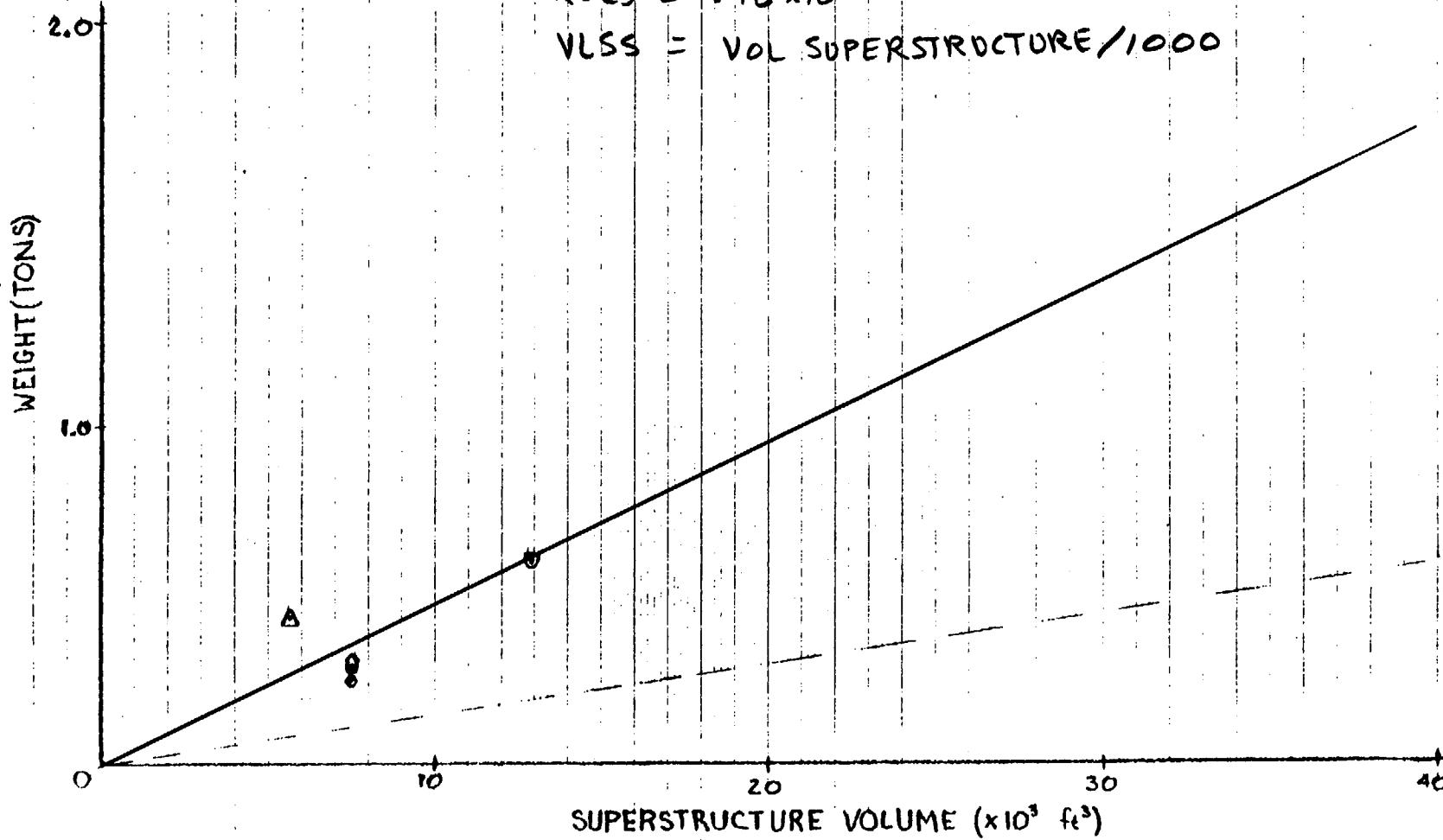
$$VLSS = \text{Superstructure Volume} * 10^{-3}, \text{ft}^3$$

SWBS GROUP W625 AIRPORTS, FIXED PORTLIGHTS, AND WINDOWS

$$W_{625} = K_{625} * VLSS$$

$$K_{625} = .48 \times 10^{-1}$$

VLSS = VOL SUPERSTRUCTURE / 1000



## 631 Painting

$$W_{631} = K_{631} * VOL_A$$

where  $K_{631} = .0185 \text{ lb/ft}^3$

( $K_{631}$  is a constant based on return weights from hydrofoils and SESs.)

$$VOL_A = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

Fig 53

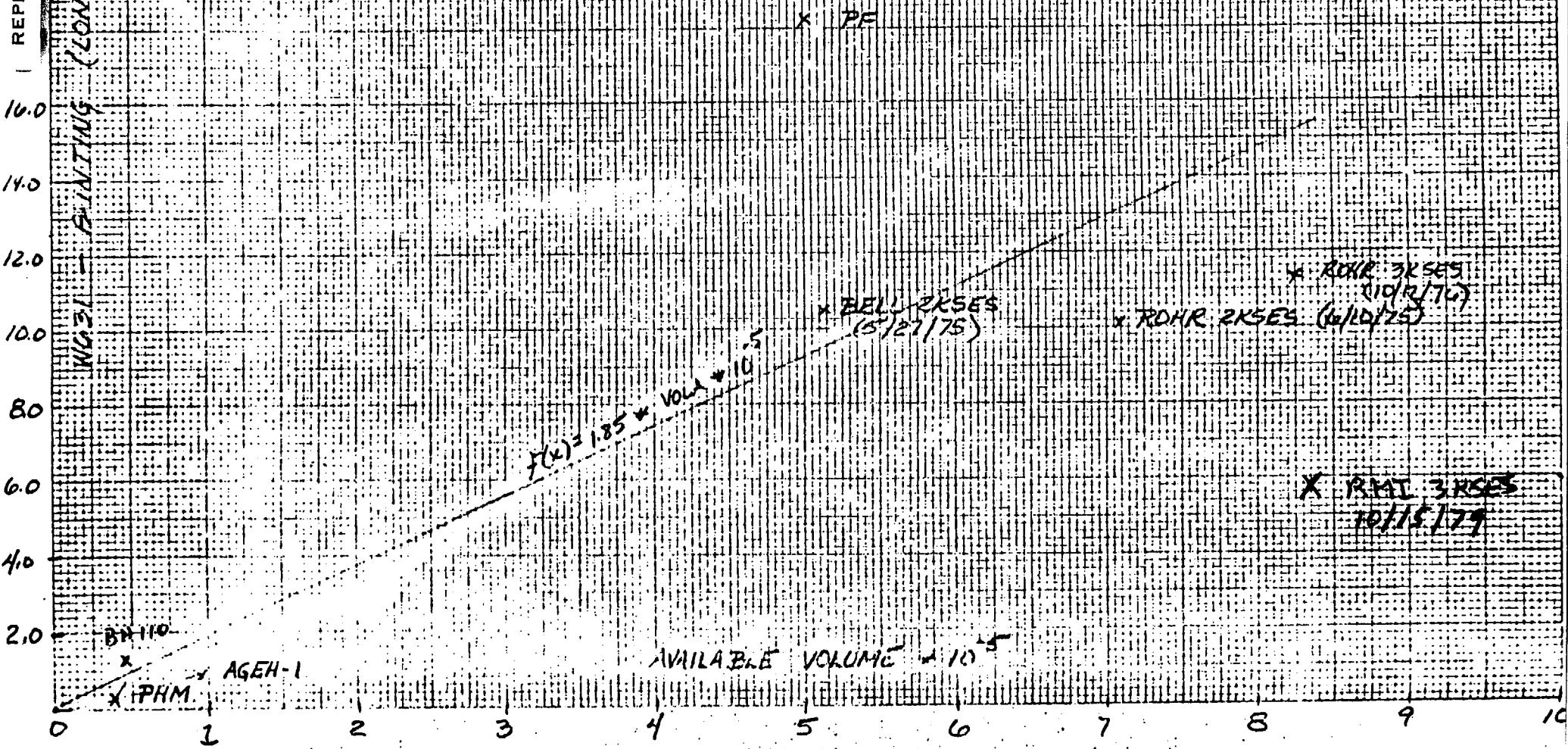
K631 = PAINTING

HAD 631 + K631 \* VOLA

K631 = .6185

VOLA = VOL 1/1000

X PF



## 633 Cathodic Protection

$$W_{633} = K_{633} \times VOLA$$

where  $K_{633} = .0032 \text{ lb/ft}^3$

( $K_{633}$  is a constant obtained from return data  
of hydrofoils and SESSs.)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

Algorithm is the same as ASSET.

## 634 Deck Covering

$$W_{634} = K_{634} \times VOL_{\Delta}$$

where  $K_{634} = .032 \text{ ft}/\text{ft}^3$

( $K_{634}$  is a constant obtain from return data from hydrologic and SES.)

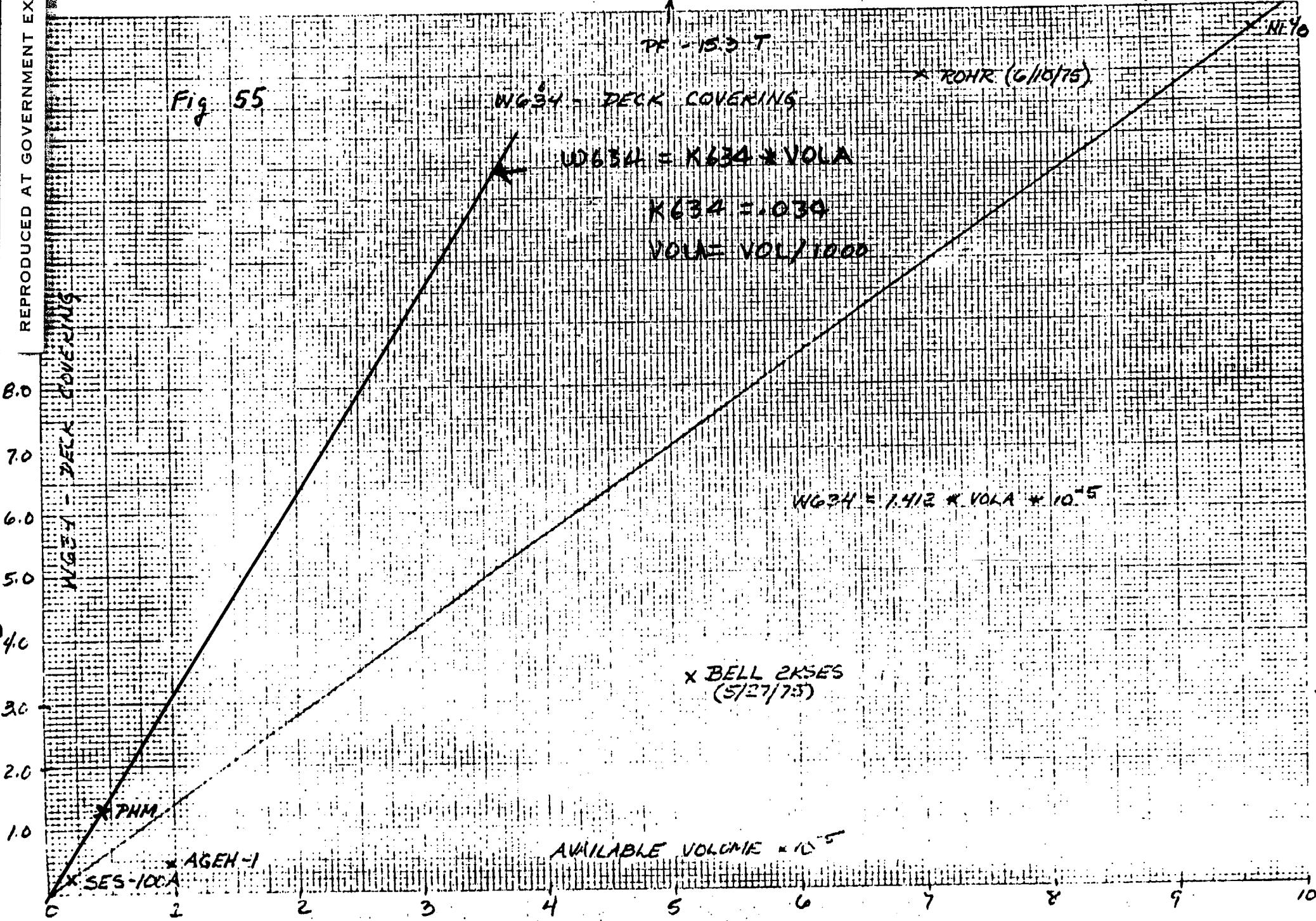
$$VOL_{\Delta} = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

Algorithm is the same as ASSET and  
SES Design Manual.

X  
ROHR 3K  
10/12/76

X HEY

Fig 55



## 635 Hull Insulation

$$WG35 = K635 \times VOLA$$

where  $K635 = .036 \text{ ft}/\text{ft}^3$

( $K635$  is a constant obtain from return data  
for hydrofoils and SESs.)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

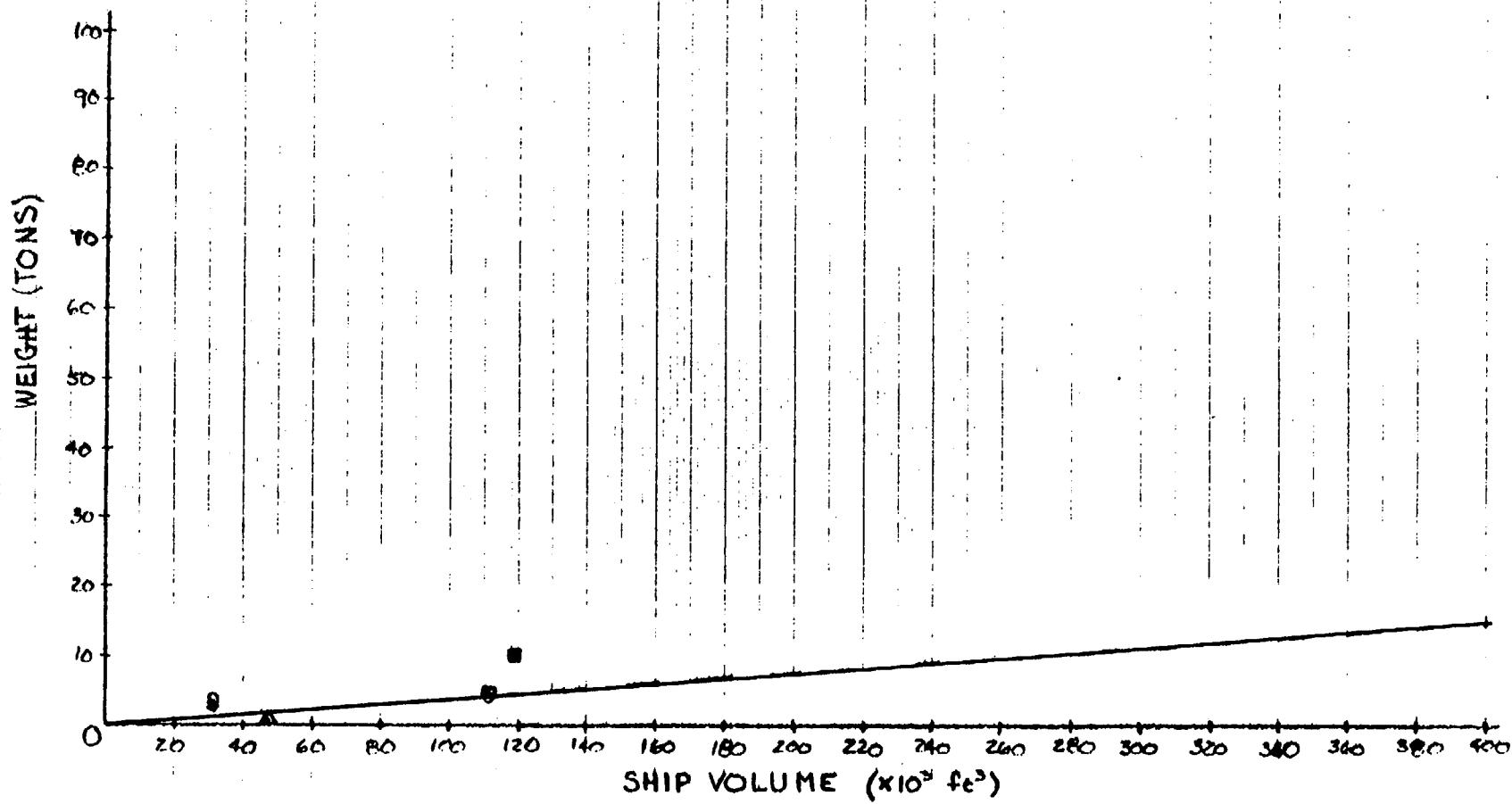
Algorithm based on SES Design Manual.

SWBS GROUP W635 HULL INSULATION

$$W635 = K635 * VOLA$$

$$K635 = .036$$

$$VOLA = VOL / 1000$$



636 Hull Damping

$$W_{636} = K_{636}$$

where  $K_{636}$  = Weight defined by  
in the combat suite.

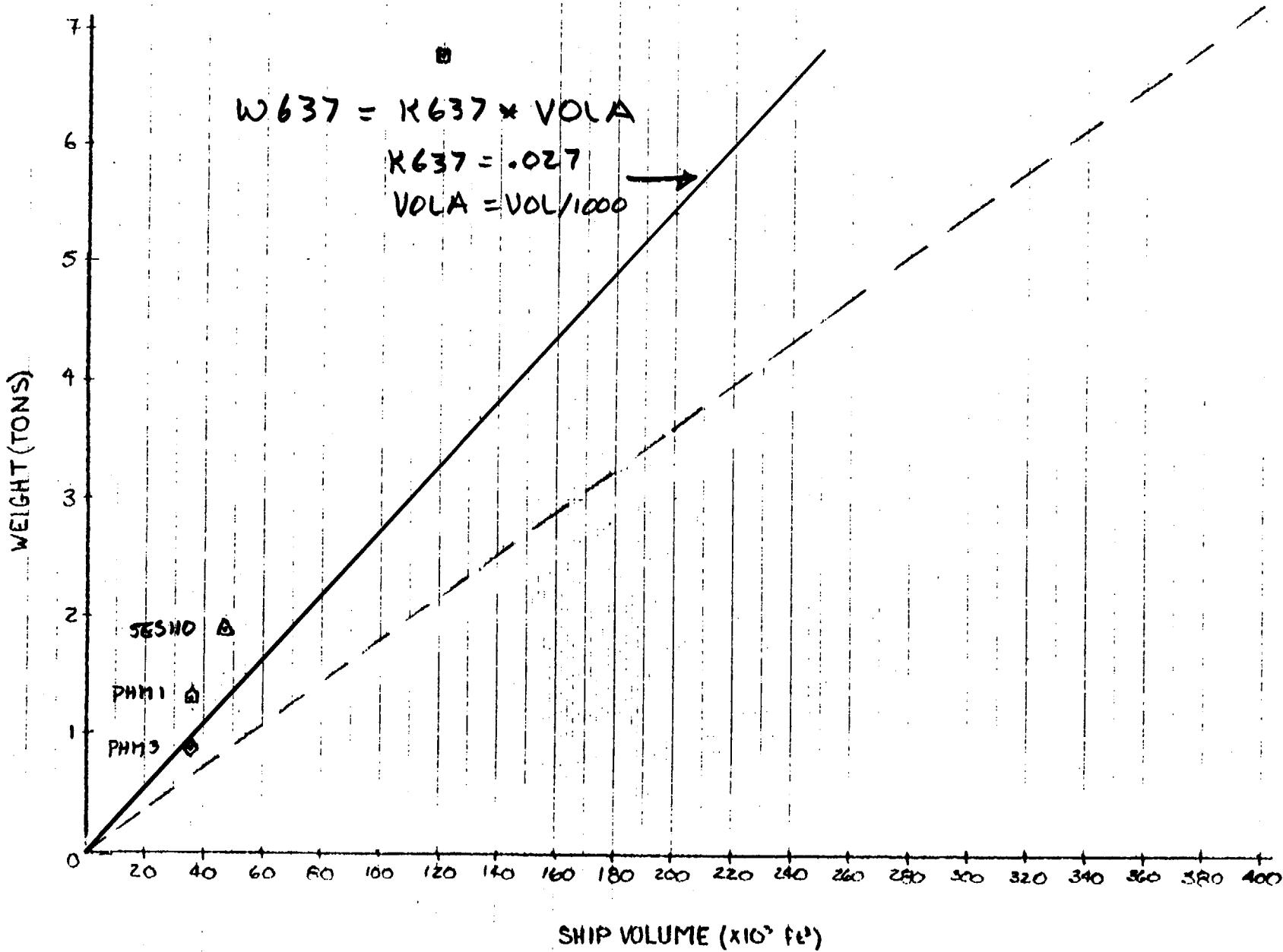
## 637 Sheathing

$$WG37 = K637 * VOLA$$

where  $K637 = .027 \text{ lb/f}^3$

( $K637$  is constant obtain from return data  
for hydrofoils.)

$VOLA = \text{Total Volume} * 10^{-3}, \text{ ft}^3$

SWBS GROUP W 637 SHEATHING

638 Refrigerated Space

$$WG38 = K638 * ACOM$$

where  $K638 = .0159 \text{ ft/person}$

( $K638$  is a constant based on return data  
for hydrofoils and SESs.)

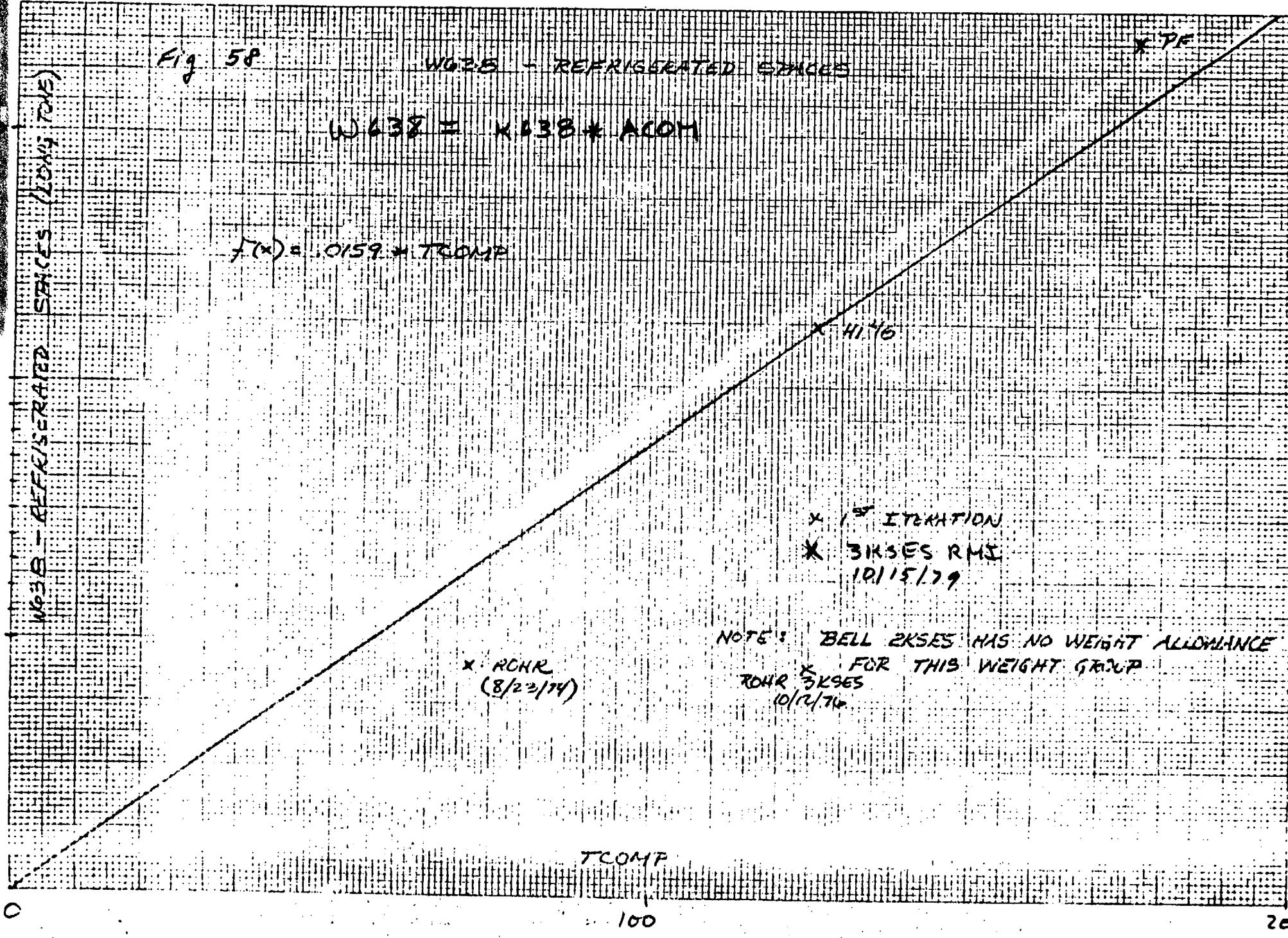
ACOM = Accommodations

This algorithm is based same as ASSET  
and SES Design Manual.

AND LARGER THAN PHM

2.0

2.0



641 Officer Berthing + Messen, Space

$$W_{641} = K_{641} * NOFF$$

where  $K_{641} = .038 \text{ ft } \underline{\underline{}}$

( $K_{641}$  is a constant based on return data  
from hydrofoils and SESs.)

$$\begin{aligned} NOFF &= \text{Number of Officer Accommodation} \\ &= 1.1 KOFF (\text{Number of Officers}) \end{aligned}$$

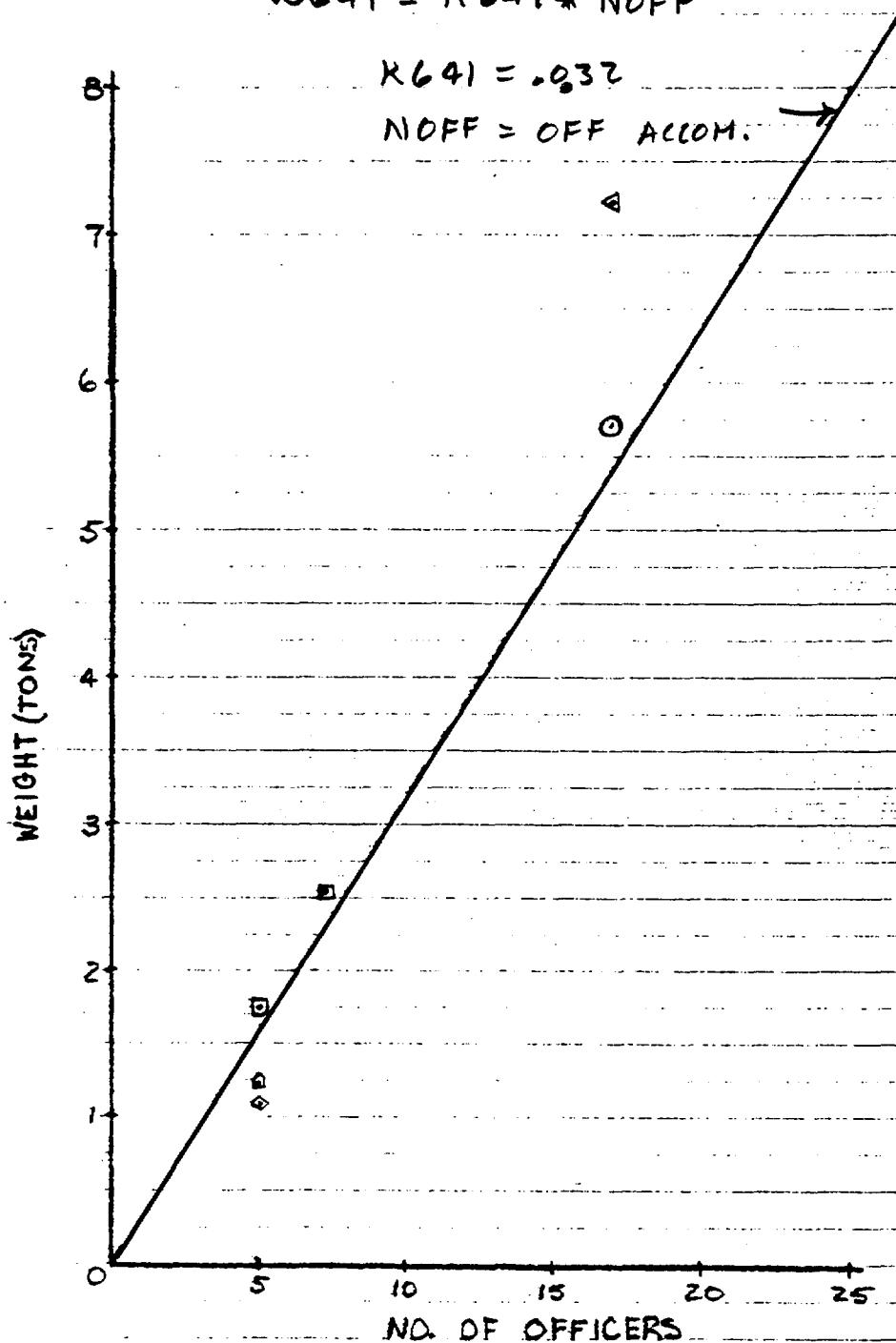
This algorithm is the same as ASSET and  
SES Design Manual.

SWBS GROUP W641 OFFICER BERTHING AND MESSING SPACES

$$W641 = K641 * NOFF$$

$$K641 = .032$$

NOFF = OFF ACCOM.



642 Non Commissioned Officer Berthing & Messing

$$W642 = K642 \times NCPO$$

where  $K642 = .153$  ft

( $K642$  is a constant obtain from the return data of hydrofoils and SESs.)

$$\begin{aligned} NCPO &= \text{Number of CPO Accommodation} \\ &= 1.1 KCPO (\text{Number of CPO}) \end{aligned}$$

Algorithm is the same as ASSET and SES Design Manual.

Exceeds PHM stds.

Fig 60

WG42 - CPO LIVING SPACES

WG42

H X 642 \* N 2 PO

$$R642 = .153$$

N CPO = CPO ACCOMMOD

f(4) = 92 + T<sub>1</sub> PO

x H 1 1/8

x BELL (5/27/75)

x ROHR 3KSES

10/12/76

x RMI 10/15/78

x ROHR (6/10/75)

x ROHR BASELINE

x PHM

ACCOMMODATIONS  
NUMBER OF CPO'S

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20

643 Enlisted Personnel Berthing + Messing

$$W643 = K643 * NENL$$

where  $K643 = .083$  et

( $K643$  is a constant obtain from the return  
weights of hydrofoils and SESs).

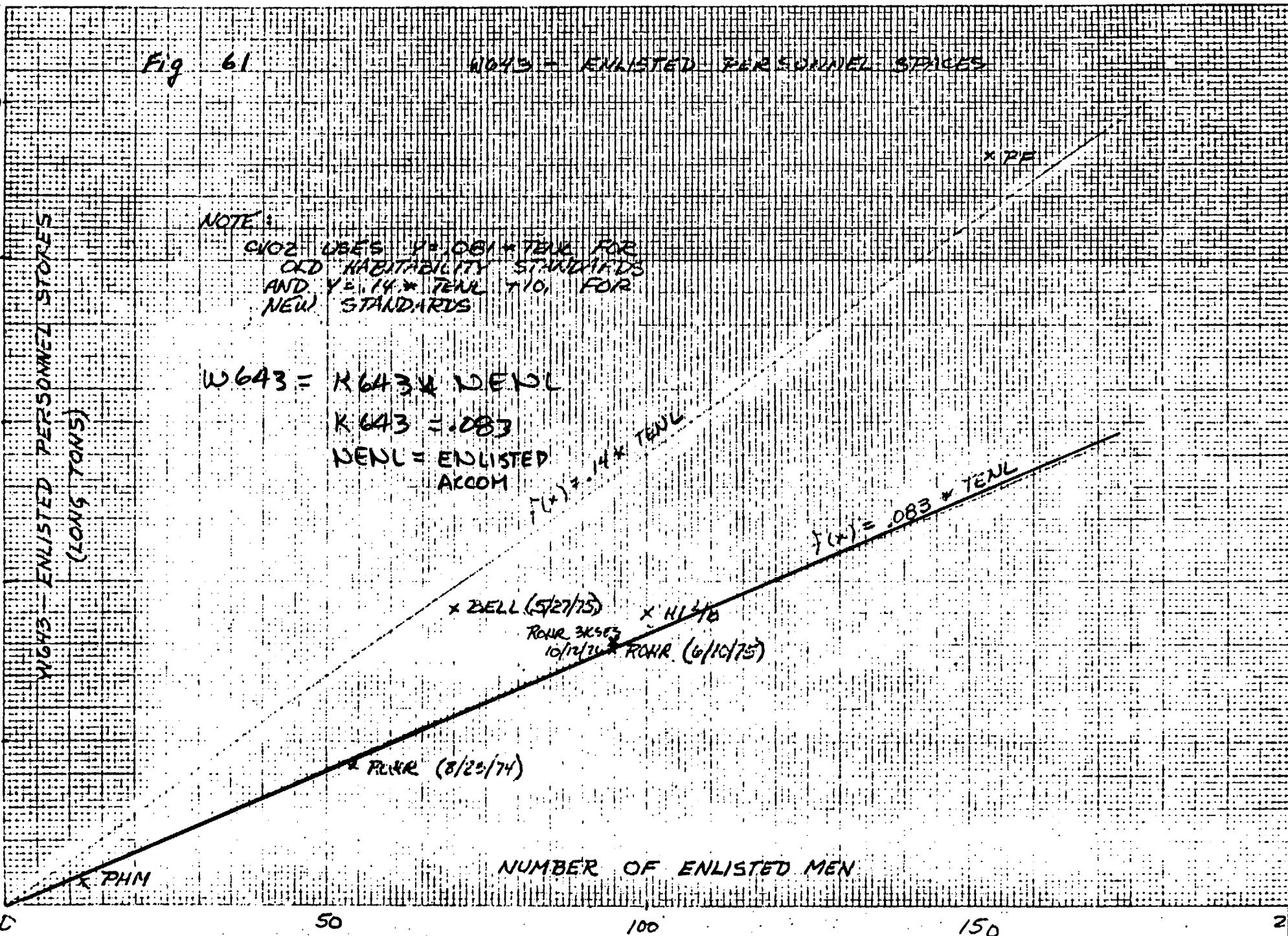
$NENL$  = Enlisted Accommodation.

$$\frac{1.1}{\cancel{1.0}} \cancel{KENL} \cancel{\text{Number}}$$

$$= 1.1 * KENL$$

$KENL$  = Number of Enlisted

The Algorithm is the same as ASSET and  
SES Design Manual.



## 644 Sanitary Space + Fixtures

5

$$W_{644} = K_{644} * A_{COM}$$

where  $K_{644} = 0.144 \text{ ft}$

( $K_{644}$  is a constant obtain from the return  
chart of hydrofoils and SESs.)

$A_{COM}$  = Number of Accommodations

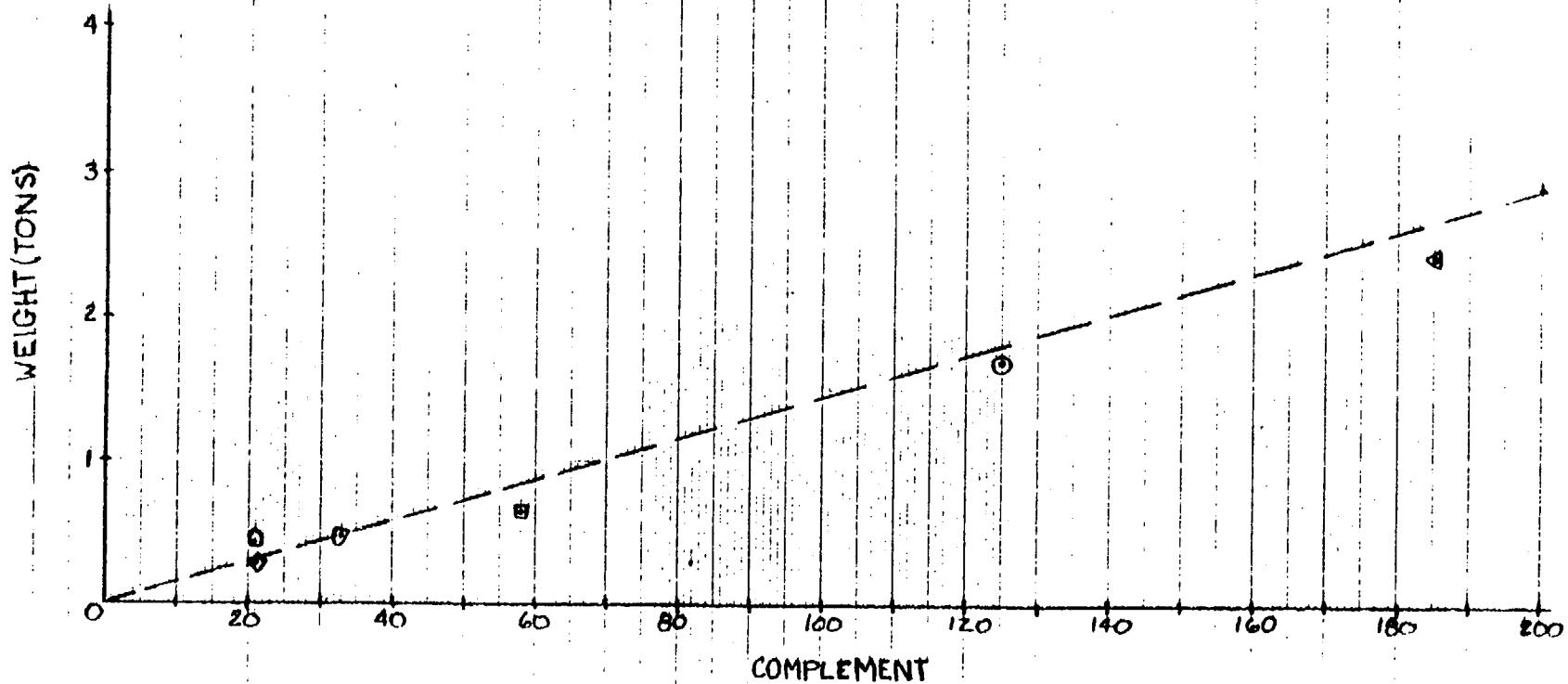
This Algorithm is same as ASSET.

SWBS GROUP W644 SANITARY SPACES AND FIXTURES

$$W644 = R644 * ACOM$$

$$R644 = .0144$$

ACOM = ACCOMMODATIONS



645 Leisure + Community Spaces

$$W645 = K645 \times ACOM$$

where  $K645 = 0$

(Based on ASSET,  $K645 = 0$  when  $ACOM < 150$ )

ACOM = Number of Accommodation

ASSET algorithm is used.

## LEISURE SPACES

SWES GROUP W645

$$W_{K645} = R_{645} + R_{645} * ACOM$$

$$L_{645} = 0 \text{ for } ACOM < 150$$

$$R_{645} = 0 \quad " \quad "$$

20

WEIGHTS (TONS)

1.5

1.0

0.5

0

G

1000

2000

DISPLACEMENT (TONS)

## 651 Commissary Spaces

$$W_{651} = \frac{K_{651}}{\text{ACOM}} + \frac{L_{651}}{\text{LESS}}$$

~~K<sub>651</sub>~~ (These constants are based on return weights of hydrofoils and LESS.)

where  $K_{651} = .035$  &  $L_{651} = .999$

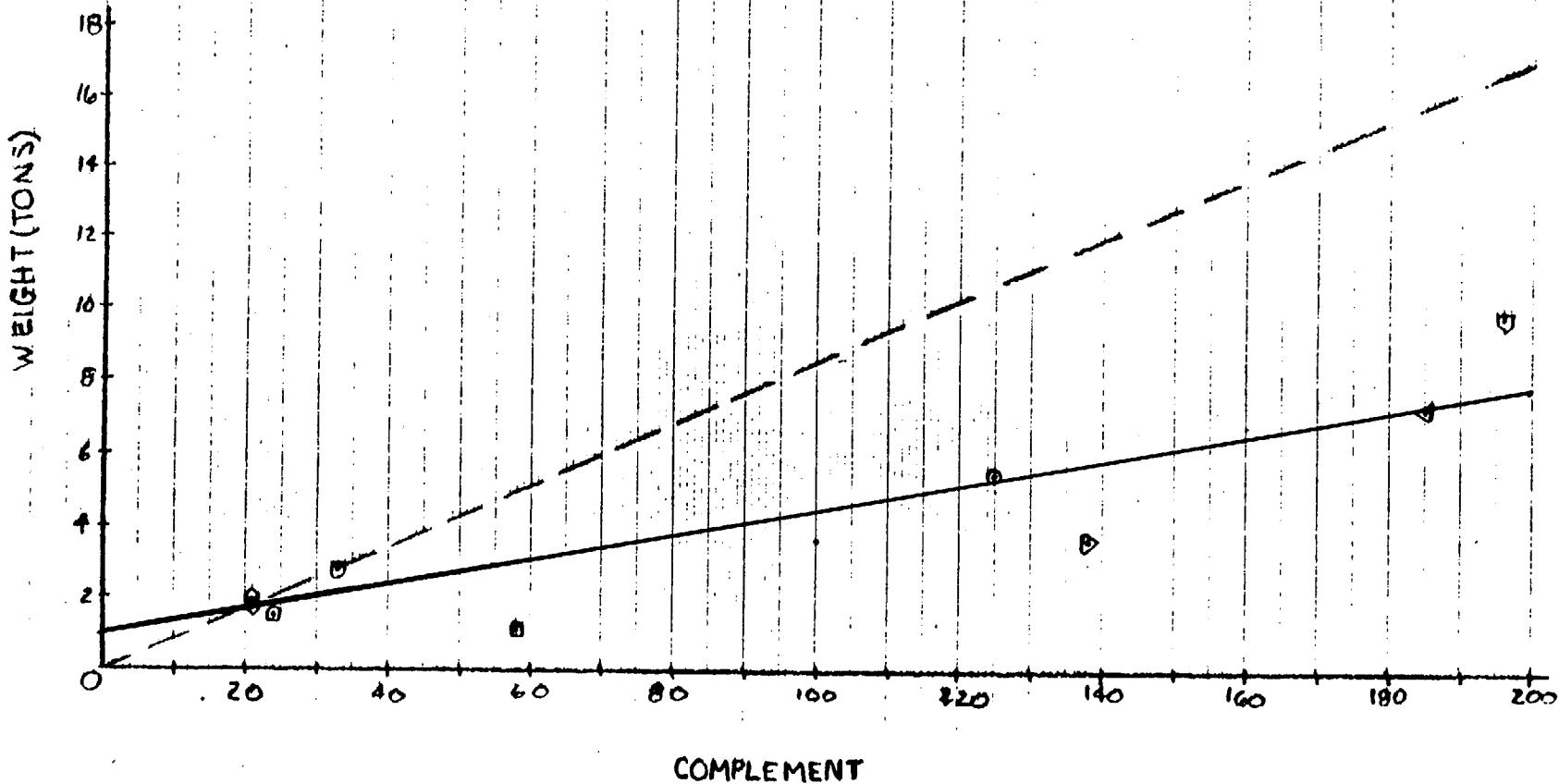
ACOM = Number of Accommodations

SWBS GROUP W651 COMMISSARY SPACES

$$W651 = L651 + K651 \Delta COM$$

$$L651 = .99$$

$$K651 = .035$$



## 652 Medicinal Space

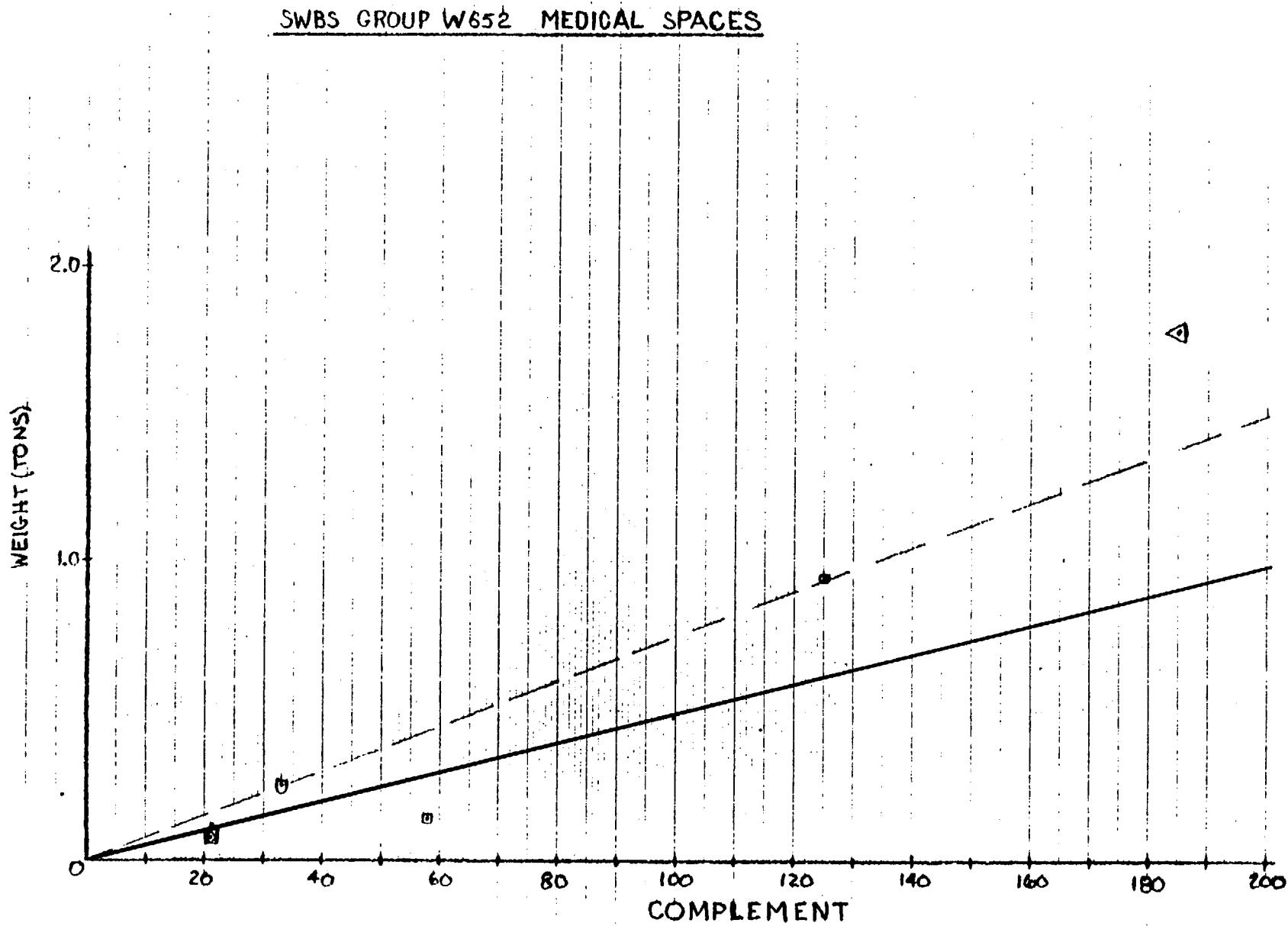
$$WGSZ = KGSZ * ACOM$$

where  $KGSZ = 1005 \text{ ft}$

( $KGSZ$  is a constant based on return data  
for hydrofoil and SESs ~~but~~ only valid  
when  $ACOM < 150$ .)

$ACOM$  = Number of Accommodation

The algorithm is based on the same as  
SES Design Manual.



## 654 Utility Space

$$W_{654} = \frac{K_{654}}{\# \text{ACOM}}$$

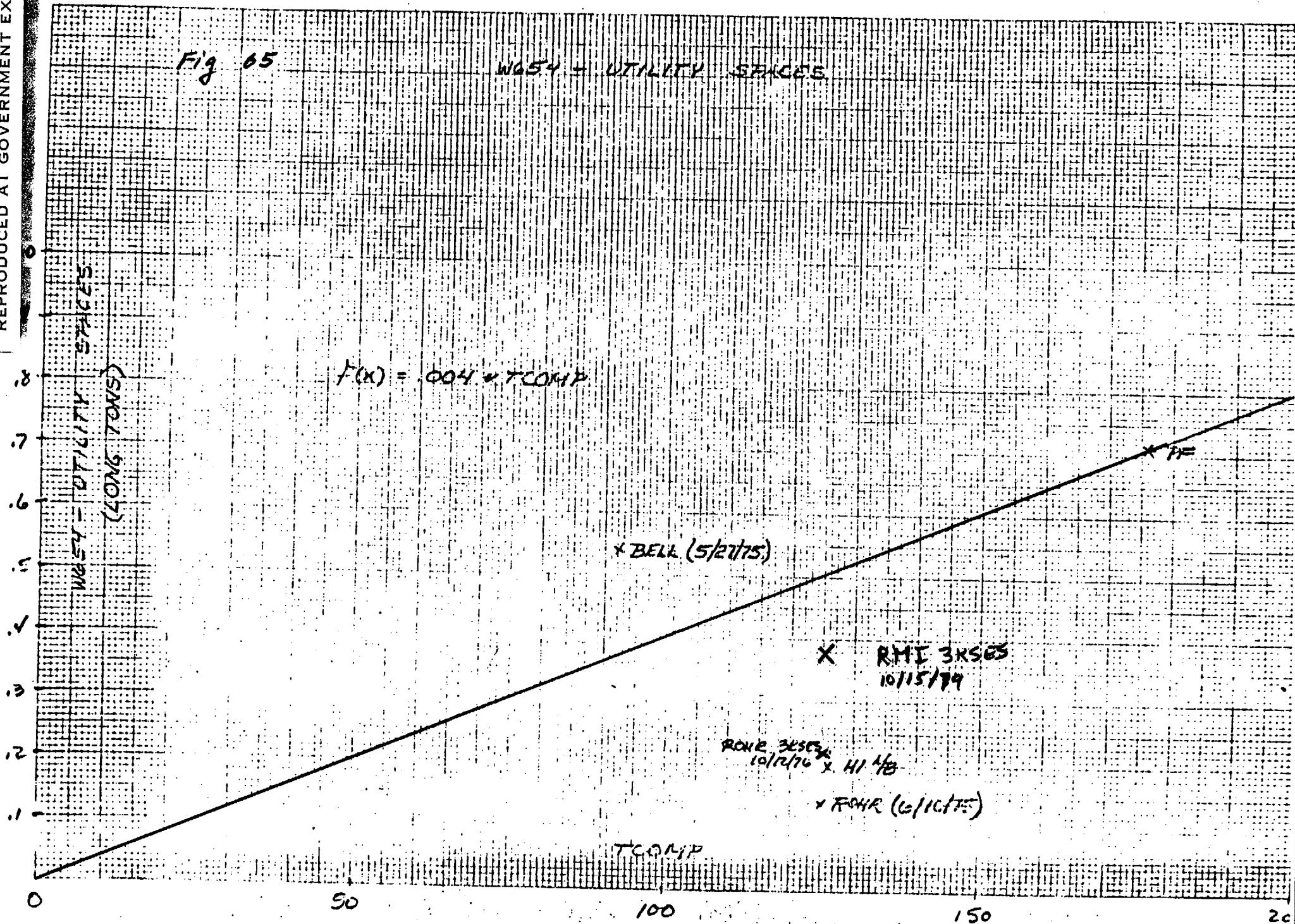
where  $K_{654} = .004$  SES Design Manual

\* ACOM = Number of Accommodation

This algorithm is from the SES Design Manual

Fig 65

WASH + UTILITY SPACES



655 Laundry Space

$$WGSS = K655 * ACOM$$

where  $K655 = .01$

( $K655$  is based SES-200 weight return  
chart.)

ACOM = Number of Accommodation

The algorithm is the same as ASSET and  
SES Design Manual.

Fig 66

WEST - LAUNDRY SERVICE

x H148

x PF

W3655 = K655 + ACOM

K655 = .01

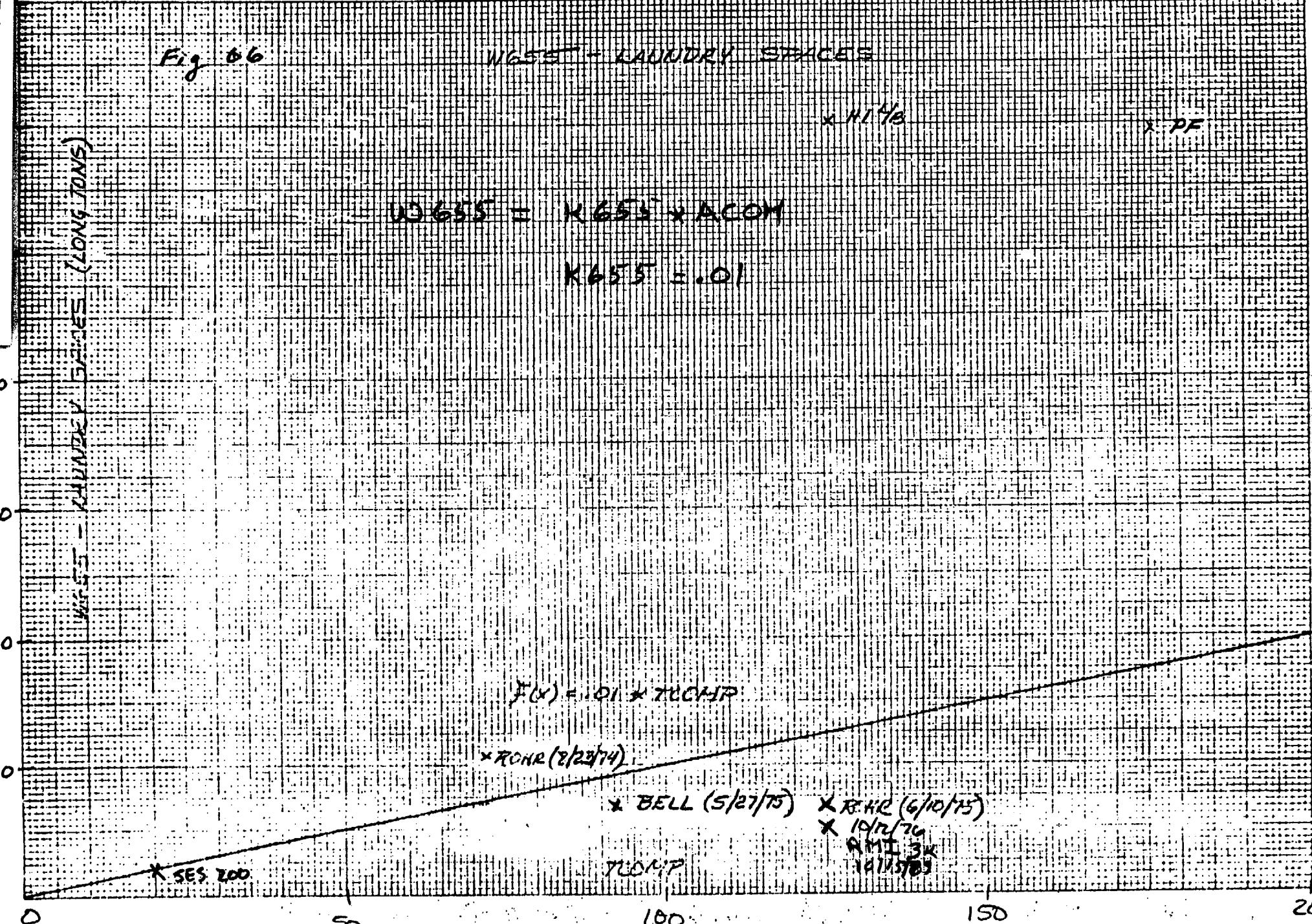
$$F(x) = .01 \times 7204P$$

x RHC (8/23/74)

x BELL (5/27/75) x RHC (6/10/75)

x 10/2/76  
2 MT 3K  
10/14/76

SES 200



## 656 Trash Disposal Space

$$W_{656} = \underline{.003} \cdot A_{COM}$$

where  $K_{656} = 10033 \text{ ft}^2$

( $K_{656}$  is based on return date of hydrofoile and SS.)

$A_{COM}$  = Number of Accommodation

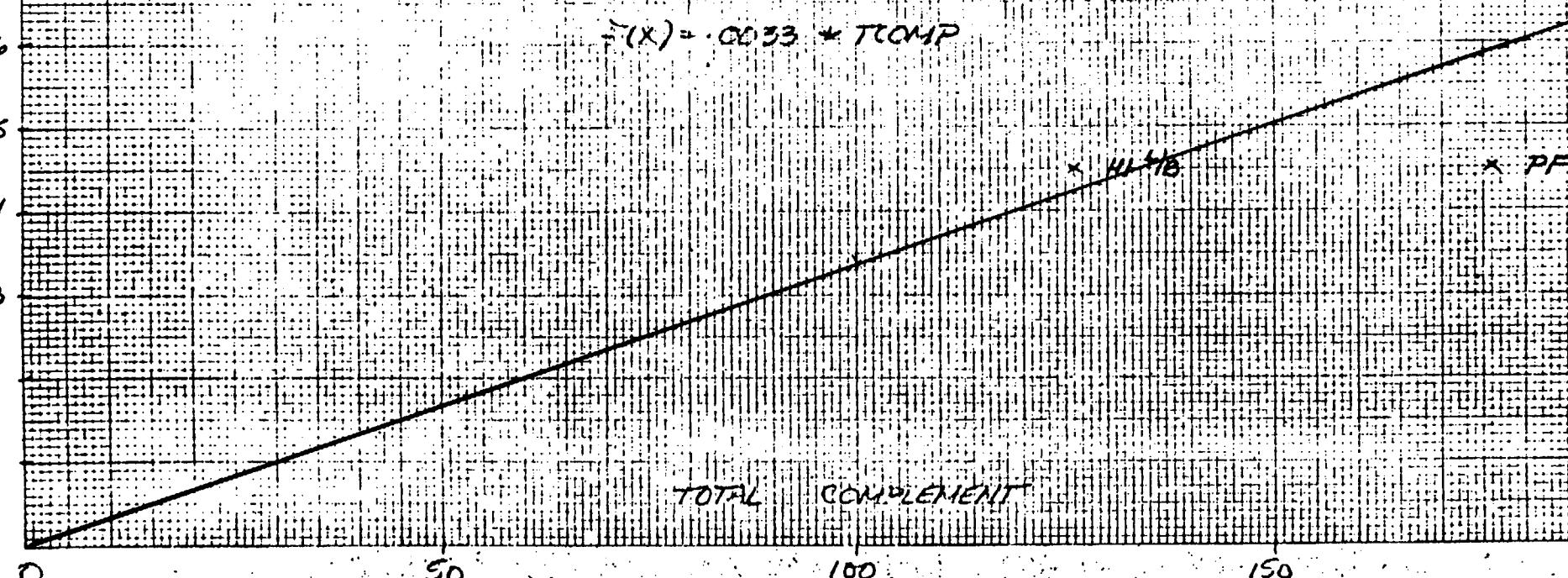
Algorithm is the same as S-75 Design  
Manual

Fig 67

WGS 67 TRANSMISSION SURFACES

NOTE: BOTH BELL & KELLY HAVE  
IMPROVED THIS MT. GROUP  
INTO "CONVENIENTLY SHAPES!"

$$\hat{r}(x) = .0033 + TCOMP$$



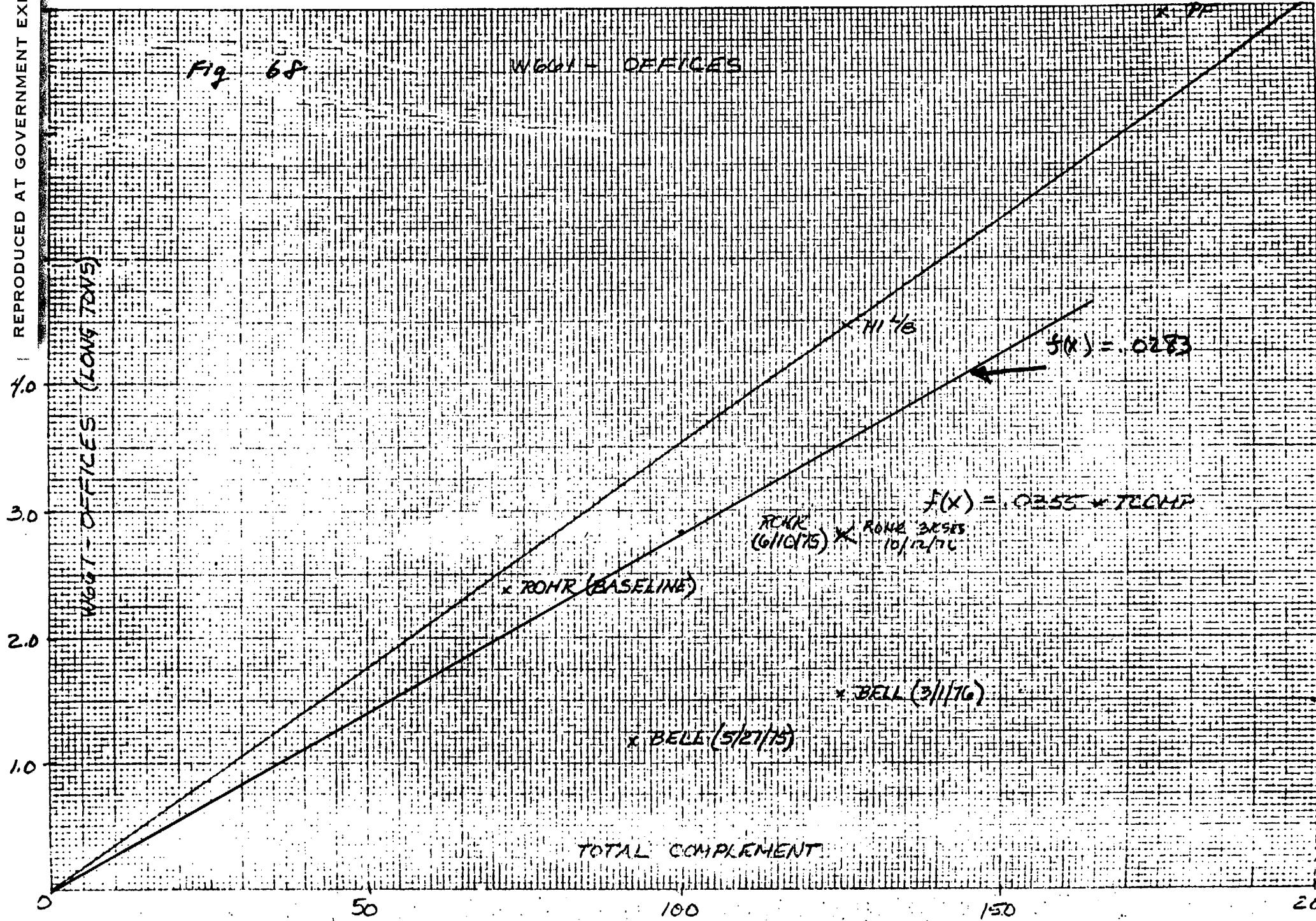
661 Officer

$$WGGI = KGGI \times ACOM$$

where  $KGGI = .62833$  ASSET

ACOM = Number of Accommodation

Algorithm is from ASSET.



## CC2 Machinery Control Center Furnishing

$$W_{CC2} = K_{CC2} \times HP$$

where  $K_{CC2} = 2.5 \times 10^{-5}$   $\text{ft}^2/\text{hp}$  (ASSET)

$HP$  = Total horsepower

Algorithm is from ASSET,  
AND FITS PHM

## 663 Electronic Control Center Furnishings

$$W_{663} = K_{663} \times VOLA$$

where  $K_{663} = .0103 \frac{lb}{ft^3}$  (ASSET)

$$VOLA = \text{Total Volume} * 10^{-3}, ft^3$$

Algorithm is the ASSET equation.

## 664 Damage Control Stations

$$W664 = K664 * VOLA + L664$$

where  $K664 = .0034 \frac{\text{ft}}{\text{ft}^3}$  &  $L664 = .35 \text{ ft}$

(These constants were obtained from return data for hydrofoils and 55 s.)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ ft}^3$$

Algorithm is the same as ASSET,

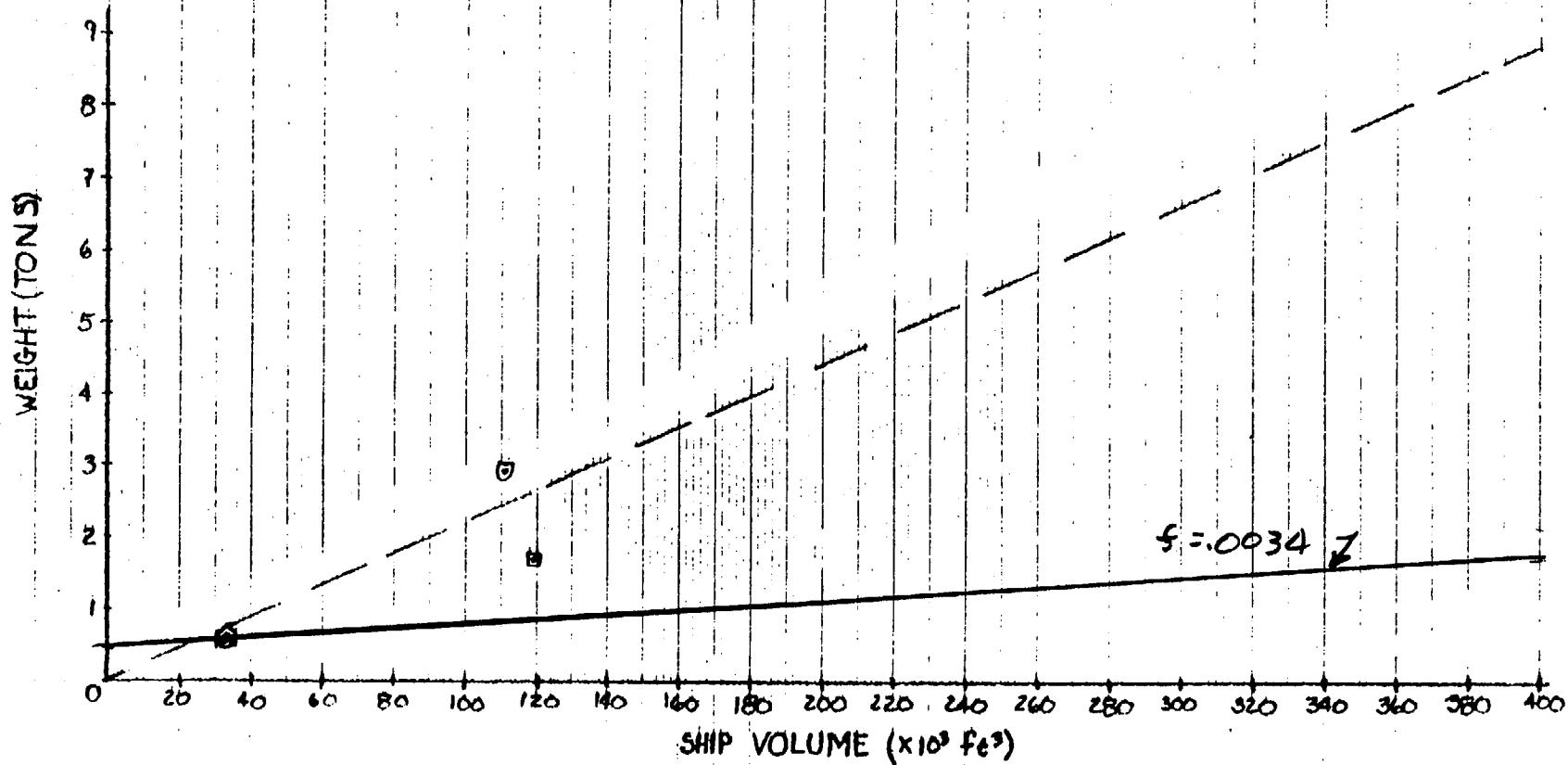
$K664$  from ASSET

$L664$  for PHM match

SWBS GROUP W 664 DAMAGE CONTROL STATIONS

$$W_{664} = K_{664} * V_{OLA} + L_{664}$$

$$K_{664} = .0034$$



## 6GS Workshops, Lmbs and Test Areas

$$W_{6GS} = K_{6GS} \times VOLA$$

where  $K_{6GS} = 0.001625 \text{ ft/f}^3$  (ASSET)

$$VOLA = \text{Total Volume} \times 10^{-3}, \text{ f}^3$$

This algorithm is from ASSET,



## 671 Lockers + Special Storage

$$WG71 = K671 * ACOM$$

where  $K671 = .017$  &

( $K671$  is a constant based on return data from hydrofoils and SESSs.)

ACOM = Number of Accommodation

The algorithm is the same as ASSET.

Fig 73

WOM - LOCKERS + SPECIAL TRAVAGE

R.P.F.

W67 - LOCKERS + SPECIAL TRAVAGE  
(LONG TDX's)

$$f(x) = .0285 \text{ m THOMP}$$

4.0

3.0

2.0

1.0

0

50

100

150

200

TOTAL COMPLEMENT

PNM

ROHR (E1-ECLINE)

BELL (5/27/75)

X HN 1/10

X BELL (3/11/76)

X ROHR 32355  
10/24/76

X ROHR (6/10/75)

$$S(x) = .017$$

672 Storerooms and Issue Rooms

$$W_{672} = K_{672} * ACOM$$

where  $K_{672} = .086$  ft (ASSET)

$\overline{ACOM}$  = Number of Accommodations

Algorithm is from ASSET.

## 698 Outfit + Furnishing Operating Fluids

$$W_{698} = \cancel{6.57 \times 10^{-4}} K_{698} (W_{600} - W_{690})$$

$$\text{where } K_{698} = 6.57 \times 10^{-4} \text{ lt (ASSET)}$$

$W_{600} - W_{690}$  = Summation of Outfit +  
Furnishing Weight except  
 $W_{698}$  and  $W_{699}$

The algorithm is same as ASSET.

699 Outfit and Furnishing Repair Parts  
+ Special Tools

$$W_{698} = K_{698} \times (W_{600} - W_{690})$$

where  $K_{698} = 6.667 \times 10^{-3}$  (ASSET)

$W_{600} - W_{690}$  = Total Outfitting and  
Furnishing Weights  
minus  $W_{698}$  and  $W_{699}$

Algorithm is the same as ASSET.

F II Ship Officer

$$WFII = KFII + NFII$$

where  $KFII = .179$  £ per person

$NFII = KOFF = \text{Number of Officers}$

F12 Ship Non Commissioned Officers

$$WF12 = KF12 * NF12$$

where  $KF12 = .147$  ft per person

$$NF12 = KCPO \equiv \text{Number of CPO}$$

## F13 Ship Enlisted Personnel

$$WF13 = KF13 \cdot NF13$$

where  $KF13 = .103$  ft per person

$NF13 = KENL$  = Number of enlisted personnel

## F21 Ship Ammunition

$$WF21 = KF21$$

where  $KF21$  = Weight of Ship Ammunition

Input Constant obtained from ~~etc.~~  
design requirements

## F22 Ordnance Delivery Systems Ammunition

$$WF22 = KF22$$

where  $KF22$  = Weight of Ordnance

Delivery System Ammunition

Input constant obtained from <sup>design</sup> requirements,

F 23      Ordnance Delivery System

$$WF_{23} = KF_{23}$$

where  $KF_{23}$  = Weight of Ordnance Delivery  
System

Input constant from obtain from design  
requirements.

F24 Ordinance Repair Parts (Ship Ammo)

$$WF24 = KF24$$

where  $KF24$  = Weight of Ordinance  
Repair Parts (Ship Ammo)

Input constant obtain from design requirements.

F25   Ordinance Repair Parts (Ord. Ammo)

$$WF25 = KF25$$

where    $KF25 = \text{Weight of Ordinance}$   
Repair Parts (Ord. Ammo)

Input constant obtain from design requirements.

F 26 Ordinance Delivery System Support Equipment

$$WF_{26} = KF_{26}$$

where  $KF_{26}$  = Weight of Ordinance  
Delivery System Support Equipment

Input Constant obtain from design requirements.

F29 Special Mission Related Systems and Expendables

$$WF29 = KF29$$

where  $KF29$  = Weight of Special Mission  
Related Systems and Expendables

Input constant obtain from design requirements.

42-381 150 SHEETS \$5 SQUARE  
42-382 200 SHEETS \$5.50 SQUARE  
42-389 200 SHEETS \$3.50 SQUARE



## F 31 Provisions + Personnel Stores

$$WF31 = NF10 * (CF30 * NSDD + CFCO * NSDC  
+ CFMO * NSDF + DFCO * NSDG)$$

where  $NF10 = \text{Complement} = NF11 + NF12 + NF13$

$NF11 = KOFF = \text{Number of Officers}$

$NF12 = KCPO = \text{Number of CPO}$

$NF13 = KENL = \text{Number of Enlisted Personnel}$

$CF30 = .00143$

$CFCO = .000736$

$CFMO = .000496$

$DFCO = .000173$

} Asset Constants

Where

$CF30$  is for dry stores

$CFCO$  is for chill stores

$CFMO$  is for frozen stores

$DFCO$  is for stock and clothes

And

$NSDD = \text{Number of dry store days}$

$NSDC = \text{Number of chill store days}$

$NSDF = \text{Number of frozen store days}$

$NSDG = \text{Number of general store days}$

## F32 General Stores

$$WF32 = NF10 \times (DF30 + NSDG + DF32)$$

where  $NF10 = NF11 + NF12 + NF13$

$$NF11 = KOFF = \text{Number of Officers}$$

$$NF12 = KCPO = \text{Number of CPOs}$$

$$NF13 = KENL = \text{Number of Enlisted Personnel}$$

$$\begin{aligned} DF30 &= .000472 \\ DF32 &= .0049 \end{aligned} \quad \left. \begin{array}{l} \text{ASSET Constants} \\ \text{for general} \\ \text{stores.} \end{array} \right.$$

$$NSDG = \text{Number of General Store Days}$$

F42      JP-5 (Aircraft Fuel)

$$WF42 = \text{Aircraft Fuel} = F42A$$

Input constraint obtain from design requirements.

## F46 Lubricating Oil

$$WF46 = KF46 * (HPT + 1.34 KWI)$$

where  $KF46 = .00028$  Based on DDG-51

$HPT$  = Total Horsepower, hp

$KWI$  = Installed Ship Service Power, kw

F 52 Fresh Water

$$WF52 = KF52 \times ACOM$$

where  $KF52 = \underline{\underline{.032}}$  based on PHM

(8.6 gallons per ~~per~~  
accommodation)

ACOM = Number of Accommodation

$$= 1.1 \times NF10$$

$$NF10 = NF11 + NF12 + NF13$$

NF11 = KOFF = Number of Officers

NF12 = KCPO = Number of CPO

NF13 = KENL = Number of Enlisted Personnel

42-381 50 SHEETS 55 SQUARE  
42-382 200 SHEETS 55 SQUARE  
42-383



665

664 Workshop, Lab & Test Areas

W665 = K665 \* VOLA

where K665 = 0.01625

ASSET (for all but CGV)

W665 = K665 *1/2*

Where K665 = 25

CGV RESOLUTION (for CGV only)

671 Lockers & Special Stowage

W671 = K671 \* VOLA

where K671 = 0.0085

NAVSEA DATA FIT

672 Store Rooms & Issue Rooms

W672 = K672 \* COMP

where K672 = 0.192

ASSET

698 Outfit & Furnishings Operative Fluids

W698 = K698 \* W650

where K698 = 0.05

SES DESIGN MANUAL

699 Outfit + Furnishings Sprte Parts

W699 = K699 \* (W600 - W698 - W699)

where K699 = 0.02

SES DESIGN MANVAL

## VARIABLE LOADS (Tons)

SWBS #	DESCRIPTION	ACTUAL DATA	SES ACC	PREDICTED ACC
F11	SHIPS OFFICERS	4.1	4.1	4.1
F12	SHIPS NONCOM COMMS	4.0	4.0	4.0
F13	SHIPS ENLISTED MEN	27.6	27.6	27.6
F21	SHIP FUEL TANKS	161.3	161.3	161.3
F22	ORDNANCE DEE S&S AMMO	0.0	0.0	0.0
F23	ORDNANCE DEE SYS.	18.6	18.6	18.6
F26	" " " SUPPORT EQUIP	18.7	18.7	18.7
F31	PROVISIONS + PERSONNEL STORES	39.5	40.4	40.4
F32	GENERIC CLOTHES	13.2	7.6	7.6
F41	ACCESSORIES	1524.0	1524.0	1524.0
F42	JET 5	100.0	100.0	100.0
F46	LUBRICATION OIL	20.0	25.0	25.0
F51	SEAWATER	0.0	0.0	0.0
F52	FRESH WATER	52.2	52.2	52.2
F55	SANITARY THIN CLOTH	6.0	6.0	6.0
F00	TOTAL LOADS	1989	1990	1990

VARIABLE LOADS FIX

SUBS &	DESCRIPTION	ACTUAL DATA	SES ALG	MULT-CD ALG
F1	SHIPS DEF LEADS	4.1	2.9	2.9
F12	SHIPS HULL AND DEFENSE	2.9	2.4	2.4
F2	SHIPS EXISTING LOAD	26.6	19.3	19.3
F21	SHIPS AIRPORT	91.8	91.8	91.8
F22	ORDNANCE DECL. SHIP ARMS	0.0	0.0	0.0
F23	" "	0.0	0.0	0.0
F26	SHIP CO. F.	0.0	0.0	0.0
F31	PRECISIONS & PERSONNEL STORES	35.2	31.1	31.1
F32	GENERAL STORES	7.9	5.8	5.8
F41	DIESEL FUEL	798.8	799.8	798.8
F42	JP-5	0.0	0.0	0.0
F46	LUB. OIL	6.6	12.1	12.1
F51	SEPARATORS	0.0	0.0	0.0
F52	TENS	44.9	36.0	36.0
F55	SANITARY TANK LIQUIDS	5.0	4.1	4.1
F00	TOTAL LOADS	1024	1004	1004

F 32 General Stores

WF 32 = DF 30 \* NF 10 where  $DF 30 = .024$   
ASSET

F 46 Lubricating Oil

WF 46 = KF 46 \* HPT where  $KF 46 = .00025$

F 52 Fresh Water

WF 52 = KFS2 \* COMP where  $KFS2 = .149$

F 55 Sanitary Tank Liquid

WF 55 = KF 55 \* COMP where  $KF 55 = .017$

# VARIABLE LOADS CGV

SWBS #	DESCRIPTION	ACTUAL DATA	SES ALC	MODIFIED ALC
F 11	SHIPS OFFICERS	16.8	16.6	16.6
F 12	SHIPS NONCOMMISSIONED OFFICERS	9.8	9.6	9.6
F 13	SHIPS ENLISTED MEN	103.1	103.0	103.0
F 21	SHIP AMMUNITION	523.9	523.9	523.9
F 22	ORDNANCE DELIVERY SYSTEMS AMMUNITION	400.0	400.0	400.0
F 23	ORDNANCE DELIVERY SYSTEMS	173.2	173.2	173.2
F 26	ORDNANCE DELIVERY SYSTEMS SUPPORT EQUIPMENT	103.2	103.2	103.2
F 31	PROVISIONS & PERSONNEL STORES	200.2	149.0	149.0
F 32	GENERAL STORES	47.9	27.8	27.8
F 41	DIESEL FUEL	2685.1	2685.1	2685.1
F 42	JP-5	700.0	700.0	700.0
F 46	LUBRICATING OIL	33.8	34.5	34.5
F 51	SEA WATER	0.0	0.0	0.0
F 52	FRESH WATER	189.5	189.8	189.8
F 55	SANITARY TANK LIQUID	10.2	21.6	21.6
F00	Total Loads	5206	5137	5137

SUBS #	DESCRIPTION	VARIABLE LOAD	DEPT	ACTUAL DATA Tons	SUS Tons	ADDITIONAL Tons
		TONS	TONS			
F11	SHIPS C-7 CARS	2.1	3.2	3.2		3.2
F12	SHIPS NONDISMISSED CREW	32	2.1	2.1		2.1
F13	SHIPS ENLISTED MEN	27.1	28.4	28.4		28.4
F21	SHIP AMMUNITION	200.9	200.9	200.9		200.9
F22	ORDNANCE DELIVERY SYSTEMS TONS.	0.0	0.0	0.0		0.0
F23	ORDNANCE DELIVERY SYSTEMS	0.0	0.0	0.0		0.0
F26	ORDNANCE DEL. SYS SUPPLIERS	0.0	0.0	0.0		0.0
F31	PROVISIONS & PERSONNEL STORES	39.5	39.7	39.7		39.7
F32	GENERAL STORES	13.2	7.4	7.4		7.4
F34	DIESEL FUEL	1199.2	1199.2	1199.2		1199.2
F42	JET-5	62.1	62.1	62.1		62
F43	LUBRICATION OIL	20.0	25.0	25.0		25.0
F51	SEA WATER	50.6	54.6	54.6		54.6
F52	FRESH WATER	45.9	50.5	50.5		50.5
F53	SANITARY TANK LIQUID	21.6	5.8	5.8		5.8
F60	TOTAL LOADS	1691	1679	1679		1679

# VARIABLE LOADS ALGORITHM

F11 Ship Officers

$$WF_{11} = KF_{11} \times NF_{11} \quad \text{where } NF_{11} = NOFF/1.1$$
$$KF_{11} = .175$$

ASSET

F12 Ship Noncommissioned Officers

$$WF_{12} = KF_{12} \times NF_{12} \quad \text{where } NF_{12} = NCPO/1.1$$
$$KF_{12} = .147$$

ASSET

F13 Ship Enlisted Personnel

$$WF_{13} = KF_{13} \times NF_{13} \quad \text{where } NF_{13} = NENL/1.1$$
$$KF_{13} = .103$$

ASSET

F31 Provision and Personnel Stores

$$WF_{31} = NF_{10} \times (CF_{30} \times NSDD + CF_{CO} \times NSDC + CF_{MO} \times NSDF + DF_{CO} \times NSOG)$$

$$\text{where } NF_{10} = NF_{11} + NF_{12} + NF_{13}$$

$$CF_{30} = .00125 \quad NSDD = 45$$

$$CF_{CO} = .000736 \quad NSDC = 30$$

$$CF_{MO} = .000494 \quad NSDF = 45$$

~~CF<sub>CO</sub>~~ 
$$= .000625 \quad NSOG = 45$$